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- 7. Watershed Management & Stream Restoration
- 8. Wednesday Sessions
- 9. Workshops

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Bookmarks

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IVERSIDE

CASFM Presentation Colorado's Flood Decision Support System

> RIVERSIDE Amy Volckens Jay Day

AMEC Graeme Aggett

CWCB Carolyn Fritz Chris Sturm

Colorado Water Conservation Board

Agency

To conserve, develop, protect and manage Colorado's water for present and future generations

Flood Section

To devise and formulate methods, means, and plans to prevent or mitigate human and infrastructure losses due to flooding, to educate the public about flood risk, and to protect the natural and beneficial functions of floodplains and watersheds.







Colorado's Flood Decision Support System



Objectives

- Provide a statewide clearinghouse of flood information
- Be useful to a varied audience
- Integrate state systems
- Provide dynamic information







Colorado's Flood Decision Support System



Flood DSS Mapping Applications

The State of Colorado has developed the following interactive mapping applications to provide a statewide clearinghouse of flood-hazard and related information.

- Flood DSS Map Viewer
 - Review effective floodplain boundaries.
 - · See real-time weather and streamflow conditions.
 - Access local and county data related to flooding.
 - Access data related to historical floods, hazards, weather modification, watershed restoration, and FEMA's National Flood Insurance Program.
- Weather Modification
 - Assess current snow conditions near weather modification locations.
- Watershed Restoration
 - Assess streamflow conditions near restoration project locations.

Additional Resources

System Requirements

At this time, the flood mapping applications support Internet Explorer 7 and Firefox 3.5 and higher. Most features are also available for other browsers. You may need to disable your pop-up blocker to view metadata or to print a formatted map.

Help

Please direct all questions or comments to the site administrator.







Logic

























































Additional Functionality

- Laserfiche
- Add
- Qui
- Meta
- Help

🖉 Flood DSS Map Viewer Help - Windows http://prevenod riverside.com/flooddor/heip/la

Flood DSS Map Viewer Help

Flood DSS Overview Map Viewer Overview Getting Started Map Contents Map Navigation

Frequently Asked Questions

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Tools

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Project Status and Plans

http://flooddss.state.co.us/

- Visit CWCB's booth!
- What next?
 - Statewide historical flood layer
 - Print functionality
 - Identify functionality for web services
 - Continue to identify use cases



Acknowledgements

For providing data and/or participating in the user needs assessment, we would like to thank:

- HDR
- CO Division of Water Resources
- CO Division of Emergency Management
- 5-2-1 Drainage Authority
- Anderson Consulting Engineers
- Colorado River Water Conservation District
- Dewberry
- FEMA Region 8
- NOAA National Severe Storms Laboratory
- NOAA National Operational Hydrologic Remote Sensing Center
- NRCS
- Pikes Peak Regional Building Department

- San Luis Valley GIS/GPS Authority
- Urban Drainage and Flood Control District
- Cities of Boulder, Fort Collins, Colorado Springs
- Counties of Adams, Arapahoe, Broomfield, Chaffee, Clear Creek, Delta, Denver, Douglas, Eagle, Elbert, Garfield, Grand, Gulpin, Gunnison, Jefferson, La Plata, Larimer, Mesa, Montezuma, Montrose, Ouray, Park, Pueblo, San Miguel, Summit, Teller, Weld



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Risk MAP Products & Datasets Overview

September 2010

Overall objective: To provide participants with a functional understanding of what flood risk products and datasets will be developed and delivered in support of Risk MAP's vision and goals.







Agenda

Overview of what will be covered

- Map Mod to Risk MAP
- Overview of Datasets
 - Changes Since Last FIRM
 - Flood Depth & Analysis Grids
 - Flood Risk Assessment Data
 - Areas of Mitigation Interest (enhanced)
- Overview of Products
 - Flood Risk Database
 - Flood Risk Report
 - Flood Risk Map
- Flood Risk Assessment Process Overview
- Flood Risk Products Project Lifecycle Overview







The Paradigm Shift: Map Mod to Risk MAP



- Map Modernization used increasinglyavailable technology to increase the quality, reliability, and availability of flood hazard maps and data
- It focused on digitizing maps to provide timely, accurate information to community planners



Increasing Resilience Togethe

Risk MAP further enhances the maps, involves communities during the assessment and planning stages, and guides and encourages them to communicate risk to their constituents



Risk MAP

Through collaboration with State, Local, and Tribal entities, Risk MAP will deliver **quality data** that increases <u>public awareness</u> and leads to <u>action that reduces risk</u> to life and property.









Program Product Comparisons



Traditional products are regulatory and subject to statutory due-process requirements Risk MAP products are nonregulatory and are not subject to statutory due-process requirements







Flood Risk Products and Data Model



Ad-Hoc Flood Risk Analyses









Flood Risk Datasets

- Changes Since Last FIRM
- Flood Depth & Analysis Grids
- Flood Risk Data
- Areas of Mitigation Interest









Changes Since Last FIRM Dataset







Purpose and Intended Uses

Identify Areas and Types of SFHA Change Between:

- Current Effective or Previous SFHAs (must be digital)
- Proposed or New SFHAs
- Results and/or SFHA Changes are Quantified

Provide Study/Reach Level Rationale for Changes Including:

- Methodology and Assumptions
- Changes of Model Inputs or Parameters (aka Contributing Engineering Factors)

• Offer Stakeholders Transparency and Answers to:

- Where has my SFHA increased or decreased?
- Why has my SFHA increased or decreased?
- Which communities are subject to new BFEs or ordinance adjustments.








Previous Mapping

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New Mapping

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Changes Since Last FIRM

Unchanged

SFHA Increase

SFHA Decrease

Unchanged

SFHA Increase

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Unchanged



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Changes Since Last FIRM

Unchanged

SFHA Increase

SFHA Decrease

Enhanced

Data Fields Include	Example Data Values
Old Study Date	e.g. 1985
Old Model Type(s)	e.g. HEC-1 / HEC-2
Old Zone Type	e.g. Zone A
Old Topography	e.g. USGS 10-ft
New Study Info/Methods	Dates, Models, etc.
New Study Zone	e.g. Zone AE
New Topography	e.g. LiDAR 2-ft
New Study Engineering Factors / Changes	e.g. new structures, gages, topo, landuse, etc.
Estimated Structures	e.g. 9
Estimated Population	e.g. 27

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Content Scalability

Base

- GIS Layer (vector polygon based upon spatial intersect of pre and post SFHA datasets)
- Attached table attributes containing pre and post SFHA zone designations and study information including contributing engineering factors.

Enhancements *

Same as above with addition of structures and population impacts (requires locally provided input data, e.g. footprints, parcels, etc.)

Changes Since Last FIRM	Riverine	Coastal	Levee
Vector Polygon Boundaries			
Pre and Post SFHA Zone Information			\checkmark
Contributing Engineering Factors			\checkmark
Structure and Population Estimates	*	*	*





Changes Since Last FIRM Distribution Context



Ad-Hoc Flood Risk Analyses









Flood Depth & Analysis Grids





Flood Depth & Analysis Grids Purpose and Intended Uses

- Communicate / "Show" Flood Inundation as Function of Event"s Magnitude or Severity
- Serve as Key Inputs to HAZUS Risk Assessment Analyses
- Serve as pre-screening criteria for mitigation project potential (e.g. BCA > 1.0 with positive 10-yr depths)
- Increase Flood Risk Awareness as Acknowledged from Varied Contexts (Depth, Probability, Velocity, etc.)
- Communicate that Hazard, and by extension Risk, varies within the mapped floodplain





Flood Depth & Analysis Grids (red = enhanced)

- Depth: 10% (10-yr), 4% (25-yr), 2% (50-yr), 0.2% (500-yr) Annual Chance
- Depth: 1% (100-yr) Annual Chance
- Depth: Additional Flood Frequencies (e.g. 50% (2-yr), 20% (5-yr), 0.5% (200-yr), 1% "plus", etc.)
- Percent Annual Chance of Flooding
- Percent Chance of Flooding over a 30-yr Period
- Water Surface Elevation: 10%, 4%, 2%, 1%, 0.2%
- Water Surface Elevation Change
- Depth: Annualized
- Velocity
- Top & Toe of Levee





Flood Depth Grids (Depth_XXpct)

• Mase Datasets

- Riverine: 10%, 4%, 2%, 1%, & 0.2%
 Annual Chance (A.C.) Floods
- Coastal: 1% A.C. Flood
- Levee: 1% A.C. Flood

Enhanced Datasets

 Riverine, Coastal, and Levee: Any depth grid associated to a flood frequency other than those listed above as Base Datasets (e.g. the 2% Coastal depth grid, the 0.5% Riverine depth grid, etc.)







• Each Grid Cell has a Unique Value







Flood Depth Grid Creation Process







Water Surface Elevations (WSE) Calculated and WSE Grid Produced







Depth Grid Calculated as Difference between WSE and Ground







10% Depth (10-Year)

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1% Annual Chance Floodplain Boundary

0.0 ft

1.5 ft

0.0 ft

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0 - 1 ft 1 - 2 ft 2 - 3 ft 3 - 6 ft 6 ft +

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0.0 ft

2.8 ft

0.0 ft

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2% Depth (50-Year)

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0.0 ft

3.8 ft

0.0 ft

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1% Depth (100-Year)

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0.0 ft

4.7 ft

0.1 ft

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0 - 1 ft 1 - 2 ft 2 - 3 ft 3 - 6 ft 6 ft +

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0.2% Depth (500-Year)

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1.7 ft

8.9 ft

4.3 ft

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0 - 1 ft 1 - 2 ft 2 - 3 ft 3 - 6 ft 6 ft +

-

Percent Annual Chance of Flooding Grid (PctAnnual_Grd)

- Mase Dataset
 - Riverine
- Enhanced Datasets
 - Coastal and Levee







Percent Annual Chance of Flooding Grid







Percent Annual Chance of Flooding Grid

Display Options



Relative Flood Hazard within Floodplain

Floodplain Extents for Each Flood Frequency





Percent Chance of Flooding over a 30-Year Period Grid (Pct30yr_Grd)

• Mase Dataset

- Riverine
- Enhanced Datasets
 - Coastal and Levee







Water Surface Elevation Grids (WSEL_XXpct)

Enhanced Dataset

- All Riverine, Coastal, and Levee Flood Analyses
- Note:
 - Water Surface Elevation grids will be <u>created</u> for each flooding source studied during Risk MAP in order to produce many of the other grids
 - However, they will <u>not</u> be <u>delivered</u> as a base dataset so that they do not get misused as a regulatory product







WSE Change Grids (WSEL_Chng_Grd)

Enhanced Datasets

- All Riverine, Coastal, and Levee Analyses
- Displays the vertical change in Water Surface Elevation between the previous study and new study
- Requires that the previous study have published elevations (i.e. non-Zone A) or be backed by an available model





Annualized Depth Grid

Enhanced Dataset

- All Riverine, Coastal, and Levee Analyses
- Provides end users with estimated flood risk (expressed as a flood depth) during any given year at a particular location
- Composite grid derived from the individual flood depth grids created for each modeled frequency





Flood Velocity Grids (Vel_XXpct)

Enhanced Datasets

- All Riverine, Coastal, and Levee Analyses
- Can be generated for both 1-D (e.g. HEC-RAS, etc.) and 2-D (e.g. FLO-2D, etc.) models
- Velocity grid resolution (i.e. cell size) should be equal to that selected for the depth and other grids







Toe and Top of Levee Grids

Toe of levee grid

* Enhanced Dataset



Cross Section View



Plan (aerial) View





Toe and Top of Levee Grids

Top of levee grid

* Enhanced Dataset



Cross Section View



Plan (aerial) View





Content Scalability

■ Summary Table of Base (☑) vs. Enhanced (★) Grids

Grid(s)	Riverine	Coastal	Levee
Depth: 10%, 4%, 2%, 0.2% Annual Chance		*	*
Depth: 1% (100-yr) Annual Chance			V
Depth: Additional Flood Frequencies (e.g. 50%, 20%, 0.5%, 1% "plus", etc.)	*	*	*
Percent Annual Chance of Flooding		*	*
Percent Chance of Flooding over a 30-yr Period	V	*	*
Water Surface Elevation : 10%, 4%, 2%, 1%, 0.2%	*	*	*
Water Surface Elevation Change	*	*	*
Depth: Annualized	*	*	*
Velocity	*	*	*
Top & Toe of Levee	N/A	N/A	*

*

Note that the <u>delivery</u> of water surface elevation grids is an enhancement





Flood Depth & Analysis Grids Distribution Context



Ad-Hoc Flood Risk Analyses







Flood Risk Assessment Data





Purpose and Intended Uses

Identify Areas with Higher Relative Flood Risk:

- Floodprone Areas
- Vulnerable people and property

Provide Flood Risk \$:

- Potential damage severity for different flood frequencies
- Identify locations with possible cost effective mitigation options

Improve on Existing Flood Risk Estimates:

- What was determined during the 2010 Average Annualized Loss Study?
- What can be improved during a new flood study?





Flood Risk Assessment Datasets

Flood Risk Assessment Data

- 2010 HAZUS Average Annualized Loss (AAL) Study
- Refined HAZUS and Other Risk Analyses



HAZUS MH



Flood Risk Assessment



2010 AAL HAZUS Study

- 2010 HAZUS-MH Flood Average Annualized Loss Estimation (AAL) was performed for continental U.S. using MR4
- Inputs:
 - County-wide study regions
 - 30 meter DEM
 - Default Census data
- Final Output included
 - Total exposure
 - Average Annualized Loss
 - Annualized Loss Ratio






Refined HAZUS Analysis

• Overview:

- Depth Grids imported into HAZUS
 - Base: For new study areas
- HAZUS run for each return period and annualized
- HAZUS results exported and stored in Flood Risk Database







Estimation of Losses

Dollar Losses

- Residential Loss
- Commercial Loss
- Other Asset Loss

Percent Damage

- Evaluates Building Stock
- Structure and Content Considerations

Business Disruption

EMA

- Considers Total Occupancy Tables
- Considers Lost Income and Wages

























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Annualized Risk

\$26,000

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\$45 000



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Enhanced Risk Assessment Analyses

Enhancements could include:

- Risk Assessments at sitespecific locations
- Incorporation of locallyprovided inventory data (firstfloor elevations and/or parcel data)
- Additional sources of flood depth grids
- Supplemental HAZUS analyses or other types of analyses







Content Scalability

Base

- ✓ HAZUS analysis for reaches with new or updated studies where depth grids can be generated
- ✓ Should include 10%, 4%, 2%, 1%, and 0.2% annual chance events and Annualized Loss
- HAZUS GBS Losses (dollar losses, percent damage, business disruption)

Enhancements *

- Additional events
- Additional HAZUS loss calculations (infrastructure, critical facilities, userdefined facilities)
- Use of local data to updated/supplement HAZUS data
- Non-HAZUS analysis methods (needs to provide same base loss estimates)





Flood Risk Assessment Distribution Context



Ad-Hoc Flood Risk Analyses





Areas of Mitigation Interest (Enhanced)





Purpose and Intended Uses

- Creating public and community awareness of issues affecting flooding and risk
- Providing "food for thought" for communities to sharpen focus and research toward future plan updates and project development
- Identifying interrelationships between upstream/downstream community issues within a watershed
- Using existing areas of focus in mitigation plans to broaden awareness to new audiences
- Showing examples between communities and the public of what has worked in other areas to reduce damages
- Demonstrating that both existing physical hydraulic features (e.g. pinch points) and future development actions (e.g. significant proposed development) can have impacts and much different mitigation techniques
- Increasing public awareness of areas where actions can be taken to reduce risks





Overview - Areas of Mitigation Interest

Items that may have an impact (positive or negative) on the identified flood hazards and/or flood risks- Examples include:

- Community Identified "Hot Spots"
- Previous Claim Areas (e.g. clusters of claim, RL, SRL)
- Riverine and Coastal Flood Control Structures (e.g. dams, levees, coastal berms, etc)
- Floodplain "Pinch Points" (e.g. undersized culverts and bridge openings, etc.)
- Significant proposed and recent floodplain development
- Locations of successful mitigation projects



Visualization of Areas of Mitigation Interest



Sources of Data



Community Provided Data

- Interviews and survey from Discovery Meeting
- Mining of existing mitigation plans
- Engineering Data
 - Review of existing H&H models
 - Engineering data from other reports (e.g. USACE)
- Other Government Agency Data
 - Claims data (inc. RL, SRL, clusters, etc)
 - CNMS data
 - Flood control structures





Verification and Ownership

Data primarily provided by the communities in the study area

- Intention <u>is not</u> to commit or prove that areas of interest are contributing to flooding or risk
- Intention <u>is</u> to provide focus on areas that the communities and the government think are worthy of further research to determine mitigation potential
- FEMA will not claim ownership or guarantee accuracy of the data but will not use data that does not pass the "straight face" test





Mitigation Planning Linkages

There are several required areas for mitigation plans for which Areas or Mitigation Interest might be helpful:

Risk Assessment Product	Mitigation Planning Requirement
Areas of Interest	 ✓ 44 CFR Part 201(d)(3), revise plans to reflect changes ✓ 44 CFR Part 201.6(c)(2)(i), profiling hazards ✓ 44 CFR Part 201.6(c)(2), risk assessment ✓ 44 CFR Part 201.6(c)(3), developing mitigation strategies



Content Scalability

Base

Not currently included within Base

Enhancements *

- In FY 2010 Areas of Mitigation Interest is being offered as an enhancement only
- As the dataset is better defined it is anticipated that it will become a base product with enhancement options in future years





Areas of Mitigation Interest Distribution Context



Ad-Hoc Flood Risk Analyses







Flood Risk Products

- Flood Risk Database
- Flood Risk Report
- Flood Risk Map







Flood Risk Database





Flood Risk Database



Primary Storage Device for:

Flood Risk Data

Stores Data to Create:

- Flood Risk Report
- Flood Risk Map
- Delivered Digitally to Stakeholders:
 - CD Delivery







Flood Risk Database (red = enhanced)

Changes Since Last FIRM

- Horizontal Changes and Results
- Structure/Population counts impacted by change

Depth & Analysis Grids

- Depth (10, 04, 02, 01, 0.2 percent chance)
- Percent Annual Chance
- Percent 30-Year Grid
- Delivery of Water Surface Elevation (multi-freq)
- Water Surface Elevation Change Grid (multi-freq)
- Velocity Grids, Annualized Depth, Top and Toe of Levee
- Multi Freq Grids for Levee and Coastal Areas, etc.

Flood Risk Assessment

- Average Annualized Loss 2010
- Refined Flood Risk Assessment
- HAZUS or Non-HAZUS with improved data/assumptions

Areas of Mitigation Interest

Areas of Mitigation Opportunity or Awareness







Distribution Context



Ad-Hoc Flood Risk Analyses





Flood Risk Report





Flood Risk Report – Potential Uses

Increase General Flood Risk Awareness

- Risk Definitions and Causes
- Risk Reduction Techniques and Mitigation Practices

Deliver Community and Project Level Results

- Project Results Summarized by:
 - Communities
 - Watershed or Project Area

Provide Information to Augment or Enhance Other Efforts

- Local Hazard Mitigation Planning
- Local Emergency Management Planning
- Local Master Planning and Building Development





Flood Risk Report Distribution Context



Flood Risk Map





Ad-Hoc Flood Risk Analyses





Content Overview



Flood Risk Report

For project areas including: Watershed USA, Village of Coastland, Village of Drytown, City of Floodville, Town of Waterloo, County A*, County B*, and County C*

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Report Number 001

MM/DD/YYYY



Background:

- Purpose, Methods
- Risk Reduction Practices

Project Results

- Changes Since Last FIRM
- Depth & Analysis Grids
- Flood Risk Assessment
- (enhanced analyses)
 - e.g. Areas of Mitigation Interest

Summarized by Locations

Communities and Watersheds





Content – Details

Risk Awareness Information





Flood Risk Report

For project areas including: Watershed USA, Village of Coastland, Village of Drytown, City of Floodville, Town of Waterloo, County A*, County B*, and County C*

*Spans more than one watershed. This report covers only the area within the studied watershed.

Report Number 001

MM/DD/YYYY



RiskMAP





Content – Details

Community Summaries













Flood Risk Report

For project areas including: Watershed USA, Village of Coastland, Village of Drytown, City of Floodville, Town of Waterloo, County A*, County B*, and County C*

*Spans more than one waterahed. This report covers only the area within the studied waterahed.

Report Number 001

MM/DD/YYYY



Risk MAP





Content – Details

Watershed /Project Level Summary













Flood Risk Report

For project areas including: Watershed USA, Village of Coastland, Village of Drytown, City of Floodville, Town of Waterloo, County A*, County B*, and County C*

*Sparis more than one waterahed. This report covers only the area within the studied waterahed

Report Number 001

MM/DD/YYYY



RiskMAP



CSLF within the Flood Risk Report



Area of Interest	Total Area (mi ²)	Increase (mi ²)	Incr Population	Incr Buildings	Decrease (mi ²)	Decr Population	Decr Buildings
Area within SFHA	21.082	1.038	1,785	4,939	-2.556	-1,909	-647
Area within Floodway	3.2121	0.739	100	42	-0.1328	-17	-17
Area of Interest	Net Change (mi ²)	Net Population	Net Buildings				
Area within SFHA	-1.519	-124	4,291	Enhon	aad		
Area within Floodway	3.0793	83	25	Ennanced			





Content – Details and Scalability

Flood Risk Report Tables

Flood Risk Assessment (example)

Watershed USA's flood risk assessment incorporates results from recently performed HAZUS-MH Level 1 and 2 analyses taken from local hazard mitigation plans. FEMA updated these analyses to account for newly modeled areas throughout the watershed and more detailed building locations and values provided by the local governments. The highest areas of flood risk were concentrated in the City of Floodville as well as unincorporated portions of the watershed along Indian Creek. This area accounts for nearly 70% of the watershed's total estimated flood risk and should be evaluated for potential risk reduction activities

Bacant Chance	Total Asset Loss		Re	Residential Asset Loss		Commercial Asset Loss		Other Asset Loss			Rusinoss	
Event	Dollar Losses	Percent Damage	Units	Dollar Losses	Percent	Units	Dollar Losses	Percent Damage	Units	Dollar Losses	Percent Damage	Disruption
10% (10-yr)	\$15,212,203	4.55%	706	\$10,439,703	13.66%	42	\$3,112,500	1.55%	33	\$1,660,000	0.33%	\$760,610
4% (25-yr)	\$20,519,895	6.13%	913	\$11,804,895	15.44%	66	\$4,980,000	2.48%	75	\$3,735,000	0.75%	\$1,025,995
2% (50-yr)	\$25,191,613	7.53%	1,079	\$13,571,613	17.76%	83	\$6,225,000	3.10%	108	\$5,395,000	1.08%	\$1,259,581
1% (100-yr)	\$40,230,797	12.02%	1,992	\$19,273,297	25.22%	125	\$9,337,500	4.64%	232	\$11,620,000	2.33%	\$2,011,540
0.2% (500-yr)	\$81,480,216	24.35%	2,532	\$32,925,216	43.08%	415	\$31,125,000	15.48%	349	\$17,430,000	3.50%	\$4,074,011
Annualized (\$/yr)	\$365,269			\$176,029			\$109,560			\$79,680		\$18,263



Content – Details and Scalability

Areas of Mitigation Interest (enhanced example)

Areas of Mitigation Interest						
Factor	Data Source	Why a Contributing Factor	Possible Solutions			
Dams (small)	National Inventory of Dams (USACE)	Increases flooding upstream along their impoundment shorelines. In there is an extremely high number of dams	Engineering assessment/EAP (State Dam Safety Program); dam removal (NRCS)			
Non-Accredited Levee	National levee survey (USACE)					
Coastal Structures	NOAA National Shoreline Survey	"Hardening" of the shoreline interrupts the dynamic processes	Increase coastal setbacks for construction (State Coastal Zone Management Program)			
Creating Erosion	State Coastal Zone Management Programs' Beach Management Plans	of the littoral flow which results in accelerated coastal erosion. Structures include: jetties, groins, sea walls, breachways	Habitat restoration programs (USACE) Wetland restoration and mitigation banking			
Flow Pinch Point	State Stormwater Management Programs (per EPA 310 Program). community surveys from scoping	These refer to drainage structures such as road/bridge culverts and when undersized and have outlived their intended capacity can result in increased flood depths within the vicinity and in areas immediately upstream	Engineering Analysis, re-engineering and replacement of structures pre- and post-disaste (FEMA HMA Grants, 406 mitigation, capitol improvement planning)			
Undersized Culvert	State/Local Hazard Mitigation Plans Stormwater management plans, community surveys from scoping	These refer to drainage structures such as road/bridge culverts and when undersized and have outlived their intended capacity can result in increased flood depths within the vicinity and in areas immediately upstream	Engineering Analysis, re-engineering and replacement of structures pre- and post-disaste (FEMA HMA Grants, 406 mitigation, capitol improvement planning)			
Impervious Area Hot Spot	Stormwater Management Plan; Water Quality Management Plan (EPA; State DEMs/DNRs)	Increases the speed and geographical extent of flood discharges; increases speed of discharges may also increase flood depths in vicinity of discharges	Stormwater BMPs, green buildings and infrastructure, higher regulatory standards, stormwater management utility creation			
Past Claims Hot Spot	FEMA NEXTGEN database; NFIP State Coordinator	Past claims, Repetitive Loss and Severe Repetitive Loss structures are indications that the locations of structures are contributing to losses	Mitigate through acquisition, elevation, relocation, flood-proofing			
Proposed Development in	Community Comprehensive Plans	Increases impermeable surface areas; interrupts/alters drainage and results in more frequent flooding of properties in	Higher regulatory standards, Stormwater BMPs, Transfer of Development rights, compensatory			
SFHA	State Growth Management Plan	low frequency	storage and equal conveyance standards, etc.			



Points of Risk MAP Integration with Mitigation Planning

Mitigation Planning Component	Flow	Risk MAP Component
Risk Assessment	\longleftrightarrow	Watershed Flood Risk Report Flood Insurance Study (History)
Mitigation Strategy	<>	Watershed Flood Risk Report (Areas of Mitigation Interest) Discovery Meeting (Are there mitigation actions that identify mapping or risk assessment priorities?) Resilience Meeting (After Risk MAP process are there new mitigation actions?)
Planning Process	$\leftarrow \rightarrow$	Enhanced Stakeholder Group (Mitigation plan update group) Synchronize update or at least annual maintenance/monitoring Four Risk MAP meetings to reflect stakeholder input





Flood Risk Map




Flood Risk Map (accompanies and is a subset of the Flood Risk Report)



Flood Risk Report

For project areas including: Watershed USA, Village of Coastland, Village of Drytown, City of Floodville, Town of Waterloo, County A*, County B*, and County C*

*(periodrove that are essential. This report covers any the area within the journed essential

Report Number 001

MM/DD/YYYY



RISKIVIA





Flood Risk Map Distribution Context



Flood Risk Map

Flood Risk Report



Ad-Hoc Flood Risk Analyses





Flood Risk Map: Watershed USA



Visually Promotes Risk Awareness

- Contains results of Risk MAP project
 non-regulatory datasets
- Promotes additional flood risk data not shown but located within the Flood Risk Database



HTTP://MSC.FEMA.GOV



MAP SYMBOLOGY

FEMA



* Areas of Mitigation Interest Offered as Enhanced Product Only



A

WATERSHED LOCATOR

Community Level per Capita Losses





NON-REGULATED DAM STRUCTURE*









Flood Risk Products – Project Lifecycle Overview







Map Modernization and Risk MAP Project Timelines

Map Modernization

3 years

.

N

Risk MAP 3 - 5 years



Questions???





Floodproofing Non-Residential Structures

Rules, Regulations and Structural Considerations

Presenters:

Dan Knapp, P.E. Anthem, LLC <u>dknapp@anthemstructural.com</u>

Katie Knapp, P.E., CFM City of Boulder <u>knappk@bouldercolorado.gov</u>

Dawn Gladwell, P.E., CFM FEMA, Region VIII dawn.gladwell@dhs.gov

Outline

- Floodproofing Methods
- FEMA Requirements
- Structural Design
- Local Requirements
- Other Considerations

Floodproofing Methods

Wet Floodproofing

- Allow flood waters to enter and exit
- Equalize pressures
- Water resistant materials (TB-2)





Floodproofing Methods





- Substantially impervious to water
- Allowable leakage
 (4-inches in 24 hours)



FEMA Floodplain Management Publications

- <u>TB-1 Openings in Foundation Walls</u>
- <u>TB-2 Flood Damage-Resistant Materials Requirements</u>
- <u>TB-3 Non-Residential Floodproofing -- Requirements and Certification</u>
- <u>TB-4 Elevator Installation</u>
- <u>TB-5 Free-of-Obstruction Requirements</u>
- <u>TB-6 Below-Grade Parking requirements</u>
- <u>TB-7 Wet floodproofing Requirements</u>
- FEMA 102 Floodproofing for Non-Residential Structures
- Army Corps of Engineers EP1165-2-314 Flood Proofing Regulations



Openings in Foundation Walls and Walls of Enclosures

Below Elevated Buildings in Special Flood Hazard Areas in accordance with the National Flood Insurance Program

Technical Bulletin 1 / August 2008



Technical Bulletin 1 Flood Vents – Wet Floodproofing



Flood Damage-Resistant Materials Requirements

for Buildings Located in Special Flood Hazard Areas in accordance with the National Flood Insurance Program

Technical Bulletin 2 / August 2008



Technical Bulletin 2 Flood Resistant Materials



FIA-TB-3

493

Non-Residential Floodproofing — Requirements and Certification for Buildings Located in Special Flood Hazard Areas in accordance with the National Flood Insurance Program





DOM DRIVEN MANAGEMENT AGENT

Technical Bulletin 3 Non-Residential Floodproofing



4/93

Elevator Installation for Buildings Located in Special Flood Hazard Areas in accordance with the National Flood Insurance Program



Technical Bulletin 4 Elevator Installation



Technical Bulletin 5 Free-of-Obstruction

Free-of-Obstruction Requirements

for Buildings Located in Coastal High Hazard Areas in accordance with the National Flood Insurance Program

Technical Bulletin 5 / August 2008





Below-Grade Parking Requirements for Buildings Located in Special Flood Hazard Areas in accordance with the National Flood Insurance Program





FEDERAL ENERGINE'S MANAGEMENT ADACS FEDERAL INVESTIGATION FLA-TB-6 491

Technical Bulletin 6 Below Grade Parking



Wet Floodproofing Requirements for Structures Located in Special Flood Hazard Areas in accordance with the National Flood Insurance Program

Technical Bulletin 7 Wet Floodproofing





FEDERAL EMERGENCY MANAGEMENT AGENCY MITHEATTON DIRECTORATE FEDERAL INDURANCE ADMINISTRATION FIA-TB-7 12/93

FEMA Resource





Federal Emergency Management Agency

FEMA 102 Floodproofing Non-Residential Structures

Army Corps of Engineers



EP165-2-314 15 Dec 1995

EP1165-2-314 Flood Proofing Regulations





Flood Proofing Regulations





US Army Corps of Engineers

Structural Considerations

- Design loads (FIA-TB-3)
- Load Path
- Flood Damage-Resistant Materials (FIA-TB-2)
- Glazing and Storefront Anchorage
- Flood Gates

Design Loads (FIA-TB-3)

- Hydrostatic Loading
 - Buoyant Forces
 - Lateral Forces
- Hydrodynamic Loading
- Impact Loading
- Special Impact Loading



Figure 1. Hydrostatic Pressure Diagram

Resultant Force Due to Hydrostatic Pressure from Free-Standing Water:

 $F_h = 1/2wH^2$

Where:

F_h = Lateral Force from Free-Standing Water (plf)
w = Specific Weight of Water (62.4 pcf)
H = Height of Standing Water to Flood Protection Elevation (Ft)

Resultant Force Due to Hydrostatic Pressure from Saturated Soil:

 $F_{sat} = 1/2SD^2 + F_h$

Where:

- F_{sat} = Lateral Force from Saturated Soil (plf)
- F_h = Lateral Force from Free-Standing Water (plf)
- S = Equivalent Fluid Weight of Saturated Soil (pcf)
- D = Depth of Saturated Soil (Ft)

Buoyancy Force

 $F_{b} = WAH$

Where:
Fb = Force Due to Buoyancy
w = Specific Weight of Water (62.4 pcf)
A = Area of Horizontal Surface Being Acted Upon (sf)
H = Depth of Floor Below Flood Protection Elevation (ft)

Hydrodynamic Loading

Hydrodynamic Force

$F_{d} = C_{d}(1/2)mV^{2}A$

Where: F_d = Hydrodynamic Force (pounds) C_d = Drag Coefficient m = Mass Density of Water (1.94 slugs per cubic foot) V = Velocity of Water (feet per second) A = Area of Wall (sf)

Debris Impact Loading

Debris Impact Force

Fi = WV/(gt)

Where:
Fi = Debris Impact Force (pounds)
W = Weight of Object (pounds) – Generally 1000#, but may be reduced to 500#.
V= Velocity of Water (feet per second)
g = Acceleration Due to Gravity (32.2 ft/s²)
t = Duration of Impact (seconds) – 1 second

Special Impact Loading

Special Impact Force

 $F_s = w_s V/(gt)$

Where: F_s = Special Impact Force (pounds) w_s = Weight of Object (100 plf x width of structure) V= Velocity of Water (feet per second) g = Acceleration Due to Gravity (32.2 ft/s²) t = Duration of Impact (seconds) – 1 second

Load Path

- Building Veneer
- Glazing & Storefront
- Flood Gates
- Floor System

Building Veneer

- Flood Damage-Resistant Materials (FIA-TB-2) Table 2, Structural Materials
- Class 4 & 5 are the only acceptable materials
- Includes:
 - Brick
 - Concrete Block (CMU)
 - Cast Stone
 - Concrete
 - Others

Building Veneer

- Veneer Back-up Structure
 - Veneer ties must be capable of resisting flood loads
 - Metal/Wood Studs
 - Reinforced and Unreinforced Masonry
 - Reinforced Concrete
Glazing & Storefront

- Glass Thickness & Temper
 Pressure Tables
- Mullions
 - Heavy Duty
- Connections

Adequate for High-Magnitude Reactions

Glazing Design



ASTM E-1300

Heavy-Duty Mullions





BT835 / BT804 / SS057 Mullion, Filler and Steel (Combined) lxx = 19.100 (794.98 x 10⁴) Sxx = 7.527 (123.52 x 10³)

- Flood Protection Elevation
- Manual versus Automatic
- Maximum Depth for Floodproofing
- Enclosure Limits
- Floodproofing Prohibition

Flood Protection Elevation



Flood Protection Elevation Base Flood Elevation



Manually Installed

Automatic



Higher Regulatory Standards

- Enclosure Limits
- Floodproofing Prohibition

 Elevate/Floodproof Mechanical and Electrical Components



Emergency Response Plan – Evacuation – Shelter in-Place



FACT The city of Boulder is the #I flash flood risk in the state of Colorado. Be prepared.

IT IS CRITICAL TO BE PREPARED FOR A FLOOD.

Even though you think such an event is unlikely to happen, it can't This flood action plan can help you prepare for this natural dimester.

Review Your Family Plan, Review the information to everyone it ignitar with the plan in the event of a food

Character an Envergency Family Contact, Ali an out offician hard or relative to be your contact. After a food, family manifest should call the perior to communicate your location and key information.

Designate Heating Flaces. In the event of a fload, you may become sequented from lawly members and out have phone or communication pairwise. Division a pleas right statistic your home in same of a satility envergency. Division is location custolic your home in same of a satility cannot return tome.

Garry Your Family Contact Information. Tour plin should include const information for family members, both at work and at allock Tour plan should also include information for your imaginary contact, membrg location and emergency services.

Suck High Ground Internalizable. Tou may need to exocute on a redenent's notice however, high ground could be the top floor. Be save everyone is aware of sub-routes and sele places.

When You Hear The Siren - When an emergency wanning is used by sines, radio or other media, tank your radio to 850 AM or TV to "Durnel 8 or local news.

IMPORTANT PHONE NUMBERS EMERGENCY RESPONSE

Hules, Fee, Andersen cal 944
Polian Cartheli 1000-222-022
Not emergency Dispatch: 300-448 5533
Fandy Doctor ______
Phone # ______
EMERGENCY CONTACTS
Name ______
Hume Address ______
Hume Address ______
Fandy Cat Phone #'s ______
Foundy Cat Phone # ______
Emergency Contact Phone # ______
Emergency Contact Phone # ______
Control Phone Mailing Phase ______
Cutside Naufploorbood Meeting Phase ______
Cutside Naufploorbood Meeting Phase ______

WWW.BOILDERFLOODINFO.NET

• Signage



This building is subject to flooding due to its proximity to Boulder Creek. In a flood event, the combination of depth and speed of flood water will be life threatening.

If you become aware of probable flooding, leave the area as quickly as possible and go south (across Arapahoe) to the University Hill Area.

Never attempt to walk or drive across a bridge during a flood event.

- Maintenance
- Critical Facilities
- Flood Insurance Costs
- Groundwater Impacts

Questions?



eLOMA – Changing the Face of the Map Amendment Process

Ryan Carroll, CFM Michael Baker Jr., Inc.

CASFM September 2010





What is eLOMA and who can use it?



eLOMA is a MIP application designed to provide licensed land surveyors and professional engineers (Licensed **Professionals or LPs**) with a web-based system to submit and print simple LOMA requests

Baker



What are the benefits of eLOMA?



 The eLOMA tool is designed to allow users to receive a determination from FEMA in minutes. The user can print a copy almost instantly.

Baker

- Electronic transfer of data
- Less mailing and printing uses less paper





When can't eLOMA be used?



Current Limitations

AE, A1-A30, AH)

No floodways

No multi-lot requests or portions of properties

No approximate study areas (Zones A, V, AO, or D)

No previous LOMA/eLOMA determinations for same property

Baker How do users gain access to eLOMA?



Surveyor or engineer must set up an account through MIP Help using individual certification information to become an eLOMA LP

The LP logs into the MIP to access eLOMA and has the option to:

Create a new application

Resume a previously saved application

Baker What data is required for eLOMA?



- User will enter all applicable data:
 - Legal property description
 - Requester information
 - Community information (CID number, etc...)
 - Map panel information
 - Latitude and longitude coordinates
 - Elevation information (LAG or LLE)
 - Subject information
 - BFE (calculated using FIS text/profile)





Baker How does eLOMA make a determination?



 eLOMA will compare the submitted BFE to the submitted Lowest Adjacent Grade (LAG) or Low Lot Elevation (LLE)



 eLOMA will ensure all required information has been entered

Baker How do the audits work?



- Audit procedures ensure accuracy.
- The LP <u>must</u> submit supporting data to FEMA.
- If APPROVED, the LP will receive an email notification to log in and print the determination.
- If REJECTED, the LOMA request will be completed by FEMA and the LP will be audited again on the next submittal.
- After an initial successful audit, the LP can generate determinations online. However, he or she will still be subject to random audits.



Baker What errors do the eLOMA auditors find?



- Legal property descriptions that need to be revised
- Subject elevations not converted to the datum used on the FIRM and in the FIS report
- Inaccurate latitude/longitude
- Lot, block, and subdivision information
- FIRM panel numbers
- Flooding sources

How much is eLOMA being used? Baker FEMA Currently, More More than than 2,500 6,300 **eLOMAs** eLOMA LPs Submitted to Registered Date Nationwide More than About 40% of 5,400 eLOMA LOMA Requests Determination Meet the Letters Issued Current eLOMA to Date Criteria 11

Baker Plans to expand eLOMA usage



Additional Types of LOMA Requests

- Multiple-lot requests
- Zone A requests
- LOMR-Fs
- Inadvertent Inclusions in the Floodway
- Annexations
- Out As Shown determinations
- Reissuances of previous LOMAs/eLOMAs

Baker Proposed eLOMA enhancements



Improved /Additional Functionality

- Create an eLOMA workflow to improve tracking and support additional LOMC types
- Upload feature to improve the audit process
- Additional data quality checks and validation
- Improved web based training materials



Baker How might eLOMA affect Floodplain Managers?

- Floodplain Managers have expressed concern that eLOMAs containing errors could be issued in their community without an audit.
 - All non-audited eLOMA determination letters are reviewed for noticeable errors.
 - Incorrect eLOMAs can be rescinded by FEMA and superseded by a standard LOMA.
 - Errors are often caught before the LP has disseminated the final determination letter.
 - To date, only two eLOMAs have warranted a correction LOMA.



Baker What is the future of eLOMA?



The plan is to...

- Increase usage by allowing more requests to be processed using eLOMA
- Improve the eLOMA process to make it easier for LPs to issue fast and accurate determinations
- Save more time and resources for property owners, eLOMA users, and FEMA
- Ultimately provide faster determinations for property owners in your community

Baker Contacts and Links



- MIP www.hazards.fema.gov
- FEMA www.fema.gov
- MIP Help miphelp@riskmapcds.com
- BakerAECOM eLOMA Coordinator (FEMA Regions 4, 8, and 9) – DMummert@mbakercorp.com

Questions and Answers



The NFIP

How Its History Affects You: The Morphology of the National Flood Insurance Program

Paul C. Currier, P.E., CFM

CASFM Conference, Sept. 23, 2010

"You can know nothing until you know its history" Dr. Elroy Shikles

- Where did the NFIP come from?
- What purpose was it intended to serve?
- How good are we at implementing it?
- How can we improve?

The Setting

- 1920's
 - Insurance industry was in its infancy
 - Decided flood insurance wasn't profitable
- 1930's 1950's
 - Public works era
 - Hard controls
 - Multitude of Congressional directives
 - Flood damage continued at great expense

The Last Straw

- 1960's: Too many "big" floods
 - Michigan
 - California
 - Denver
 - Others



Photo Courtesy of DCL

Congress Steps In

- 1968 National Flood Insurance Act
 - Transfer costs to occupants of flood prone areas
 - Create a modicum of financial resilience via Federally backed insurance
 - Guide development and re-development within flood prone areas

But Did it Work?

- People didn't buy the insurance
- People still lived, worked and built in flood prone areas
- You decide: did it work?
Corrective Action

- A good hurricane (Agnes, 1973)
- Severe rainfall along the eastern seaboard
- "Most" expensive storm in U.S. history until that point
- Congress inquired as to why their Federal Insurance program wasn't popular.
- And....

... Took Social Action

- Flood Disaster Protection Act (1973)
 - Flood insurance now mandatory if you want a property loan that's backed by the Feds.
- Result: by 1980 nearly 2,000,000 policies vs only 100,000 in 1973
- Self supporting by 1986

But did it stop floods?

State Street, Salt Lake City City Creek flood - 1983



Opryland - 2010



So how is it that we are still getting flooded?

Why the "100 year" recurrence interval standard?

More correctly, why p=0.01 ?

One word...

\$\$\$\$\$

The NFIP is not:

A flood <u>prediction</u> program

Nor a flood protection program

The NFIP is:

- A fiduciary management tool intended to create financial resilience:
 - -On a National scale
 - Paid for by the users / beneficiaries
- It has ancillary benefits of reducing loss of life and property

So is p=0.01 arbitrary?

- Yes?
- No?
- If applied for reasons outside of its scope, its extremely arbitrary

What about other NFIP ideas?

- BFE?
- Floodway?
- No debris blockage?

Project "Creep" Happens

- Same is true with the NFIP
- Example: ASFM brainstorming on floodplain success
 - Disaster resilient communities
 - Room is provided for rivers and floodplains to function naturally
 - Human occupance in all high risk flood zones has been abandoned
 - The principle of individual responsibility is reflected in public policy.

Project Creep in the NFIP

- Trends of "ab"using it as a:
 - Poorly thought out ecological tool
 - Land use development tool
 - An attitude of "preservation" vs."stewardship"
 - Good Stewardship = wise use
 - Preservation = avoidance



National Flood Insurance Program Flood Insurance Manual

May 2008 Revised October 2008 Revised May 2009 Revised October 2009 Revised May 2010 Revised October 2010



NFIP Insurance - 2010

I. AMOUNT OF INSURANCE AVAILABLE

		REGULAR PROGRAM		
BUILDING COVERAGE	EMERGENCY PROGRAM	Basic Insurance Limits	Additional Insurance Limits	Total Insurance Limits
Single Family Dwelling 2-4 Family Dwelling Other Residential Non- Residential	\$ 35,000 * \$ 35,000 * \$100,000** \$100,000**	\$ 60,000 \$ 60,000 \$175,000 \$175,000	\$190,000 \$190,000 \$ 75,000 \$325,000	\$250,000 \$250,000 \$250,000 \$500,000
CONTENTS COVERAGE				
Residential Non-Residential	\$ 10,000 \$100,000	\$25,000 \$150,000	\$ 75,000 \$350,000	\$100,000 \$500,000

* In Alaska, Guam, Hawaii, and U.S. Virgin Islands, the amount available is \$50,000.

** In Alaska, Guam, Hawaii, and U.S. Virgin Islands, the amount available is \$150,000.

NOTE: For RCBAP, refer to CONDO Section for basic insurance limits and maximum coverage available.

Back to Flood Resilience

- Do we have a flooding issue?
- Or do we have an Insurance issue?

Take Home Thoughts

- As a planner, consultant, regulator, have I been tempted to read more into floodplain regulations than I should?
- If we view ourselves as working for the good of the public, should we be asking different questions?
- Is the NFIP the only solution to floodplain management?



The Cherry Creek Flood, Denver 1864, Photo by George D. Wakely.

The Triple Bottom Line (TBL) of Sustainable Floodplain Management



Brian Varrella, P.E., CFM Floodplain Administrator Fort Collins Utilities 970-416-2217 office bvarrella@fcgov.com

The Triple Bottom Line (TBL) of Sustainable Floodplain Management

National Trends in Sustainable Floodplain Management





National Trends in Sustainable Floodplain Management Past practices are not working long-term

- Conventional Approach to floodplain regulation
 - Control the river to protect public from harm
 - Convey floodwaters through town
 - Minimize flooded area during storms
 - Maximize developable land
- Baseline principle -- human intervention over nature



Human Intervention Over Nature







Human Impacts



Habitat Loss



Wildlife Conflicts

Water Pollution

National Trends in Sustainable Floodplain Management

Increasingly substantial evidence suggests that the present approach to managing flood threats in the United States is not sustainable with respect to <u>public</u> <u>safety</u> and <u>economic</u> and <u>environmental</u> consequences. -- Darryl W. Davis, US Army Corps of Engineers retired (2007)



National Trends in Sustainable Floodplain Management

New trends in thought are sweeping the nation

- National desire for long-term public safety solutions
- Recognizing flood losses are increasing
 - The NFIP is not working as intended
- States are increasing minimum FPM standards
- No Adverse Impact (NAI) is making sense
 - Encouraging tools that fit community values
 - Meeting community needs at the local level



National Trends in Sustainable Floodplain Management

No adverse impact principles [can] be applied in all land use and development decision making. The standard of "not causing harm". . . will result in the protection of people, property, and <u>natural resources</u> and functions **now and into the future**.

-- ASFPM (2007, emphasis added), FPM 2050, Pg. 33



The Triple Bottom Line (TBL) of Sustainable Floodplain Management

Enter The Triple Bottom Line (TBL);

An Introduction







• Basic Principles:

- Sustainability development that meets the needs of the present without compromising the ability of future generations to meet their own needs. -- Brundtland Commission, 1987
- Triple Bottom Line practices that optimize
 economic, environmental, and social considerations
 for sustainable outcomes.



Why a 3-fold bottom line?

- How do we give the environment equal consideration with public safety?
 - Utilities Management, 2008
- How do we factor political will into a decision?
 - City Mgr.'s Office official, 2010
- How do we make public safety a community indicator?
 - Plan Fort Collins vision team, 2010



Triple Bottom Line = Common Sense

- TBL is a method of framing decisions
- Allows one person to understand many perspectives on an issue or a decision
 - Reveals gaps in thinking
 - Removes personal bias
- Not unlike what you are doing right now



Enter the TBL; An Introduction THIS IS NOT A REVOLUTION Just a new way of describing different perceptions



The Triple Bottom Line (TBL) of Sustainable Floodplain Management

The Triple Bottom Line Analysis Map (TBLAM)





TBLAM (front page)

Project or Decision: Text Text		Evaluated by: name	Ut liber
Social WorkForce / Flex Column Community		Environmental	Economic
		Environmentar	Economic
STRENGTHS: Capacity Job Creation Increase Morale/ Performance In-House Expertise	STRENGTHS: • Engages • Better Service • Health Benefits • Awareness • Aesthetics • Safety • Economic Benefit	STRENGTHS: Minimizes adverse impact increases efficient use of natural assets Maximizes life cycle to minimize resource impacts Meets, exceeds, or improves regulatory compliance	 STRENGTHS: Offers a positive Return on Investment (ROI) Life Cycle Cost Analysis supports continued financial health of the organization Local businesses or residents benefit from the project
LIMITATIONS: Budget Lack Of Support/ Resistance Insufficient Staff Lack Of Capacity Lack Of Measures/ Material/ Space Cost Of Staffing Poor Management	LIMITATIONS: • Lack Of Support • Burdens • Conflicting Interests • Detrimental • Costly • Opposition • Short Term Benefit/ Long-Term Harm • Disruptive	LIMITATIONS: • Budget • Lack Of Support / Resistance • Cost of Staff / Lack Of Capacity • Lack Of Measures / Material / Space • Poor Management • Trade-Off Of Benefits (Helps In One Way, Hurts In Another) • Regulatory Concerns • Lack Of Technology	LIMITATIONS: Increased collateral costs associated with project Project-related opportunity costs Local businesses or residents are adversely impacted by costs
OPPORTUNITIES: • Future Staff Increase • Professional Development • Diversified Staff • Leadership	OPPORTUNITIES: • Education • Follows Trend • Long-Term Benefit • Improved Economic Potential	OPPORTUNITIES: Provides opportunity to demonstrate innovation and leadership Provides opportunity to develop new metrics to measure success (Research Opportunities)	OPPORTUNITIES: Project offers chance for job creation Project attracts businesses to the area Project encourages others to join in or follow example
THREATS: Loss Of Revenue Budget / RiFs Heath Attrition Economy Backlash Institutional Memory	THREATS: • Special Interests • Backlash • Political	THREATS: • Loss Of Revenue • Health • Institutional Memory • Political Opposition • Resource Allocation Constraints (staff / time, funding, etc.)	THREATS: • Loss of business or revenues • Political backlash • Competes with existing businesses •

This is a brainstorming tool

- The methodology can be applied to *any* decision
- Requires non-quantifiable input
- Flexible (made to be creative)
- Best input falls into multiple cells
- No wrong answers, and no weighting
 - All input is relevant
 - All input is equally-valuable



TBLAM (back page)

NOTES:

S.L.O.T. analysis is a strategic planning and analysis method used to break a situation, project, or business opportunity down into and analyze the internal and external factors that will positively and negatively affect the objective under study. In this analysis, the Strengths, Limitations, Opportunities, and Threats are identified and captured on a chart to offer a more detailed view of the interaction of the positive and negative aspects of the objective under review. Below are some typical examples of the kinds of issues that might figure into each of the categories in a S.L.O.T analysis:

Strengths: (more tangible)

- Advantages improvement/ efficiency gain
- Available Resources
 - staff, funding, \$\$, qualifications, internal/external support, technology, location, product, BMP's
- Measurable

Limitations:

- Lack of resources staffing, \$\$, qualifications
- No or limited gain in efficiency
- Lack of metrics (not measurable)
- Trends

Opportunities: [less tangible (potential strengths)]

- Increased possibilities (ROI, increased education, performance)
- · Help accomplish goal or objective
- Industry or lifestyle trend
- · Long term benefit

Threats:

- Uncontrolled variables
 - o (out of sphere of control/ influence) weather, nature, economy, society, political
- Major barriers policies, laws, regulations, biological/ viral
- Fatal Flaw

Revision Date: April 2010

This form is based on research by the City of Olympia and Evergreen State College

- SLOT analysis by **rows (4)**
 - Strengths = tangible benefit (today)
 - Limitations = tangible detriment (today)
 - Opportunity = potential benefit (future)
 - Threats = potential detriment (future)
- TBL by columns (4)
 - Social
 - Environmental
 - Economic
 - Flex column




The Triple Bottom Line (TBL) of Sustainable Floodplain Management

Top 10 Best Practices & Myth-Busting





TBL Best Practices & Myth-Busting Top 10 Best Practices (Slide 1 of 4)

- 1. NO FATAL FLAWS
 - Find one? -- re-evaluate your goals
 - No project, policy, or decision may have a fatal flaw and move forward

2. Always use TBL before a decision is made, not after

- If applied at the beginning, you will get a TBL product
- If applied as a polish at the end, your product will NOT shine



ollins

TBL Best Practices & Myth-Busting Top 10 Best Practices (Slide 2 of 4)

- 3. Thou shalt not steal
 - Do not borrow from one column to feed the others
- 4. Do not attempt to quantify
 - This is not a spreadsheet
 - Intrinsic benefits cannot be attached to \$\$\$
- 5. Support your TBLAM with real data
 - Attach memo, photos, web links, etc.
 - Attach spreadsheets, B/C calcs, graphs, etc.



TBL Best Practices & Myth-Busting Top 10 Best Practices (Slide 3 of 4)

6. Do not confuse **costs** with **detriments**

- Cost is economics only
- Limitations = current detriments
- Threats = perceived future detriments
- 7. Air your dirty laundry too
 - Full disclosure, especially to the public (SDIC)
- 8. No greenwashing



TBL Best Practices & Myth-Busting Top 10 Best Practices (Slide 4 of 4)

9. No drama

- Some ideas should be placed in multiple columns
- Some benefits create detriments (and vice versa)

10. Never TBLAM alone

- Group decisions require group input
- No outside input = biased data



TBL Best Practices & Myth-Busting

Myth-Busting the Triple Bottom Line

- This is just a green movement
- TBL analysis is difficult to do
- TBL analysis requires lots of paperwork
 - How green is that?? Honestly . . .
- This is a top-down order
 - Policy flavor of the month
 - This too shall pass
- The City is using TBL to finance economically irresponsible projects



TBL Best Practices & Myth-Busting

The [Plan FC environmental vision] statement identifies and rationalizes triple bottom line objectives though appears to suggest environmental and social objectives can be achieved in the absence of economically sustainable practices. -- Actual Plan FC public input, July 6, 2010

FALSE



The Triple Bottom Line (TBL) of Sustainable Floodplain Management

TBL Pitfalls and Fine Print





TBL Pitfalls and Fine Print TBL challenges – the fine print (1 of 2):

- TBL thinking requires difficult decisions to be made
 - Economy, society, and environment are all given equal consideration in decision-making
- Requires a long-term focus with short-term sacrifices
 - Good business decisions today may create safety hazards and financial burdens tomorrow
 - Sustainable = good today, good tomorrow



TBL Pitfalls and Fine Print TBL challenges – the fine print (2 of 2):

- Some decisions require buy-in from other departments
- Money is tight, and cash is still king
 - Changing the benefit-cost analysis mindset is tough
 - Everyone wants to boil it down to \$\$\$
- TBLAM format may not be compatible with the public or with decision-makers
- Alignment with community values is ever-changing
 - Every community has unique needs



TBL Pitfalls and Fine Print Will TBL survive?

- It must our own existence depends on it
- Becoming a worldwide business movement
- Written into the FC Utilities mission statement
- Ingrained in City staff culture
 - Gaining grass-roots support
 - Largely at the office staff level





July 8, 2010 Sustainable construction

VIDEO: Green building critical in triple bottom line accounting

Building design and construction standards will undergo significant changes as "triple bottom line" accounting becomes more commonplace in the industry, a Saskatchewan-based economist says.

In addition to just financial performance, the triple bettom line takes into account social and environmental impacts – or, people, planet and prefit.

Making Balanced Decisions

"These form the three pillars for the sustainability of the economy," economist Grah the Construction Specifications Canada conference in Saskatoon recently.

'Life cycle analysis is central to triple bottom line accounting," he noted.

'Increasingly the public looks towards environmental accounts to start to understan And with that information they move billions of dollars in the consumer marketplace corporate marketplace, which also has to comply with an increasing amount of legis



Making Balanced Decisions

We use the <u>Sustainable Action Map (SAM)</u> as a decision-making guide to ensure we are in alignment with Council's goal of community livability and the Public Works' vision of "balance and harmony between people and nature."

SAM is a simple, easy to use, one page worksheet that is a way for us to optimize a solution, rather than compromise one. The fundamentals of sustainability center on creating solutions that provide balance. Balance includes delivering the level of service citizens expect; doing it in an environmentally and socially responsible way; and insuring the best economic choice for the long term.

SAM has three key dimensions that work together:

- NICE: There are four key components of sustainability · Natural, Individual, Community, and Economy. All four of these components must be in balance to achieve a sustainable solution.
- SWOT: Strengths, Weaknesses, Opportunities, and Threats are described for each action (policy/decision) being considered and factored into the final decision.
- Green, Yellow, Red Stoplight: This system provides an indicator for how well a particular action achieves the individual components (NICE) of sustainability.
 - Green: The action provides value to that component (more strengths and opportunities).
 - Yellow: There are risks, but they are manageable.
 - Red: There may be a fatal flaw (many weaknesses and threats). You should consider innovative solutions to overcome these risks before moving forward.



Triple Bottom Line Reporting of Sustainable Water Utility Performance



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TBL Pitfalls and Fine Print

Free TBL Resources

- This presentation
- TBL Staff at Fort Collins Utilities (970-221-6700)
- TBLAM document
- The Triple Bottom Line by Andrew W. Savitz (2006)
- Fort Collins wiki site (coming in 2010/2011)
- Fort Collins publication (coming in 2011/2012)



ALBUQUERQUE WEST LEVEE LOMR: BENEFITS AND CHALLENGES USING

FLO-2D

25

Google



AUTHORS

Chad Morris, P.E., CFM



Dai Thomas, P.E.

Jerry Lovato, P.E.





Albuquerque Metropolitan Arroyo Flood Control Authority





Albuquerque West Levee





BACKGROUND / HISTORY

2003

November 19, 2003 Effective FIS:

West overbank area protected by the Albuquerque West Levee from the 1% annual chance flood (100-year event).



BACKGROUND / HISTORY

• **2006**

- USACE completes study to determine certification status of certain levees within the Albuquerque District.
- Study concludes that the Albuquerque West Levee, which is basically a spoil embankment levee, can not be certified.

• **2007**

 FEMA develops plan to conduct restudy of Bernalillo County as part of Map Modernization Program.



BACKGROUND / HISTORY

- **2008**
 - FEMA completes county-wide restudy.

Key Points of 2008 FIS

- No changes to hydrologic analysis.*
- Steady-state hydraulic analysis.
- West overbank modeled as separate flow path, using lateral structures to represent an assumed failure at the upstream end of the levee.
- * Revised hydrology developed by USACE in 2006





BACKGROUND / HISTORY

2008

September 26, 2008 Effective FIS

- West overbank no longer protected from the 1% annual chance flood by the Albuquerque West Levee.
- Approximately 2,550 acres of land in the Southwest Valley were placed inside the regulatory floodplain.



BACKGROUND / HISTORY

- **2008**
 - Plan devised to construct engineered replacement levee.
 - Estimated Completion Date: Fall 2009

Can anything be done in the meantime?

- Revised hydrologic analysis?
- Revised hydraulic modeling approach?





REVISED HYDROLOGY

2006

- USACE revises Rio Grande flood hydrology
- Regulated vs.
 Unregulated Flows
- Snowmelt Runoff vs.
 Local Rainfall Runoff





REVISED HYDROLOGY

Unregulated Rainfall Runoff greater than Regulated Snowmelt Runoff



HYDROLOGY RESULTS

Annual Chance Flood (percent)	Recurrence Interval (years)	Effective FIS (cfs)	Revised (cfs)
10	10	7,100	8,180
2	50	14,700	10,790
1	100	21,700	13,170
0.2	500	41,000	21,330





Hydraulic Model

• FLO-2D

- 2-dimensional
- Unsteady flow

Model Development

- Initially developed along entire Middle Rio Grande (180 miles)
- Developed for USACE
- Model Grid
 - 250' x 250'
 - 167,000 grid elements



Simulation Reach

- Shorter Simulation
 Time
- Hydrologic Boundary Condition
- 21 miles long
- 27,000 grid elements



Project Reach

- Levee Removed
- 6,100 grid elements





Hydraulic Results

100-year Event





Floodplain Reduction

- Regulatory Floodplain area reduced from 2,550 acres to 1,292 acres.
- 50% Reduction.
- Significant impact on flood insurance costs.



Benefits

- Improved hydraulic results based on limitedduration hydrographs.
 - Need to understand your hydrology
 - May not be applicable for long-duration snowmelt runoff events
- Provides ability to reduce extent of floodplain boundaries without physical changes to the project area.



Challenges

- Coordination with FEMA
 - FEMA representatives are generally not as familiar with this model format.
 - May require more explanation in LOMR application.
 - Accepted techniques may be dependent on the opinion of the specific reviewer or reviewing agency!



Challenges

- Output Format: Cross Sections vs. Grid
 Elements
 - Mapping, profiles, and tables
- Base Flood Elevations
 Contour delineation



Challenges

- Output Format: Cross Sections vs. Grid Elements
 - Mapping, profiles, and tables
- Base Flood Elevations
 Contour delineation
- Floodplain Boundary Delineation

 Compatibility with model elements

...Reminder: accepted techniques may be very dependent on the opinion of the specific reviewer or reviewing agency!



QUESTIONS?

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TETRA TECH Google

Tł

Southwest Valley

Pan American Fwy












































Predictions for Various Sub-area Discretized Models

The test square watershed has a total area of 300 acres on a slope of 2.0% and imperviousness of 40%. Four cases were developed for testing. They are: Case 1. The watershed is divided into 6 <u>sub areas of 50 acres</u> Case 2. The watershed is divided into 3 <u>sub areas of 100 acres</u> Case 3. The watershed is divided into <u>2 subareas: 200- and 100-acre</u> Case 4. The watershed is modeled as <u>a 300-acre single tributary area</u> All sub-areas are modeled as a square with a diagonal waterway on a 2.0% slope. Between sub-areas, the channel was defaulted to be a 5-ft trapezoidal channel of 500-ft in length.

Cases	CUHP2005-now Q in cfs	CUHP2005-revised Q in cfs	Comments
Six Areas of 50 acres	947	761	six small basins
Three Areas of 100 acres	885	763	a small + a large basin
Two Areas of 200 and 100 acres	833	793	mixed sizes
Single Area of 300 acres	718	718	a large basin

Cheers !



















							r		-						
Land	BMP	R	D	TA	IA	PA	DICA	SPA		Cascading	Plane				
Use	Level			total	Imp	Perv	area	area	Upper	Lower	Areal			Effective	Site
Imp				Area	Area	Area			UIA	RPA	Imp	f/i	PARF	Imp	Imp
IA%					IA%*TA	TA-IA	D*IA	(1-R)*PA	area	area	Ia%	ratio		Ie%	IE%
(<1.0)				acres	acres	acres	acres	acres	acres	acres	(<1.0)			(<1.0)	(<1.
0.60	0	0.25	0.90	2.00	1.20	0.80	1.08	0.60	0.12	0.20	0.38	2.00	0.65	0.24	0
0.60	1	0.41	0.70	2.00	1.20	0.80	0.84	0.47	0.36	0.33	0.52	2.00	0.65	0.34	0
0.60	2	0.59	0.30	2.00	1.20	0.80	0.36	0.33	0.84	0.47	0.64	2.00	0.65	0.42	C
0 40	2	0.42	0.20	2.00	0.80	1 20	0.16	0.70	0.64	0.50	0.56	2 00	0.65	0.36	
0.60	2	0.58	0.30	2.00	1.20	0.80	0.36	0.34	0.84	0.46	0.64	2.00	0.65	0.42	0
0.80	2	0.70	0.60	2.00	1.60	0.40	0.96	0.12	0.64	0.28	0.70	2.00	0.65	0.45	C
0.40	2	0.42	0.20	2.00	0.80	1.20	0.16	0.70	0.64	0.50	0.56	0.77	0.82	0.46	0
0.60	2	0.58	0.30	2.00	1.20	0.80	0.36	0.34	0.84	0.46	0.64	0.77	0.86	0.55	0
0.80	2	0.70	0.60	2.00	1.60	0.40	0.96	0.12	0.64	0.28	0.70	0.77	0.91	0.63	0

Example: A 2-acre lot is developed using the R and D curves. Consider f/i=2 for

1. A LID layout has more runoff reduction on the frequent events than the extreme.

2. A LID layout has more runoff reduction on Level 2 than that on Level 0

3. The R and D curves are developed for planning and can be overridden by on-site design.

4. Two sets of PARF work consistently. PARF has been adopted as the STORMWATER LID Incentive index for stormwater fees and taxes.





Hydrographs Comparison of SWMM5 and CUHP 2005

CASFM Annual Conference 2010 September 21-24, 2010



AMEC Earth & Environmental

Jeffrey Y.C. Cheng, PE Szu-Min Yang , ASLA



SEMSWA

Monica Bortolini, PE CFM

CUHP and SWMM5 Hydrograph Generation

- The Colorado Urban Hydrograph Procedure (CUHP) is an evolution of the Snyder unit hydrograph. (CUHP Manual 2010)
- EPA-SWMM5's subcatchment flow calculations are based on overland flow length and width uses the Kinematic Wave method. (SWMM application Manual 2009)

Snyder Unit Hydrograph

DEFINITION OF PROPERTIES OF SNYDER'S UNIT HYDROGRAPH



Lca - length to watershed centroid
L - length of longest drainage path
Approximate watershed centroid

$$t_{lR} = t_l = C_1 C_t (LL_c)^{0.3}$$



Parameter	Typical Value(s)	Comments
C _t	1.8 - 2.2	Both C _t and C _p should be calibrated or developed from existing UHG's.
C _p	0.5 - 0.7	
L	TBD	The length of the longest drainage path in miles
L _c	TBD	The main channel length from outlet to a point opposite the center of gravity of the basin (miles).
А	TBD	Drainage area in square miles.



Kinematic Wave Unit Hydrograph



$$\frac{\partial q}{\partial x} + \frac{\partial y}{\partial t} = i_e$$

$$\frac{\partial V}{\partial t} + V \frac{\partial V}{\partial x} + g \frac{\partial y}{\partial x} - g(S_0 - S_f) = 0$$

$$q = \frac{1.49}{n} Y^{\frac{5}{3}} \sqrt{S_o} \qquad S_0 = S_f$$

- Watershed has to be rectangular in shape
- Watershed has to include both overland flow area and a concentrated flow channel

Snyder Unit hydrograph and KW Unit Hydrograph



CUHP / Snyder unit Hydrograph

Kinematic Wave method Hydrograph Snyder method variable

- Watershed flow length (L)
- Distance to Centroid (Lc)
- Lag Time factor Ct
- Peak Flow Factor Cp

KW method variable

• Watershed overland flow width (W)

- Impervious "n"
- Pervious "n"



Slide 6

MSOffice1 Jeff - what is phase 2? You only show phase 1 , 9/10/2010



SPECIAL CASES



Slide 7

MSOffice2 Same comment , 9/10/2010

Conditions for Shape Function





Comparison of CUHP-SWMM

Stormwater Volume



	CUHP Input information								
Area (sq Mi)	Distance to Centroid (mi)	Length (mi)	Slope (ft/ft)	Percent Imperviousness					
0.0156	0.0625	0.1250	0.01	70					
0.0469	0.1083	0.2165	0.01	70					
0.1250	0.1768	0.3536	0.01	70					
0.1875	0.2165	0.4330	0.01	70					
0.4688	0.3423	0.6847	0.01	70					
0.7813	0.4419	0.8839	0.01	70					

	SWMM Input information								
Area (acre)	Width (ft)	Slope (ft/ft)	Percent Imperviousness						
10	1320	0.01	70						
30	2286.3071	0.01	70						
80	3733.5238	0.01	70						
120	4572.6141	0.01	70						
300	7229.9378	0.01	70						
500	9333.8095	0.01	70						

Stormwater Volume

Comparison of CUHP-SWMM amec^o





Comparison of CUHP-SWMM

Peak Flow



	Peak Flow Comparison							
Area (acre)	CUHP	SWMM Center channel	SWMM side channel	SWMM Center channel	SWMM side channel			
acre	cfs	cfs	cfs	%	%			
10	54.86	71.43	63.24	30.2%	15.3%			
30	151.23	196.09	159.77	29.7%	5.7%			
80	390.52	458.01	341.56	17.3%	-12.5%			
120	583.00	639.13	476.41	9.6%	-18.3%			
300	1484.74	1302.18	987.12	-12.3%	-33.5%			
500	2193.59	1971.65	1437.31	-10.1%	-34.5%			



Testing watershed selection criteria

• Mature urban developed watershed with rain gage MSOffice7 and stream gage.

- Watershed size should be less than 2000 acres.
- Stream gage location should not impact by backwater effect.
- Watershed width/Length ratio between 0.75 to 4.





MSOffice7 Jeff - please add the Littles Creek watershed here with the proposed stream gages locates where you think they should be with a large mark. , 9/10/2010



Test Case – Littles Creek





CUHP						S	WMM	
Area	L	Slope	Lc	Qp	Ζ	Lw	Sw	Qp
acre	ft	%	ft	cfs	%	ft	%	cfs
33.51	1934.97	1.94%	771.61	162.27	1	1682.45	1.47%	211.67

MSOffice3 Jeff - add what this test is showing under the title. Is it a special shape? Is it random subbasin? If so, which number basin is it? Should be show the whole basin and the subbasins used for comparison with CUHP?


MSOffice4 Same comment , 9/10/2010







CUHP						SWMM			
Area	L	Slope	Lc	Qp	Ζ	Lw	Sw	Qp	
acre	ft	%	ft	cfs	%	ft	%	cfs	
149.57	4971.85	1.13%	1762.52	435.18	0.9	2936.38	1.09%	404.22	

MSOffice5 Same comment , 9/10/2010



MSOffice6 Test Case – Littles Creek





CUHP						SWMM			
Area	L	Slope	Lc	Qp	Ζ	Lw	Sw	Qp	
acre	ft	%	ft	cfs	%	ft	%	cfs	
47.69	2024.93	1.24%	1112.64	137.43	1	2270.88	0.79%	172.62	

MSOffice6 same comment , 9/10/2010



- Compare peak flow
- Compare volume
- Compare time to peak





• Watershed size analysis



Highline Cannel crossing Tributary area =715 acres

Dry Creek Pond. Tributary area=164 acres



Impact of Coupled One-Dimensional and Two-Dimensional Model in Master Planning Studies September 23, 2010

Aaron Cook





Presentation Outline

- One-Dimensional Modeling
- Two-Dimensional Modeling
- Coupled Modeling
- Benefits of Coupled and Two-Dimensional Modeling
- Challenges of Coupled and Two-Dimensional Modeling
- Examples
- Summary/Conclusions

One-Dimensional Modeling

- Typical approach to determining peak flows and floodplain extents
- Steady state
- Water flow is computed in the longitudinal direction
- Terrain represented as a series of cross sections
- Water surface profile determined by solving the energy equation
- Maximum instantaneous peak flow

One-Dimensional Modeling



One-Dimensional Modeling

- No floodplain storage
- Peak flow remains relatively unchanged downstream
- Not an accurate reflection of reality
- Examples:
 - HEC-RAS (Hydrologic Engineering Center River Analysis System)
 - MIKE 11

Two-Dimensional Modeling

- Terrain represented as a continuous surface through a finite element mesh
- Water is allowed to flow in the longitudinal or lateral direction at each element in the mesh
- Hydrographs loaded at elements in the mesh

Two-Dimensional Modeling



Two-Dimensional Modeling

- Accounts for floodplain storage
- Peak flow allowed to change
- More accurate hydraulic modeling approach
- Examples
 - MIKE 21
 - FLOW 2D

Coupled One-Dimensional and Two-Dimensional Modeling

- Channels/Pipes represented as a series of cross sections/culverts/bridges
- Floodplains represented as a finite element mesh
- Water moves between the 1D cross sections and 2D mesh in the direction of the hydraulic gradient
- Example:
 - MIKE FLOOD

Coupled One-Dimensional and Two-Dimensional Modeling



Benefits of Two-Dimensional and Coupled Modeling in Master Planning

- Complicated floodplain systems
 - Multiple flow paths/split flows
- Complicated urban flooding
 - Flow in streets
- Accounts for floodplain storage
- Attenuation of hydrographs
 - More accurate results
- More accurate results

Challenges of Two-Dimensional and Coupled Modeling in Master Planning

- Improvements such as increased conveyance through channels and pipes decreases floodplain storage and attenuation of hydrographs
 - Floodplain storage often caused by undersized infrastructure
 - Floodplain management issues
- Increased flow rates downstream
- Previous estimates for peak flow rates likely underestimate the peak flow with proposed improvements

Challenges of Two-Dimensional and Coupled Modeling in Master Planning

- Coupled or 2D Model must be re-run to determine the new peak flow rate downstream
 - Not cost effective
- More accurate peak flows required to size improvements downstream
- Several hours/days to run simulation versus minutes/seconds for 1D model
 - Simplified approach to save computation time

- Split flow upstream of US Highway 36
- Flow overtops US Highway 36
- Flow along South Boulder Creek mainstem and flow in West Valley
- Floodplain storage throughout the West Valley
 - Road Crossings



- 2D Model identified flood threat to West Valley
- Computation time for regulatory model > 2 Weeks
 - Not time effective to develop model for each alternative
- Simplified approach necessary for master planning purposes

Simplified approach:

- Use coupled model to determine peak flows at key locations
- Assume that known peak flow rates are additive downstream
- Adding peak flow rates may overestimate actual peak flow rates but provides a conservative estimate
 - Assumes no floodplain storage or attenuation of hydrographs
 - Other programs to size infrastructure
 - EPA SWMM 5, FlowMaster, CulvertMaster



Simplified approach:

- Initial master plan recommendations made based on this approach
 - Cost effective approach
- Best alternative plans input into coupled model
 - More accurate results
- Best alternative plans modified based on results

Example: Complex Urban Development Analysis

- Urban flooding
- Multiple flow paths with multiple loading points

Example: Complex Urban Development Analysis

• 2D Modeling Approach

- Flow in pipes removed from hydrographs
- Remaining hydrograph loaded to 2D finite element mesh
- Sinks added where flow leaves the 2D system
- Determine peak flows on surface at key locations
- 2D run time approximately 1 hour
- Best alternative plans can be input into coupled model
 - Coupled run time expected to be greater than 1 hour
 - Interaction between 1D and 2D systems

Example: Complex Urban Development Analysis



Summary/Conclusions

- Coupled or 2D models may provide more accurate floodplain results and may identify additional flood threats
 - Floodplain storage
 - Attenuation of hydrographs
 - Better representation of topography
 - Flow in longitudinal and lateral directions
- Coupled or 2D models used for complicated floodplain situations
 - Multiple flow paths/split flows
 - Urban flooding flow in streets

Summary/Conclusions

- Simplified approach may be necessary
 - Cost effective
 - Saves time
 - Input best alternative plans into Coupled model
 - D Model still run for best alternatives
 - More accurate results

Questions



Modern Stream Equilibrium Analysis

By George Cotton, PE GK Cotton Consulting, Inc.





BACKGROUND

- Very fundamental geomorphic tools where developed in the 1950's by the USGS and USBR including:
 - Leopold and Maddock (1953),
 - Lane (1955),
 - Leopold and Miller (1956),
 - Leopold and Wolman (1957)
- These tools have been used extensively for channel assessment, reclamation and restoration. They link four important stream physical process variables to stream shape.
 - Stream discharge
 - Sediment load
 - Stream gradient
 - Bed material size





GK Cotton Consulting, Inc.

Page 2



Empirical Hydraulic Geometry

The Hydraulic Geometry of Stream Channels and Some Physiographic Implications

By LUNA B. LEOPOLD and THOMAS MADDOCK, Ja.

GEOLOGICAL SURVEY PROFESSIONAL PAPER 252

Quantitative measurement of some of the hydraulic factors that help to determine the shape of natural stream channels: depth, width, velocity, and surpended load, and how they vary with discharge as simple power functions. Their interrelations are described by the term "hydraulic geometry."



6

UNITED STATES GOVERNMENT PRINTING OFFICE, WASHINGTON | 1953



Page 3


Hydraulic Geometry



 $\mathcal{N}(\mathcal{X})$





Equilibrium Condition

American Society of Civil Engineering, Proceedings, 1955, Vol 81, paper 795, pp. 1–17 Copyright 1955 by The American Society of Civil Engineers

8

The Importance of Fluvial Morphology in Hydraulic Engineering

E. W. LANE

The following very general expression will be found useful in analyzing qualitatively many problems of stream morphology:

Q_S d∼Q_wS

Here Q_s is the quantity of sediment, d is the particle diameter or size of the sediment, Q_w is the water discharge, and S is the slope of the stream. This is an equation of equilibrium and if any of the four variables is altered, it indicates the changes which are necessary in one or more of the others to restore equilibrium. For example, if a stream with its sediment load is flowing

9/3/2010

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Channel Equilibrium

(original illustration was by Whit Borland, USBR)





Stream Health



9/3/2010



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Prototype/Model Similitude

GK Cotton Consulting, Inc.

9/3/2010



Effect of Roughness

$$S_{fr} = \left(\frac{n_r^2}{D_r^{1/3}}\right) Fr_r^2 \qquad n_r = d_r^{1/6}$$
$$S_{fr} = \left(\frac{d_r}{D_r}\right)^{1/3} Fr_r^2$$

Sediment Transport

 $g_{b} = b' \vee^{m1} D^{m2}$.





Derived Scaling Relationships

$$D_{r} = Q_{r}^{6/17} d_{r}^{2/17}$$

$$B_{r} = Q_{r}^{8/17} d_{r}^{-3/17}$$

$$V_{r} = Q_{r}^{3/17} d_{r}^{1/17}$$

$$S_{r} = Q_{r}^{-2/17} d_{r}^{5/17}$$

$$G_{br} = Q_{r}^{e} d_{r}^{r}$$

where: e = (8 + 3m1 +6m2)/17 f = (-3 + m1 + 2m2)/17

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Comparison: Theoretical to Empirical

Scaling	Empirical*	Theor	retical
Variable	j	j	k'
Br	0.5	0.47	-0.18
Dr	0.4	0.35	0.12
Vr	0.1	0.18	0.06
Sr	-0.1	-0.12	0.29
Gbr	none	Function of sediment	transport relationship

*Leopold and Maddock (1953)

9/3/2010



Lane Relationship Enhanced

G_b dα Q S

$$G_{br} d_r^g = Q_r^h S_r$$

where:

$$g = 5/17 - f$$

 $h = 2/17 + e$

$$I_E = \frac{Q_r^n S_r}{G_{br} d_r^g}$$



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	UDSWM		DA	2-yr		UDSWM		DA	2-yr
Reach	DP	Location	(sq.mi.)	Existing	Reach	DP	Location	(sq.mi.)	Existing
	286	Park Boundary	361	2,142		274	Lincoln Avenue	305	1,544
1					5				
	280	County Line	338	1,798		266	West Parker Road	288	1,302
2					6				
	337	Cottonwood Drive	333	1,567		262	Stroh Avenue	267	1,170
3					7				
	276	E-470	310	1,558		250	Scott Road	241	972
4					8				
	274	Lincoln Avenue	305	1,544		247	SH 86	207	664



HEC-RAS 4 Derived Sediment Transport Equation

A test relationship was developed from data on the Platte River (Big Bend reach) to demonstrate how HEC-RAS 4 can be used to develop a power function for sediment transport. The sediment gradation is as follows:



Eq	Q (cfs)	Tons	Tons/day	C (ppm)	V (ft/s)	R (ft)	So (ft/ft)
Ackers	100	0.0095	9.48	35	1.8	2.53	0.0005
Ackers	200	0.0291	29.13	54	2.2	3.44	0.0005
Ackers	500	0.1013	101.26	75	2.7	4.85	0.0005
Ackers	1000	0.2311	231.10	86	3.1	6.02	0.0005
Ackers	2000	0.5021	502.10	93	3.6	7.26	0.0005
Ackers	5000	1.3658	1365.81	101	4.2	9.13	0.0005
Ackers	10000	2.6533	2653.31	98	4.5	10.41	0.0005
Ackers	100	0.0368	36.76	136	2.2	2.14	0.0010
Ackers	200	0.1029	102.90	191	2.8	2.96	0.0010
Ackers	500	0.3397	339.74	252	3.5	4.29	0.0010
Ackers	1000	0.7635	763.54	283	4.1	5.43	0.0010
Ackers	2000	1.6314	1631.38	303	4.7	6.63	0.0010
Ackers	5000	4.3717	4371.74	324	5.5	8.39	0.0010
Ackers	10000	8.8831	8883.06	330	6.2	9.82	0.0010
Ackers	100	0.1222	122.24	453	2.8	1.80	0.0020
Ackers	200	0.3262	326.19	605	3.5	2.53	0.0020
Ackers	500	1.0577	1057.74	785	4.6	3.76	0.0020
Ackers	1000	2.3848	2384.84	885	5.4	4.85	0.0020
Ackers	2000	5.1164	5116.41	949	6.3	6.02	0.0020
Ackers	5000	13.6302	13630.21	1011	7.4	7.69	0.0020
Ackers	10000	28.5359	28535.93	1059	8.3	9.14	0.0020
Ackers	100	0.2354	235.37	873	3.2	1.63	0.0030
Ackers	200	0.6189	618.88	1148	4.1	2.30	0.0030
Ackers	500	2.0050	2005.02	1466	5.3	3.46	0.0030
Ackers	1000	4.5570	4556.96	1690	6.4	4.52	0.0030
Ackers	2000	9.8705	9870.45	1831	7.4	5.67	0.0030
Ackers	5000	26.3605	26360.51	1956	8.8	7.30	0.0030
Ackers	10000	65.6673	55557.33	2061	9.8	8.70	0.0030



9/3/2010

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Existing Conditions

Reach	Q _{2vr} (cfs)	So (%)	B-active (ft)	B-total (ft)	D-active (ft)	Y _{2vr} (ft)	Qactive (cfs)	V _{ave-active} (ft/s)	G _b (T/day)
1	1798	0.409	30.0	300	2.9	4.4	986	7.5	23,963
2	1567	0.394	28.0	280	3.4	4.7	983	7.5	22,911
3	1558	0.369	21.0	210	4.0	5.6	910	7.7	20,707
4	1544	0.369	22.0	220	3.4	5.1	832	7.4	17,820
5	1302	0.414	27.0	270	3.0	4.2	809	7.2	17,329
6	1170	0.365	16.0	165	3.8	5.5	632	7.2	11,519
7	972	0.408	24.0	240	3.1	4.0	666	6.9	12,305
8	664	0.392	16.0	160	3.7	4.6	485	6.6	7,340
Р	664	0.390	18.0	160.0	2.0	3.2	347	5.9	4,266



Reach	Gbr	d٢	Qr ^h	Sr	IE
1	5.62	1.00	5.05	1.05	0.94
2	5.37	1.00	5.02	1.01	0.95
3	4.85	1.00	4.46	0.95	0.87
4	4.18	1.00	3.88	0.95	0.88
5	4.06	1.00	3.71	1.06	0.97
6	2.70	1.00	2.54	0.94	0.88
7	2.88	1.00	2.75	1.05	1.00
8	1.72	1.00	1.68	1.01	0.98
Р	1.00	1.00	1.00	1.00	1.00

9/3/2010

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Existing Conditions Adjusted to Equilibrium

Reach	Q _{2vr} (cfs)	So (%)	B _{active} (ft)	B _{total} (ft)	D _{active} (ft)	Y _{2vr} (ft)	Q _{active} (cfs)	V _{ave-active} (ft/s)	Gb (T/day)
1	1798	0.390	34.7	300	3.4	4.6	1213	7.6	29,684
2	1567	0.390	32.1	280	3.3	4.5	1074	7.4	24,599
3	1558	0.390	34.0	210	3.3	4.6	1168	7.5	28,005
4	1544	0.390	33.4	220	3.3	4.5	1130	7.5	26,616
5	1302	0.390	27.3	270	2.8	4.0	764	6.9	14,466
6	1170	0.390	29.0	165	2.9	4.2	863	7.1	17,511
7	972	0.390	21.4	240	2.3	3.6	482	6.3	7,099
8	664	0.390	18.2	160	2.0	3.3	354	6.0	4,398
Р	664	0.390	18.0	160.0	2.0	3.2	347	5.9	4,266



Reach	Gbr	dr ^g	Qr ^h	Sr	ΙE
1	6.96	1.00	6.96	1.00	1.00
2	5.77	1.00	5.77	1.00	1.00
3	6.56	1.00	6.56	1.00	1.00
4	6.24	1.00	6.24	1.00	1.00
5	3.39	1.00	3.40	1.00	1.00
6	4.10	1.00	4.10	1.00	1.00
7	1.66	1.00	1.67	1.00	1.00
8	1.03	1.00	1.03	1.00	1.00
Р	1.00	1.00	1.00	1.00	1.00

9/3/2010

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Comparison: Existing to Equilibrium Conditions



GK Cotton Consulting, Inc.



Questions?

• Contact information

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9/3/2010

Statistical Methods in Flood Hydrology

Benefits of the Using Statistical Analysis of Gage Records for determining flood frequency-discharge relationships

Stream Gage Records integrate the consideration of all stochastic hydrologic variables that are determinant of stream flood flow for rural watersheds that have not experienced significant urbanization

Stream Gage Records represent the result of all the random hydrologic variables that contribute stream flow



Statistical Analysis of U.S.G.S Stream Gage Records

- Statistical Analysis of Stream Gage flow records is accomplished using the Log Pearson Type III Distribution as proposed in Bulletin 17 B published by the U.S. Water Resources Council
- The Log Pearson Type III distribution is characterized by Three Moments (Mean, Variance and Skew)
- Without consideration of the third order Moment (Skew) the Log Pearson Type III distribution becomes the log normal distribution

Analysis of Measured Stream Flow

- Analysis of stream flow data from reliable gage sites (Typically USGS Stream Gaging Stations) allows for consideration of all random hydrologic variables that are determinant of stream flow as represented in
- Stream gage records are useful in the prediction of flood peaks for various return periods at un-gaged sites
- Stream flood flow relationships between watershed descriptors such as drainage area ;Mean channel slope, and Lake and Marsh Area are generally non-linear with respect to observed flow - The principles of linear modeling and multiple regression analysis can be used with non-linear prediction equations that have been transformed to an equation that is linear in the coefficients.

Increased Sampling Variation Occurs for Higher Order Moments

 Due to the significant sampling error associated with skew (the third order moment in the Log Pearson Type III Distribution) - Station Skew should be weighted with the regional skew as determined by the using iso-skew map included in Bulletin 17B.

Historic Flood Data

 Historic flood information should be incorporated into the systematic stream gage record when this can be done with reasonable accuracy

Comparisons should be made with similar watersheds when possible

 Gage Comparisons should be made with other gage stations in a homogeneous region for a flood event.

Evaluation of Flood Risk

 When events can be considered to be independent the Binomial Theorem can be used to evaluate Risk - The Binomial Theorem can be used to evaluate the probability of (I) flood events over the course of N Years with a given exceedance probability.

Application of the Binomial Theorem

The binomial expression for risk is:
RI= N!/(I!((N-I)! * (1-P)^N-1)

In which RI is the estimated risk of obtaining in N Years exactly I number of flood events exceeding a flood magnitude with annual exceedance probability P.
When I equals o equation 10-1 reduces to

Ro = (1-P)^N

Risk Evaluation for Independent Events

 Example for evaluating risk using the binomial theorem. The Binomial Theorem can be used to evaluate the probability of independent events
 Example:

A bridge with a design life of 40 years is designed to pass a 100-year flood. The design engineer is interested in determining the probability that the bridge will be submerged two times during its design life.
The probability of the bridge being submerged in exactly two times in 40 years is
PI*(1-p) ^(n-x)* .01^2
(.01)^2*.98^.38 = .050

Flood Estimates based on Precipitation Data

 Flood Estimates based on precipitation data and a valid watershed model can be integrated with the systematic gage records when adequate precipitation data , land use and soil type data is available is available for use in a hydrologic model Advantages of Predicting Peak Flood Flows using Statistical Inference from Peak flow Data

 Stream Gage records represent the end data that includes consideration of all random hydrologic variables that combine to determine Peak Flow for a flood event

• Pertinent hydrologic variables include:

- Precipitation Amount
- Precipitation Intensity
- Antecedent Soil Moisture Condition
- Soil Permeability
- Temporal Pattern of Precipitation

Randomness of Precipitation Events

 In general, an array of flood events may be considered a random sample of independent events

 Even when a test of serial correlation indicates a deviation from this assumption; the annual peak data may provide for an unbiased estimate of return period for flood events

Estimating Generalized Skew

- The skew in the Log –Pearson Type III distribution is sensitive to extreme events
- There are two generalized methods of determining the appropriate skew.
- Calculating the skew of 40 Stations within a 100 mile radius of the stream gage station being evaluated
- Development of a skew iso-line map from skew calculations for all gaging stations used in the analysis

Skew Isoline Map from Bulletin 17B

- Bulletin 17B includes a skew map for the United States
- Weighting of Station Skew and Generalized Skew
 Following is the equation for weighting:

 the
 the

 Station Skew and Generalized Skew

Gw =Weighted Skew

Generalized Skew Map



Skew Coefficient

• Effects of Neutral, Positive and Negative Skew



Skew results in asymmetric distribution

Statistical Inference for Flood Flows

 The non-linear equations that typically relate flood peak discharge and watershed characteristics must be transformed to equations that are linear in the coefficients

Quantifiable Drainage Area Characteristics

Drainage Area Characteristics typically related to drainage area characteristics in a non-linear manner Example: Q(2) = (Peak Flow for the two year flood) $Q(2) = (D.A.^X_1)^*(LMA^X_2)^*(CS^X_3)$ Where D.A. = Drainage Area in Square miles LMA = Lake and Marsh Area in Square Miles CS = Average Channel Slope in (ft. per mi.) Predictive Equations transformed to be linear in the Coefficients Example $Q_2 = X_1^*(\log D.A.(Sq. Mi.)) + X_2^*(\log C.S.))(ft./mi.$ $+X_3^*((\log LMA)(Sq. Mi.))$ Mathematics of the Linear Model Normal Equations in the Linear Model

Watershed Changes

• It has become increasingly difficult to find watersheds that have not changed significantly over the period of record for the gaged location.

 The use of statistical inference in the form of a linear model should be used for watersheds that have not experienced significant increases in impervious area in the recent past

Determination of the Flood Frequency Relationship

 An annual or partial duration series can be employed when determining a flood frequency relationship

 The annual series consists of only the annual peak in any Water Year

Statistical Analysis of Stream Gage Records

 The log Pearson Type III distribution has been adopted in Bulleting 17B

• All flows in the period of record should be transformed to the logarithm of the peak flow
Drawing inference from un-gaged sites

 Use of Linear Modeling techniques to draw inference about peak flood flows based on Linear Modeling (Regression) techniques

 The relationships between a watershed response and a measureable watershed characteristic is generally nonlinear

 This condition is dealt with by transforming prediction equations an equivalent predictive equation that is linear in the coefficients

Predictive Equations that express are transformed to be linear in the coefficients

 Non-linear equations that can be used to predict flood flows as a function of watershed characteristics if the predictive equations are transformed to be linear in the coefficients

> Non-linear Equation Q=βo *(D.A.^β1)*(LMA^β2)*(CS^β3)

• Transformed Equation that is linear in the Coefficients Example : $Q = \log \beta o + \beta 1^* \log D.A. + \beta 2^* \log LMA + \beta 3^* \log CS$

Coefficient Matrix for the Linear Model



Solving the Linear Model Simultaneous Equations

 EXCEL Math Tools can be used to invert the coefficient Matrix and multiply the inverted coefficient matrix times the right hand vector for an ordinary least squares model or a generalized least squares model

Stream Stats by the U.S Geological Survey

Stream Stats by the U.S Geological Survey
 Allows for generalized least squares (variance weighted)
 Ordinary Least Squares (not variance weighted)

Stream Stats allows for access to all USGS Stream Gage Records and development of linear model for prediction of flood flows

Techniques for Integrating Hydrologic Analysis with Statistical Hydrologic Methods

 Simulating a period of hydrologic record to produce peak annual flood flows can serve as another hydrologic analysis technique that allows for inclusion of all of the random variables in the determination of annual flood flows

 Is there any reason to think that the peak flows obtained from a model that can simulate flood flows would not fit a Log Pearson Type III Distribution ?

Good References for Statistical Hydrology

Bulletin 17 B Published by the U.S Water Resource Council

Statistical Hydrology by C. T. Haan

Stochastic Processes in Hydrology Probability and Statistics in Hydrology by Vujica Yevjevich

Statistical Analysis is Fun!

- Imagine the excitement that comes with collecting your own flood data from the USGS Stream Gage Records and doing the math using excel
 - Excel can multiply two matrices
 - Invert matrices
 - Multiply an inverted coefficient matrix with a vector to obtain a solution vector

 Or.....exercise your own good judgment and let Stream Stats predict flood flows accepted stream gage records using

Aquatic Organism Passage Design Guidelines for Culverts

Roger Kilgore, Kilgore Consulting and Management

CASFM Conference September 21-24, 2010 Snowmass Colorado

Goal for AOP Culvert Designs (HEC 26)

- Culvert designs providing aquatic organism passage (AOP).
- Culvert designs satisfying peak hydraulic criteria and protective of the public.
- Objective and reproducible design criteria and procedure.
- Fill a void where guidance is lacking or not subject to consensus.
- **#** Defensible procedure for justifying expenditures.

FHWA HEC 26 Approach

- Create conditions within the crossing similar to those in the natural channel in both bed structure and function.
- Presumption: Bed material experiences same forces as aquatic organisms (AO). If bed behavior is similar in crossing, AO that pass stream can pass crossing.
- Proxy approach. Range of flow from low passage to high passage.
- Use where no other approach is already accepted or for comparison.

Presentation Outline

Design procedure outline
Case studies
North Thompson Creek, Colorado
Sickle Creek, Michigan
Results comparison

Fundamental Tests in Design Procedure

Does culvert satisfy peak flow, Q_P requirements?

Is bed material stable or in equilibrium for high passage flow, Q_H ?

Is bed stable/protected at peak flow.

Is velocity acceptable compared to stream?

Is depth acceptable compared to stream?







Tools Available

Culvert hydraulics HEC-RAS HY8/Normal depth computations **#** Channel analysis HEC-RAS Normal depth computations **#** HEC 26 spreadsheet (channel stability and data management)

Case Study: North Thompson Creek, Colorado



Source: Mark Weinhold (USFS)

Existing 36" CMP culvert.

Inlet





Step 1. Determine design flows: Q_P, Q_H, Q_L

- **\ddagger** Peak discharge, Q_P .
 - Based on pertinent high flow criteria.
- **\ddagger** High passage discharge, Q_{H} .
 - Site-specific guidelines
 - 10% exceedance on annual flow duration curve
 - 0.25 of Q₂
- **\blacksquare** Low passage discharge, Q_L .
 - Site-specific guidelines
 - 90% exceedance on annual flow duration curve or 7Q2.
 - 1 ft³/s minimum

Discharge Estimates

	Blakemore, et al.	Kircher, et al. (1985)	
Discharge	(1997) High Elevation	Mountain Region,	
Quantity	Region 1, ft ³ /s (m ³ /s)	ft³/s (m³/s)	
Q ₂₅	Q _P = 103 (2.92)	66 (1.9)	
Q ₂	41 (1.2)	30 (0.85)	
Q _{10%}		Q _H = 8.8 (0.25)	
0.25Q ₂	10.2 (0.3)	7.5 (0.21)	
Q _{90%}		0.15 (0.0042)	
7Q2		0.13 (0.0037)	
Q _L (min)		$Q_L = 1 (0.028)$	

Step 2. Determine Project Reach and Characteristics

Reach length upstream and downstream:
Three culvert lengths (3 x 46 = 138 ft)
200 ft
Selected: 200 ft downstream, 300 ft upstream
Cross sections. Min of 3 upstream and downstream (4 downstream, 5 upstream)
Bed material.



Steps 3 and 4.

- Step 3. Check for dynamic equilibrium.
 No indicators of instability at site.
- # Step 4. Analyze and Mitigate Channel Instability.
 - Not necessary at this site.
 - If mitigation was necessary, other tools beyond HEC 26 are required.

Step 5. Align and Size Culvert for Q_P

Determine design criteria.
Select Bed Material (Use natural, D₅ no greater than 2 mm)
Horizontal alignment.
Vertical alignment.
Embedment criteria.

Vertical profile of project reach



Bed Material Gradation

Quantile	XS 57 (mm)	XS 172/215 (mm)	Design (mm)	Design with added fines (mm)
D ₉₅	218	285	250	250
D ₈₄	151	194	170	170
D ₅₀	55	45	50	50
D ₁₆	22	21	21	20
D ₅	13	13	13	2

Align and Size Culvert for Q_P

- Design criteria: HW/D < 1.2 or 1.0 (for larger culverts) and no overtopping.</p>
- Select Bed Material. Manning's n for bed (0.044)/walls (0.035). Need composite n
- **#** Horizontal alignment: maintain existing.
- Vertical alignment: S=0.0267 ft/ft (Existing culvert S=0.0395 ft/ft)
- Embedment depth: 30% (for circular pipe) minimum 2 ft rise.

Initial Trial: 6.5 ft CMP with 2.0 ft embedment.

Step 6. Is culvert bed stable at Q_H ?

Determine Manning's n for bed
Determine permissible shear stress.
Modified permissible shear stress.
Critical unit discharge.
Determine applied shear stress:

Inlet and outlet of culvert
Upstream and downstream cross-sections.



Culvert bed in 6.5 ft CMP not stable.



Step 7. Check Channel Bed Mobility at Q_H.

- If shear stress in any channel XS is less than permissible redesign culvert.
- If shear stresses in all channel XS are greater than permissible, bed is considered mobile.
 - Culvert shear stresses within range in channel? OK.
 - Culvert shear stresses exceed channel shear stresses? Redesign culvert.

Culvert bed in 6.5 ft CMP and in channel. Redesign culvert.



2nd Trial

Try 7.5 ft CMP.

- Passes peak flow in Step 5.
- Culvert bed stable in Step 6. (No need for Step 7.)
- **#** Proceed to Step 8.

Step 8. Check Culvert Bed Stability at Q_P

 Few sites will exhibit bed stability at Q_P.
 For 7.5 ft CMP on North Thompson Creek the shear stresses range from 2.6 to 3.2 lbs/ft² at the inlet and outlet of the culvert with either HEC-RAS or HY-8.

■ Permissible shear stress is 1.0 lbs/ft².

Bed not stable, go to Step 9.

Step 9. Design Stable Bed

Provide an oversized sublayer to resist further lowering of bed and to provide a rough base for replenishment of native materials.

H Minimum Criteria:

- Native streambed layer: Largest of D₉₅ (native material) or 1ft.
- Oversized sublayer: 1.5 D₉₅ (oversize material) for circular pipes.
- Two layers combined should be no less than the minimum required embedment.

Oversize Bed Gradation

	Native	Oversize
Quantile	(mm)	(mm)
D_{95}	250	305
D ₈₄	170	226
D ₅₀	50	162
D ₁₆	20	36
D_5	2	2

- Initial trials were unsuccessful. (Spreadsheet tool available.) Culvert increased to 8.5 ft CMP.
- **\blacksquare** Native layer = 1.0 ft
- Oversize layer = 1.55 ft
- **\blacksquare** Total embedment = 2.55 ft
Step 10. Check Velocity at Q_H.



Step 11. Check depth at Q_L.



Step 12. Provide Low-flow Channel in Culvert.

Design triangular low-flow channel.
1:8 (V:H) side slopes
Result: Thalweg 0.5 ft deeper than edges. (Note that native D₈₄ is 0.55 ft.)
Stream processes will modify channel over time.

Step 13. Review Design

- \$\$ 8.5 ft CMP
 \$\$ 2.5 ft Embedment
 Oversize layer
- **#** Cover
- **#** Constructability
- **#** Service life.
- ➡ Other shapes or materials?
- ♯ Open-bottom design?



Design Comparison

	North Thompson	Tributary to Bear	Sickle Creek,
語いにも小いたとう	Creek, Colorado	Creek, Alaska	Michigan
AOP barrier/	3-ft CMP	5-ft CMP	Twin 3-ft CMPs
Existing		マネタンシス シンシ	いたべたりシストン
As-built	12'x ? squash pipe	9.75'x 6.6' pipe arch	16'x 6' concrete arch
シストラインシスト			bridge
HEC-26 procedure	8.5' CMP	12' CMP	10' CMP
Difference in span	-3.5 ft	+2.25 ft	-6 ft
Bankfull Width	8 - 17	7 - 11	not available
Estimate (ft)	法公历法律师	公司法法官议议	先不同或益能

- Not surprisingly, AOP Design results in larger openings than "hydraulically efficient" design.
- Some culverts larger, some smaller, compared to alternative methods, e.g. stream simulation.

Summary

- HEC 26 provides a documented reproducible procedure based on sound analytical tools for designing culverts for AOP.
- All AOP design methods use a proxy for aquatic organism behavior. For HEC 26 the proxy is bed stability with checks for velocity and depth. For stream simulation the proxy is bank full width.
- Where other methods are adopted by agreement for AOP, those methods should be used. HEC 26 provides a tool set where one is needed or can be used as a check.

CONSTRUCTION VIBRATION MONITORING

2010 ANNUAL CASFM CONFERENCE SEPTEMBER 23, 2010 PRESENTED BY:

SOUTHEAST METRO STORMWATER AUTHORITY URBAN DRAINAGE AND FLOOD CONTROL DISTRICT





RECENT PROJECTS -CONSTRUCTION COMPONENTS AND METHODS -UNFORESEEN COSTS TO ADDRESS VIBRATION CONCERNS -VIBRATION MONITORING RESULTS -LESSONS LEARNED

FUTURE PROJECT CONSIDERATIONS -BUDGET CONSIDERATION -DESIGN CONSIDERATIONS -CONSTRUCTION CONSIDERATIONS

CONCLUSION

LITTLE DRY CREEK

CAISSONS

CUTOFF WALL



LITTLE DRY CREEK



BEFORE





LITTLE DRY CREEK

CONSTRUCTION COMPONENTS -DEMOLITION -DELIVERY OF MATERIALS -PAVING OPERATIONS -CUTOFF WALL -CAISSON DRILLING



CONSTRUCTION METHODS –CUTOFF WALL (SHEET PILE VS. CONCRETE)

PINEY CREEK

SHEET PILE DROP STRUCTURE



BRIDGE ABUTMENTS

SHEET PILE DROP STRUCTURE **PINEY CREEK**



BEFORE





PINEY CREEK

CONSTRUCTION COMPONENTS

DELIVERY OF MATERIALS – BOULDERS SHEET PILE DRIVING FOR DROP STRUCTURES H-PILE DRIVING FOR BRIDGE ABUTMENTS PAVING

CONSTRUCTION METHODS –NO ALTERNATIVES



UNFORESEEN COSTS TO ADDRESS VIBRATION CONCERNS LITTLE DRY CREEK

RESIDENTIAL STRUCTURAL INSPECTION AND ANALYSIS OF DAMAGE CLAIMED COST = \$1,840.70

VIBRATION MONITORING COST = \$2,516.67

TOTAL COSTS = \$4,357.37



UNFORESEEN COSTS TO ADDRESS VIBRATION CONCERNS **PINEY CREEK**

RESIDENTIAL STRUCTURAL INSPECTION COST = \$3,638.80 X 2 (PRE & POST) **RESIDENTIAL WELL INSPECTIONS** COST = \$5,500.00 X 2 (PRE & POST) **RESIDENTIAL SEPTIC INSPECTIONS** COST = \$540.00 X 2 (PRE & POST) **VIBRATION MONITORING** COST = \$4,000.00CONSTRUCTION DELAY COSTS COST = \$13,500.00

TOTAL COSTS = \$36,857.60



VIBRATION MONITORING RESULTS

LITTLE DRY CREEK

VIBRATION FROM SHOVEL FALLING (.445 in/sec)

HIGHEST READING (.805 in/sec) FROM TECH STEPPING NEXT TO MONITORING UNIT

MAX READING (.750 in/sec) THRESHOLD THAT COULD CAUSE DRY WALL CRACKING

DAMAGE OBSERVED IN HOME WAS INCONCLUSIVE



VIBRATION MONITORING RESULTS

PINEY CREEK

HIGHEST READING (.660 in/sec) 18-INCHES FROM H-PILE DRIVING WITH COMBUSTION HAMMER

MAX READING (.750 in/sec) THAT COULD CAUSE CRACKING OF DRY WALL



LESSONS LEARNED

BE PROACTIVE VS. REACTIVE

CONSIDER INVESTIGATION THAT CAN BE DONE AT GEOTECHNICAL ENGINEERING LEVEL

VIBRATION MONITORING IS CHEAPEST INSURANCE

IDENTIFY ANY PRE-EXISTING STRUCTURAL OR FOUNDATION ISSUES

IDENTIFY RURAL UTILITIES AND ISSUES

BUDGET CONSIDERATIONS

DESIGN •GEOPHYSICIST INCLUDED WITH SCOPE OF GEOTECHNICAL INVESTIGATION •EVALUATION OF CONSTRUCTION COMPONENTS AND METHODS

CONSTRUCTION •MONITORING •INSPECTIONS



DESIGN CONSIDERATIONS



CONDITIONS THAT VIBRATION EVALUATION IS NEEDED

GEOTECHNICAL SCOPING AND INVOLVEMENT GEOPHYSICIST TO DETERMINE INFLUENCE LIMITS

TYPE OF PROJECT COMPONENTS AND CONSTRUCTION METHODS

CONTINUOUS ON-SITE MONITORING FOR HIGH RISK ACTIVITIES

SCHEDULE/TIME OF WORK

CONSTRUCTION CONSIDERATIONS

INSPECTIONS PRE AND POST CONSTRUCTION •STRUCTURAL, WELL, SEPTIC •NEW CRACKS VS. OLD •IMPACTS TO WELL FROM TESTING

VIBRATION MONITORING DURING CONSTRUCTION •MONITORING READINGS •TECH EVALUATES READINGS CLOSE TO THRESHOLDS

CONSTRUCTION CONSIDERATIONS

SOMETHING NOT ANTICIPATED (#\$&%!) •DUE TO PROPERTY OWNER COMPLAINT •CHANGE IN CONSTRUCTION METHOD

SCHEDULE IMPACT TO PROJECT
POTENTIAL CLAIMS FROM CONTRACTOR
LIMITING CERTAIN TYPES OF WORK OUTSIDE NORMAL WORKING HOURS
DELAYS FOR UNKNOWN UTILITIES
HOMEOWNER FRUSTRATIONS AND COMPLAINTS
START FINDING PROBLEMS

CONCLUSION

PLAN ON SPENDING A LOT OF MONEY TO SHOW PEOPLE THAT THERE IS NO DAMAGE

MONITORING AND INSPECTIONS ARE INSURANCE TO AVOID PROPERTY OWNER CLAIMS

BETTER TO BE PROACTIVE VS. REACTIVE TO SAVE POTENTIAL DELAY COSTS AND CLAIMS

THIS PRESENTATION IS A ROUGH OUTLINE OF GUIDELINES THAT WE ARE WORKING ON WITH A CONSULTANT IN ORDER TO REFINE AND USE FOR FUTURE PROJECTS

QUESTIONS



Using the HEC-14 CSU Rigid Boundary Basin Method with Grouted Boulders for Storm Sewer Outfalls

Getting Aesthetically Softer Results from hard protection

- Background HEC-14 CSU Rigid Boundary Basin
- 2. Rigid Outfalls in Natural or Park Areas
- 3. Overview of Method with Boulders
- 4. Construction and End Results
- 5. Conclusion

CSU Rigid Boundary Basin



CSU Rigid Boundary Basin

- Uses staggered rows of rectangular roughness elements in a concrete apron to initiate a hydraulic jump.
- Basic relationships for roughness element geometry and the size/shape of the element array are given.



Prepared by:	Eugene Voldansky	Checked By	C. Haggerty
Project Name:	Hampden Heights Outtall	Date:	2/19/2000
Cocation	Derwer, CO	Task No:	31537A

HEC-14 - CSU Rigid Boundary Basin Calculation

Sizing of Energy Dissipator

Cu	verd #	3	height (#) RCB		
	W, *	8	width (ft)		1
	L.e.	53	length (tt)		K
	S÷	0.003	slope (#011)		1
	Q =	360	discharge (8%s)		1 (1
	n *	0.013	roughness coefficier	4	1.1
	Ye =	2.31	cotical depth (it) (Val	ue acquired from FlowMaster]	X
	- X42	3	normal depth (ft) [Fu	(Pipe)	3
ownstream netural char	onie/:				
	W=	36	channel width (t)		-
	TWE	3.08	tailwater depth (ft)	[Value acquired from FlowMaster]	
1. Sec. 1				Tailwater Depth actualy 2.09 ft plus 1 ft freeboard	
alution	1000	an a	and the second second	and a local of the local states and	
vib 1	Go	mpute the ve	socity, V a, depth, Y a, an	d Froude number, Fr, at the culvert outlet.	
Y.	y _k =	3	outiet depth (it) [Val-	e acquired from FlowMaster]	
- M	V. =	15	culvert outlet velocit	(I (velocity at normal depth) [Value acquired from FlowMas	ster]
Y # *					

Step 2,

Select a trial basin from table 9.1 based on the W _MW_ expansion ratio best suiled for site geometry constraints:

Culture Indet

Right Brinning Basin

Choose W_{\pm}/W_{α_1} number of rows, Nr, number of elements, N, and ratios hig $_{\pm}$ and L/h. is = 4.50

channel/culvert widths =

Try the following rectangular basin [Table 9.1]

WyW,=	4.5	basin width to culvert width ratio	
WyW,=	0,5	element width to culvert width ratio	
N.=	3	rows	
N =	12	elements	
h/y _A =	1	element height to approach flow average depth ratio	h=2'
L/h =	3	element length spacing to element height ratio	spacing=6"



Prepared by:	Eugene Voldansky	Checked By	C. Haggerty
Project Name:	Hampden Heights Outtall	Date:	2/19/2008
Location	Derwer, CO	Task No:	31537A

HEC-14 - CSU Rigid Boundary Basin Calculation

W=

TWe

36

3.08

Sizing of Energy Dissipator

Downstream netural chennel!

Given

Culvert =	8	height (ft) RCB
W., =	8	width (ft)
L'=	53	length (ft)
5 =	0.003	slope (fbft)
Q =	360	discharge (th ² /s)
n =	0.013	roughness coefficient
y., =	2.31	critical depth (it) [Value acquired from FlowMaster]
¥.=	3	normal depth (ft) [Full Pipe]



which may never them it have not a set of the set of the	and the set of the set	the second se	and the local sector of the	could be a successful to the
CONCLUMENTER DESCRIPTION V	GADD V.	ACTUAL PROVIDENT	DURING PAR	AT MIE CONVERTIONNE

channel width (it)

taiwater depth (ft)

		· 이상 방향 그 '부탁/ 이용 한 방향(방송, 그런 이 지수는 것 같은 것 같
$y_{k}\equiv y_{k}\equiv$	3	outlet depth (it) [Value acquired from FlowMaster]
V . = V. =	15	culvert outlet velocity (f(velocity at normal depth) [Value acquired from FlowMaster
Fr=	1.528	froude number = $V_{\nu}(y_{\nu}g)^{V_{\alpha}}$

Step 2,

Solution Step 1

Select a trial basin from table 9.1 based on the W ___WW__ expansion ratio best suiled for site geometry constraints:

Choose W_{\pm}/W_{α_1} number of rows, Nr, number of elements, N, and ratios h/y $_{\pm}$ and L/h. Ins = 4.50

channel/culvert widths =

Try the following rectangular basin [Table 9.1]

WyW,=	4.5	basin width to culvert width ratio	
WyW,=	0,5	element width to culvert width ratio	
N,=	3	rows	
N =	12	elements	
h/y _A =	1	element height to approach flow average depth ratio	h=2'
L/h =	3	element length spacing to element height ratio	spacing=6'



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Project Name:	Hampden Heights Outtall	Date:	2/19/2000
Location	Derwer, CO	Task No:	31537A

HEC-14 - CSU Rigid Boundary Basin Calculation Sizing of Energy Dissipator

W=

TWE

36

3.08

4.50

Downstream natural channel:

Given

Culvert =	8	height (it) RCB
W _e =	8	width (ft)
Le	53	length (ft)
5 =	0.003	slope (1011)
Q =	360	discharge (tt ² /s)
n =	0.013	roughness coefficient
y,, =	2.31	critical depth (it) [Value acquired from FlowMaster]
¥.=	3	normal depth (ft) [Full Pipe]

channel width (tt)



Figure 2.1. CBJ Right Brandwy Basin

Solution			Tailwater Depth actualy 2.09 ft plus 1 it theeboard
Step 1	Co	mpute the ve	locity, V ., depth, y ., and Froude number, Fr, at the culvert outlet.
	.y, = y, =	3	outlet depth (it) [Value acquired from FlowMaster]
	V. = V. =	15	culvert outlet velocity (f(velocity at normal depth) [Value acquired from FlowMaster]
	Fra	1,528	froude number = VU(Vu) ^{Na}
Step 2.	Se Ch	lect a trial ba oose W _* /W	sin from table 9.1 based on the W_{\pm}/W_{\pm} expansion ratio best suited for site geometry constraint $_{a}$, number of rows, Nr, number of elements, N, and ratios h/y $_{\pm}$ and Lfh.

taiwater depth (h) [Value acquired from FlowMaster]

channel/culvert widths =

Try the following rectangular basin [Table 9.1]

		a canada a secondar a s	
V./W. =	4.5	basin width to culvert width ratio	
VyWy =	0,5	element width to culvert width ratio	
N.=	.9	rows	
N =	12	elements	
h/y _A =	1	element height to approach flow average depth ratio	h=2'
L/h =	3	element length spacing to element height ratio	spacing=6*



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Project Name:	Hampden Heights Outtall	Date:	2/19/2009
Location	Derwer, CO	Task No:	31537A

HEC-14 - CSU Rigid Boundary Basin Calculation

Sizing of Energy Dissipator

Downstream natural channel:

Given

Culvert = W, =	8	height (ft) RCB width (ft)
L =	53	length (#)
0=	360	slope (1011) discharge (19 ² /s)
n =	0.013	roughness coefficient
y., =	2.31	critical depth (it) [Value acquired from FlowMaster]
'Y*=	3	normal depth (ft) [Full Pipe]

channel width (tt)

taiwater depth (ft)



Solution

Step 1 Compute the velocity, V =, depth, y =, and Froude number, Fr, at the culvert outlet. Y_a = Y_a = 3 outlet depth (t) [Value acquired from FlowMaster] V_a = V_a = 15 culvert outlet velocity (t(velocity at normal depth) [Value acquired from FlowMaster] Fr = 1.528 froude number = V_v(y_a)^{Value} Step 2 Select a trial basin from fable 9.1 based on the W = /W_a expansion ratio best suited for ste geometry constraints Choose W = /W_a, number of rows, Nr, number of elements, N, and ratios kiy = and L/h.

channel/culvert widths = 4.50

W=

TWE

36

3.08

Te.	Allow Halling	Costs and off hims for	show A section 7	Fach lot 10 413
	THE FURDA	THE PERSON	FREE STREET	1 4047 (F 1 5
1 2 2 4 4 4 V				

WVW = 0.5 element width to culvert width rabo
AL - A AND AND A
IN THE LEASE
N = 12 elements
hype I element height to approach flow average depth ratio h=2"
L/h # 3 element length spacing to element height ratio spacing #6

• Empirically developed Drag Coefficients, array

W _B /W _o		2 to 4		5		6		7		8				
W ₁ /W _o			0.57		0.63		0.6		0.58		0.62			
R	Rows (N	√r)	4	5	6	4	5	6	4	5	6	5	6	6
Elements (N)		14	17	21	15	19	23	17	22	27	24	30	30	
≌ h/y _A L/h						Basin Drag Coefficient, C _B								
BUL	0.91	6	0.32	0.28	0.24	0.32	0.28	0.24	0.31	0.27	0.23	0.26	0.22	0.22
ANC	0.71	6	0.44	0.40	0.37	0.42	0.38	0.35	0.40	0.36	0.33	0.34	0.31	0.29
CT	0.48	12	0.60	0.55	0.51	0.56	0.51	0.47	0.53	0.48	0.43	0.46	0.39	0.35
R	0.37	12	0.68	0.66	0.65	0.65	0.62	0.60	0.62	0.58	0.55	0.54	0.50	0.45
	0.91	6	0.21	0.20	0.48	0.21	0.19	0.17	0.21	0.19	0.17	0.18	0.16	
AR	0.71	6	0.29	0.27	0.40	0.27	0.25	0.23	0.25	0.23	0.22	0.22	0.20	
cul	0.31	6	0.38	0.36	0.34	0.36	0.34	0.32	0.34	0.32	0.30	0.30	0.28	
CIR	0.48	12	0.45	0.42	0.25	0.40	0.38	0.36	0.36	0.34	0.32	0.30	0.28	
	0.37	12	0.52	0.50	0.18	0.48	0.46	0.44	0.44	0.42	0.40	0.38	0.36	

Table 9.1. Design Values for Roughness Elements

Layout Configurations



Figure 9.3. Roughness Configurations Tested

		Annual of a serie y a store spyroet	n to the rough was even and provide when when a comparation.			
2(W)) =	16	two culvert widths (ft) [distance	from end of culvert to first row of elements]			
Fransit exit Now conditions	1.100	Foundary 4.1 (for bound)	× 145, 030			
U U U U U U U U U U U U U U U U U U U	0.102	Equation 41 for odivest	= 1.65 - 0.071 = 1.65 - 0.45 ObjeC			
×2×0-	-0.181	Equation a 2 (for circular pipes)				
×**	17,88	velocity at curvert outer (10.5) [if	circular pipe is being utilized PLEASE, revise tormula for V _10 account for this chang			
F	or 4 < W _o /W, +	8, read y, from Figure 4.3 (Rectan	gular) or 4.4 (Circular).			
	1,526					
	1.0'8					
¥~7, *	0.23	obtain from Figure 4.3 (average	depth for abrupt expansion below rectangular culvert butlet			
уд =	0.69	approach flow average depth (fl	9			
Step 4. F	or the trial roug	hness height to depth ratio h/y $_A$ and	nd length to height ratio determine dissipator parameters from Table 9.1.			
a. h = $(h/y_A)y_A =$	0.7	roughness element height (ft)				
b. L = (L/h)h =	2.1	spacing between rows of eleme	nts (ft)			
c. $W_B = (W_B M V_0) W_0 =$	36	width of basin (ft)				
d. $W_1 = (W_1 M V_0) W_0 =$	4	element width (ft)	4 (ft) - rounded value			
e. u _E = 4/7 + 10L/(7W _o) = 0.94		divergence	1 rounded value			
f. C ₀ =	0.4	basin drag coefficient (from Tab	le 9.1]			
g. A _c = W, h =	2.76	roughness element frontal area	(R ⁺)			
h. C _a =	0.7	from Figure 9.4 [energy and mo	mentum coefficients for rectangular culverts)			
1. Lo = 2Wa + LNL =	22.2	Total basin length (ft)				
Stan 6	the normal i	for conditions and solve For 0.11	by C . A . N and company to C . A . N for basis			
	alculated C - A	-N for hasin parameters for hasin	ar o profil and compare to o profil for sealar.			
Calculate C-A-N from Equation 5	k1	The set second period and set we will be				
Since W ₂ =	36	(II) compare the downstream ch	annal width 36 (ft) to trial basin using option 1			
v =	3.09	Downstream (#) ITM	anne man bo (i) to ear bear a any aport i.			
V ₀ = Q/(W ₁) =	3.2	Velocity of the basin (fb/s)				
Equation 9.1 = a	V. 0+Cv. ² W	12=C.A.NoV.2/2+oV.Ot-Q2//2V.2V	Y-)			
Terms with V _o and y _o :	12048.5	$= \rho V_0 Q + C_{\mu} \gamma y_0^* W_0 / 2$	p = density of water = 1.94 slugs/tt ⁻¹			
Terms with Vp.	12984.6	$- \rho V_0 Q_1 Q_1 Q^2 / (2 V_0^2 W_0)$	y = unit weight of water = 62.4 lbs/tt ⁻¹			
Terms with CpArN is CpArN:	310,2	$= (\rho V_{\pm}^{2}/2)$				
C ₁ A ₁ N =	-3.0					
C	alculate CoArN	I for basin based on parameters del	termined in steps 2 and 4 ((N ,="X", C;;""X", A;="X" #")).			
	sing these valu	es: C ₀ A ₀ N = 13.	25			
Basin resistance test:	Basin Sufficie	- If "Revise Basin" is required n	evise the values located within Step 2.			
Non #	and a lower of	- If "Basin Sufficient, Resistanc	e of Dissipator Greater than Forces on it.			
Step c. V	5 00	ion to roughness element height is	i berween the larger range of 2 to o.			
44/45 =	0.80					
	Step 3. D	etermine flow o	condition V $_{\rm A}$ and y $_{\rm A}$ at the approach	to the roughness element field (two culvert widths downstream).		
--	--	---	--	---	--	--
Transit with V_{n} (V_{n}	2(W ₆) =	16 two culvert widths (ft) [distan		om end of culvert to first row of elements]		
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	Transit exit flow conditions					
$V_{n}V = 0.181 \text{Equation 4.2 (for creater pipes)} = 1.85 - 0.45 G/vgD^2$ $V_{n} = 1.7.89 \text{velocity at culvert outlet (Mt) [If circular pipes is being utilized PLEASE revise formula for V A to account for this dwater for 4 < W0/W, < 8, ready, from Figure 4.3 (Rectangular) or 4.4 (Circular). Fr = 1.528 L = 1.078 V/s = 0.23 go datin from Figure 4.3 (average depth for abrupt expansion below rectangular culvert outlet] V/s = 0.89 approach flow average depth (ft) Step 4 To the trial roughness height to depth ratio hy A and length to height ratio determine dissipator parameters from Table 9.1 a. h = (My)_{N/s} = 0.27 roughness incoments (ft) L = (Mh) = 2.11 spacing between rows of elements (ft) L = (Mh) = 2.11 spacing between rows of elements (ft) C. W0 = (W0/W0), 84 divergence 1 roughness (ft) L = 4.77 + 10L/(7W0) = 0.84 divergence 1 rounded value L = C = 0.44 basin drag coefficient [from Table 9.1] K = 2.76 roughness element hoft area (ft) K = 0.7 Boom Figure 9.4 lensergy and momentum coefficients. for rectangular culverts] L = 2.75 To congenous element form Table 9.1 K = 2.76 To roughness element form the side normal flow constituent for the size (ft) K = 0.7 Boom Figure 9.4 lensergy and momentum coefficients. for rectangular culverts] L = 2.76 To congenous element form and end (ft) K = 2.76 To congenous element form and end (ft) K = 2.76 To congenous element form and end (ft) K = 2.76 To congenous element form and end (ft) K = 0.92 U/W_{V/N} = 3.2 Velocity of the basin (ft) K = 0.92 U/W_{V/N} = 3.2 Velocity of the basin (ft) K = 0.92 U/W_{V/N} = 0.92 U/W_{V/N$	V _o Vo =	1.192	Equation 4.1 (for boxes)	= 1.65 - 0.3Fr		
$V_{n} = 17.89 \text{velocity at cultert outlet (this) [If circular pipe is being utilized PLEASE revise formula for V_A to account for this det For 4 < W_{n}W_{n} < 8, ready, from Figure 4.3 (Rectangular) or 4.4 (Circular). Fi = 1.008 U_{n} = 0.23 obtain from Figure 4.3 (average depth for abrupt expansion below rectangular cultert outlet] U_{n} = 0.89 approach flow average depth for abrupt expansion below rectangular cultert outlet] U_{n} = 0.89 approach flow average depth (th) Step 4 For the trial roughness beinght to depth ratio hy A, and length to height ratio determine dissipator parameters from Table 9.1. a. h = (hy_{n})_{N} = 0.7 roughness teement height (t) U_{n} = 0.4 beach day of the depth ratio determine dissipator parameters from Table 9.1. C. U_{0} = (V_{0}V_{0}V_{0}V_{0}V_{0}) = 0.84 divergence 1 rounded value E. U_{0} = 4/7 + 10U(TW) = 0.94 divergence 1 rounded value E. U_{0} = 4/7 + 10U(TW) = 0.94 divergence (t) D_{0} = 0.4 beach days coefficient (f) D_{0} = 0.4 beach days deficient for traited avea (f) D_{0} = 0.4 beach days deficient (f) D_{0} = 0.4 beach da$	V_/Vo =	-0.181	Equation 4.2 (for circular pipes)	= 1.65 - 0.45 Q/vgO		
$Fr 4 + W_{n} < 8, ready, from Figure 4.3 (Rectangular) or 4.4 (Circular). Fr = 1.528 V_{n} = 0.23 obtain from Figure 4.3 (average depth for abrupt expansion below rectangular culvent outlet(V_{n} = 0.23 obtain from Figure 4.3 (average depth for abrupt expansion below rectangular culvent outlet(V_{n} = 0.23 obtain from Figure 4.3 (average depth for abrupt expansion below rectangular culvent outlet(V_{n} = 0.23 obtain from Figure 4.3 (average depth for bright ratio determine dissipator parameters from Table 9.1 e. the (thy) V_{n} = 0.7 roughness depth (to height ratio determine dissipator parameters from Table 9.1 E. (the (thy)) = 0.1 spacing between rough of elements (ft) b. t = (thy) V_{n} = 0.7 roughness dement height (to the value e. up = 47 + 100 (TW) = 0.44 divergence 1 rounded value e. up = 47 + 100 (TW) = 0.44 divergence 1 rounded value f. C_{0} = 0.7 from Figure 9.4 (none conditions and solve Equ. 9.1 for C _{0.4}, N and compare to C _{0.4}, N for basin. Cabulated C _{0.4}, N for basin parameters for basin resistance. Cabulated C _{0.4}, N for basin parameters for basin resistance. Cabulated C _{0.4}, N for basin parameters for basin resistance. Cabulated C _{0.4}, N for basin parameters for basin resistance. Cabulated C _{0.4}, N for basin parameters for basin resistance. Cabulated C _{0.4}, N for basin parameters for basin resistance. Cabulated C _{0.4}, N for basin parameters for basin resistance. Cabulated C _{0.4}, N for basin parameters for basin fresistance. Cabulated C _{0.4}, N for basin parameters for basin fresistance. Cabulate C _{0.4}, N for basin based on parameters for basin fresistance. Cabulate C _{0.4}, N for basin based on parameters for basin resistance. Cabulate C _{0.4}, N for basin based on parameters for basin terms with V_{0.4} and V_{0.4} $	V _A =	17.88	velocity at culvert outlet (ft/s) [If o	ar pipe is being utilized PLEASE revise formula for V $_{\rm A}$ to account for this change]		
$ \begin{array}{cccc} F_{1} & 1.533 \\ Y_{1} & 0.23 \\ Y_{2} & 0.69 \end{array} dots in from Figure 4.3 [swerage depth for abrupt expansion below rectangular culvent outlet] \\ Y_{2} & 0.69 \qquad approach flow average depth (ft) \\ \hline \\ Step 4 \qquad For the trial roughness beight to depth ratio by y, and length to height ratio determine dissipator parameters from Table 9.1 \\ a. h= (bhy_{3}y_{1}, = 0.7) \qquad roughness element height (ft) \\ b. L= (U/h)^{1} = 0.1 \qquad spacing between rows of elements (ft) \\ c. W_{3} = (W,W,W,W_{3}, = 36) \qquad width of basin (ft) \\ d. W_{4} = (W_{2} = 447 + 10U/(W_{2}) = 0.84 \qquad divergence 1 \qquad rounded value \\ f. C_{6} = 0.4 \qquad basin drag coefficient (ftom Table 9.1) \\ g. A_{4} = W_{4} = 0.7 \qquad from Figure 9.4 [secargy and momentum coefficients for rectangular culvents] \\ h. C_{6} = 0.7 \qquad from Figure 9.4 [secargy and momentum coefficients for rectangular culvents] \\ h. C_{6} = 0.7 \qquad from Figure 9.4 [secargy and momentum coefficients for rectangular culvents] \\ h. C_{6} = 0.7 \qquad from Figure 9.4 [secargy and momentum coefficients for rectangular culvents] \\ h. C_{6} = 0.7 \qquad from Figure 9.4 [secargy and momentum coefficients for rectangular culvents] \\ h. C_{7} = 0.04 \qquad basin drag coefficient (ftom Table 9.1] \\ g. A_{7} = VW_{7} + UV_{7} = 222 \qquad Total basin length (ft) \\ Step 5 \qquad Calculated C_{1}A_{1} N for basin parameters for basin resistance. \\ Calculates C_{7}A_{1} N for basin parameters for basin measurement. Calculated C_{1}A_{2} N for basin. \\ Calculates 0.4 \qquad Y_{1} = 3.09 \qquad Downstream (ft) [TW] \\ V_{1} = 0.0W_{1}(y_{1}) = 3.2 \qquad Velocity of the basin (ft) \\ Terms with V_{9}$ and $Y_{1} = 12948.5 \qquad - pV_{1}(O_{1}C_{1}Y_{1}^{2}W_{2}O_{2} \qquad p = density of water = 1.94 suggift3 \\ Terms with V_{9}$ and $Y_{1} = 12948.5 \qquad - pV_{1}(O_{1}C_{1}Y_{1}^{2}W_{2}O_{2} \qquad p = density of water = 62.4 \ busit^{3} \\ Terms with V_{9}$ and $Y_{1} = 12948.5 \qquad - pV_{1}(O_{1}C_{1}Y_{1}^{2}W_{2}O_{2} \qquad p = density of water = 62.4 \ busit^{3} \\ Terms with V_{9}$ and $Y_{1} = 12948.5 \qquad - pV_{1}(O_{1}C_{1}Y_{1}^{2}W_{2}O_{2}O_{2}W_{2}W_{2}O_{2}W_{2$	Fe	or 4 < W_W, <	8, read y, from Figure 4.3 (Rectang	ular) or 4.4 (Circular).		
$ \begin{array}{cccc} L = & 1.0^{18} \\ y/y = & 0.23 \\ y/y = & 0.23 \\ y/y = & 0.89 \\ approach flow average depth for abrupt expansion below rectangular culvent outlet() \\ y/y = & 0.89 \\ approach flow average depth (ft) \\ \hline \\ Step 4 \\ a. h = (h/y)y_y = & 0.7 \\ roughness beight to depth ratio hy , and kingth to height ratio determine dissipator parameters from Table 9.1. \\ a. h = (h/y)y_y = & 0.7 \\ roughness dement height (ft) \\ b. L = (Un)h = & 2.1 \\ spacing between rows of elements (ft) \\ d. W_1 = (W_1,W_2,W_2,W_3,W_4 = 4 \\ element width (ft) & 4 (t) - rounded value \\ f. C_0 = & 0.4 \\ 0.4 \\ y. A = W, h = & 2.76 \\ roughness dement height (ft) \\ f. C_0 = & 0.7 \\ h. C_0 = & 0.7 \\ f. C_0 = & 0.7 \\ h. C_0 = & 0.7 \\ h. C_0 = & 0.7 \\ h. C_0 = & 0.7 \\ f. C_0 = & 0.4 \\ f. C_0 = & 0.4 \\ f. C_0 = & 0.4 \\ f. C_0 = & 0.7 \\ h. C_0 = & 0.7 \\ f. C_0 = & 0.7 \\ f. C_0 = & 0.7 \\ h. C_0 = & 0.7 \\ f. C_0 = & 0.7 \\ h. C_0 = & 0.8 \\ h. D = & 0.8 \\ h. $	Fr =	1.526				
$y_{n}^{2} = 0.23 obtain from Figure 4.3 [average depth for abrupt expansion below rectangular culvent outlet] y_{n} = 0.23 obtain from average depth (%) Step 4 . For the thail roughness height to depth ratio hy , and length to height ratio determine dissipator parameters from Table 9.1. a. h = (hy)_{N} = 0.7 roughness height to depth ratio hy , and length to height ratio determine dissipator parameters from Table 9.1. a. h = (hy)_{N} = 0.7 roughness height to depth ratio hy , and length to height ratio determine dissipator parameters from Table 9.1. b. L = (Un)h = 2.1 spacing between rows of element height (h) b. L = (Un)h = 2.4 spacing between rows of element to (%) c. W0 = (W0W0W0W0 = 4 element width (f) 4 (%) - rounded value e. u0 = 4/7 + 10U(TW0) = 0.54 divergence 1 rounded value f. C0 = 0.4 besin drag coefficient (from Table 9.1) y_{n} = 2.76 no coefficient (from Table 9.1) y_{n} = 2.77 for nonghness teement from table 9.1 y_{n} = 0.7 for nonghness teement from table 9.1 for C 0A, N and compare to C 0A, N for basin. Calculate C 0A. N for basin parameters for basin resistance. Calculate C 0A. N for basin parameters for basin resistance. Calculate C 0A. N for basin parameters for basin resistance. Calculate C 0A. N for basin parameters for basin resistance. Calculate C 0A. N for basin parameters for basin resistance. Calculate C 0A. N for basin parameters for basin resistance. Calculate C 0A. N for basin parameters for basin resistance. Calculate C 0A. N for basin parameters (h) TW] V0 = 0(W0(y) = 3.2 Velocity of the basin (ht): Equation 9.1 = pV_0C+C_yY_0^{-1}(XV_0^{-1}(XV_0^{-1}W_0) y = unit weight of water = 1.94 stuggift3 Terms with V0 and y0 = 1204.5 = pV_0C+C_yY_0^{-1}(XV_0^{-1}W_0) y = unit weight of water = 62.4 thult2 Terms with C 0A. N is C 0A. N for basin based on parameters determined in steps 2 and 4 ((N, **X', C_0**X', A, **X' *1)). Using these values: C 0A. N = 13.25 Basin resistance tat. Explore the sum t$	L= 1.0'B					
$y_{A} = 0.69 \text{approach flow average depth (ft)}$ Step 4. For the trail roughness height to depth ratio by _A and length to height ratio determine dissipator parameters from Table 9.1. a. h = (hy)_{y_{A}} = 0.7 roughness element height (ft) b. L = (U/h) = 2.1 $\text{spacing between rows of elements (ft)}$ c. $W_{b} = (W_{c}W_{c}W_{c}W_{c}W_{c}W_{c}W_{c}W_{c}$	y.dy, =	y,/y, = 0.23 obtain from Figure 4.3 [average depth for abrupt expansion below rectangular culvert outlet]				
Step 4 For the trial roughness height to depth ratio My and length to height ratio determine dissipator parameters from Table 9.1. a. h = (My,3)x, = 0.7 roughness element height (ft) b. L = (L/h)h = 2.1 spacing between rows of elements (ft) c. W_a = (Me,W_A,W_A,W_a) 36 width of basin (ft) d. W, = (W,W_A,W_A,W_a) 4 element width (ft) 4 (ft) - rounded value e. u_g = 477 + 10L/(TW_a) = 0.94 divergence 1 rounded value f. C_g = 0.4 basin diag coefficient [from Table 9.1] g. A = W, h = 2.75 f. C_g = 0.7 from Figure 9.4 [energy and momentum coefficients for rectangular culverts] 1. L = 2W, + LL = 2.22 I. L = 2W, + LL = 2.22 Total basin length (ft) 35 (ft) to trial basin using option 1. y = 3.5 (ft) compare the downstream channel width 36 (ft) to trial basin using option 1. y = 3.6 (ft) compare the downstream channel width 36 (ft) to trial basin using option 1. y = 3.2 Velocity of the basin (ft/s) 1204.5 - pV,0+C_yW,^3W/2 p = density of water = 1.94 slugs/ft ² Terms with V_s and y : 1204.5 - pV,0+C_yW,^3W/2 p = density of wat	у _А =	0.69	approach flow average depth (ft)			
a. h = (h/k)/yk = 0.7 roughness element height (f) b. L = (L/h)h = 2.1 spacing between rows of elements (f) c. W ₂ = (W ₂ /W ₂)/W ₂ = 36 width of basin (f) d. W ₁ = (W ₁ /W ₂)/W ₂ = 4 element width (f) 4 (f) - rounded value e. u _g = 47 + 10L/(7W) = 0.94 divergence 1 rounded value f. C ₀ = 0.4 basin diag coefficient (form Table 9.1) g. A ₁ = V(h = 2.76 roughness element borital area (f ¹) h. C ₂ = 0.7 Bron Figure 9.4 (energy and momentum coefficients for rectangular culverts) 1 L _g = 2W ₁ + L ₄ = 22.2 Total basin length (f) Step 5 Use the normal flow conditions and solve Equ 9.1 for C (A / N and compare to C (A / N for basin Calculated C (A / N for basin parameters for basin resistance. Calculated C (A / N for basin parameters for basin resistance. Calculated C (A / N for basin parameters for basin resistance. Calculated C (A / N for basin parameters for basin resistance. Calculated C (A / N for basin parameters for basin resistance. Calculated C (A / N for basin 0.1 y = 3.0 Downstream (f) (TW) V ₈ = 0(W ₁ W ₂) = 3.2 Velocity of the basin (ft) Equation 9.1 = pV_0C+C ₁ Y ₂ /W ₁ /2-C ₀ A/ ₁ N g/A ² /2+pV ₁ Q+Q ² /(2V ₂ ² W ₀) Terms with V ₄ and y ₄ : 12048.5 - pV ₄ O+C ₁ Y ₂ ² (V/2 ²) C (A N = 3.0 Calculate C ₁ A/N for basin based on parameters determined in steps 2 and 4 ((N = "X", C ₁ ="X", A ="X", F")). Using these values: C ₁ (A N = 13.25 Basin resistance text Element Sufficient is required revises the values located within Step 2. - If "Basin Sufficient is required revises the values located within Step 2. - If "Basin Sufficient is required revises the values located within Step 2. - If "Basin Sufficient is interpart range of 2 to 3. W ₁ /4 = 5.80	Step 4. Fo	or the trial roug	hness height to depth ratio h/y $_{\rm A}$ and	d length to height ratio determine dissipator parameters from Table 9.1.		
b. $l = (Jn)h = 2.1$ spacing between rows of elements (ft) c. $W_0 = (W_0N/W_0)W_0 = 36$ width of basin (ft) d. $W_0 = (M_0N/W_0)W_0 = 4$ element width (ft) 4 (ft) - rounded value e. $u_E = 477 + 10L/(7W_0) = 0.94$ divergence 1 rounded value f. $C_0 = 0.4$ basin drag coefficient (from Table 9.1] g. $A_r = W_r$ he = 2.76 coefficient (from Table 9.1] g. $A_r = W_r$ he = 2.77 from Figure 9.4 (energy and momentum coefficients, for rectangular culverts) h. $C_0 = 0.7$ from Figure 9.4 (energy and momentum coefficients, for rectangular culverts) h. $L_0 = 2W_r + DA = 22.2$ Total basin length (ft) Step 5 Use the normal flow conditions and solve Equ. 9.1 for C (A, N and compare to C (A, N for basin. Calculated C (A, N for basin parameters for basin resistance. Calculated C (A, N for basin parameters for basin resistance. Calculated C (A, N for basin parameters for basin resistance. Calculated C (A, N for basin parameters for basin (ft)) $W_0 = Ol(W_0)$, $= 3.2$ Velocity of the basin (ft)) Equation 9.1 = $\rho V_0 C_0 T V_0 V_0 V_0 V_0 V_0 V_0 V_0 V_0 V_0 V_0$	a. h = (h/y _A)y _A =	0.7	roughness element height (ft)			
c. W ₀ = (W ₀ /W ₀)W ₀ = 36 width of basin (ft) d. W ₁ = (W ₁ /W ₁)W ₀ = 4 element width (ft) 4 (ft) - rounded value e. u ₀ = 4/7 + 10U/(W ₀) = 0.94 divergence 1 rounded value f. C ₀ = 0.4 basin drag coefficient (from Table 9.1) g. A ₀ = W ₁ h = 2,76 roughness element frontal area (ft ⁻) h. C ₀ = 0.7 from Figure 9.4 (energy and momentum coefficients for rectangular culverta) 1. U ₀ = 2V6 + U ₀ = 22.2 Total basin length (ft) Step 5 Use the normal flow conditions and solve Equ. 9.1 for C (ft A ₁ N and compare to C (ft A ₁ N for basin Calculate C (ft A ₁ N for basin parameters for basin resistance. Calculate C (ft A ₁ N for basin parameters for basin resistance. Calculate C (ft A ₁ N for basin parameters for basin resistance. Calculate C (ft A ₁ N for basin parameters for basin resistance. Calculate C (ft A ₁ N for basin parameters for basin resistance. Calculate C (ft A ₁ N for basin parameters for basin resistance. Calculate C (ft A ₁ N for basin for basin formation (ft) V ₀ = 0.0(W ₁) ₀ = 3.2 Velocity of the basin (ft) V ₀ = 0.0(W ₁) ₀ = 3.2 Velocity of the basin (ft) Terms with V ₀ and y ₀ : 1204.5 - ρV/(2 + Q ² /(2 + Q ²)/(2 + Q	b, L = (L/h)h =	2.1	spacing between rows of elements (ft)			
d. W ₁ = (W ₁ , W ₂)W ₂ = 4 element width (ft) 4 (ft) - rounded value e. u _E = 47 + 10L(7W, 0) = 0.94 divergence 1 rounded value 1. C ₀ = 0.4 basin drag coefficient [from Table 9.1] 9. A ₁ = W ₁ + 104 2.76 roughness element bortal area (ft ⁻¹) h. C ₀ = 0.7 from Figure 9.4 [energy and momentum coefficients for rectangular culverts] 1. L ₀ = 2W ₀ + 104 22.2 Total basin length (ft) Step 5 Use the normal flow conditions and solve Equ. 9.1 for C (ft A, N and compare to C (ft A, N for basin. Calculated C (ft A, N for basin parameters for basin resistance. Calculate C ₀ A ₀ N for basin parameters for basin resistance. Calculate C ₀ A ₀ N for basin parameters for basin resistance. Calculate C ₀ A ₀ N for basin parameters for basin resistance. Calculate C ₀ A ₀ N for basin parameters for basin resistance. Step 5 Use the normal flow conditions and solve Equ. 9.1 for C (ft A, N and compare to C (ft A, N for basin using option 1. y ₁ = 3.09 Downstream channel width 36 (ft) to trial basin using option 1. y ₁ = 3.09 Downstream (ft) [TW] Terms with V ₀ and y ₀ : 12048.5 <td>c. $W_B = (W_B M V_0) W_0 =$</td> <td>36</td> <td>width of basin (ft)</td> <td></td>	c. $W_B = (W_B M V_0) W_0 =$	36	width of basin (ft)			
e. $u_e = 4/7 + 10L/(7W_e) =$ 0.94 divergence 1 rounded value f. $C_0 =$ 0.4 basin drag coefficient (from Table 9.1) g. A. + W, h 2.76 roughness element fordal area (ft*) h. $C_0 =$ 0.7 from Figure 9.4 (energy and momentum coefficients for rectangular culverts) i. L_0 = 2W_0 + UA = 22.2 Total basin length (ft) Step 5 Use the normal flow conditions and solve Equ. 9.1 for C (A, N and compare to C (A, N for basin. Calculated C (A, N for basin parameters for basin resistance. Calculate C_0A, N form Equation 9.1 Since W ₀ = 36 (ft) compare the downstream channel width 36 (ft) to trial basin using option 1. y. a 3.09 Downstream (ft) [TW] 32 Velocity of the basin (ft/s) Equation 9.1 = pV_0C+C_07y_0^2W_0/2=C_0A_1NpV_0^2/2+pV_0C+Q^2/(2V_0^2W_0) p = density of water = 1.94 sluguft ³ Terms with V_a and y: 1204.5 $-pV_0C+C_07y_0^2/(2V_0^2W_0)$ $y = unit weight of water = 62.4 (bs/ft-1) C_0A, N is C_0A, N is 1296.4.5 -pV_0C+C_07y_0^2/(2V_0^2W_0) y = unit weight of water = 62.4 (bs/ft-1) Terms with V_a and y: 1296.4.5 -pV_0C+C_07y_0^2/(2V_0^2W_0) y = unit weight of water = 62.4 (bs/ft-1) C_0A, N is 0.2 = (pV_0^2/C_0^2) C_0^2A_N = -$	d. $W_1 = (W_1 M V_0) W_0 =$	4	element width (ft)	4 (ft) - rounded value		
$ \begin{array}{cccc} f. G_{0} & 0.4 & \text{basin drag coefficient [from Table 9, 1]} \\ g. A_{+} = W_{+} h_{+} & 2.76 & \text{roughness element fondal area (ft^{+})} \\ h. C_{0} & 0.7 & \text{from Figure 9.4 [energy and momentum coefficients for rectangular culverts]} \\ f. U_{0} = 2W_{0} + 10.4 & 22.2 & \text{Total basin length (f)} \\ \end{array} $ Step 5 & Use the normal flow conditions and solve Equ. 9.1 for C $_{0}A_{+}N$ and compare to C $_{0}A_{+}N$ for basin. Calculated C $_{0}A_{+}N$ for basin parameters for basin resistance. Calculated C $_{0}A_{+}N$ for basin parameters for basin resistance. Calculated C $_{0}A_{+}N$ for mEquation 9.1 $& \text{Since W}_{0} = & 36 & (ft) compare the downstream channel width & 36 (ft) to trial basin using option 1. & y_{+} = & 3.09 & \text{Downstream (ft) [TM]} \\ V_{0} = O(W_{0}y_{*}) = & 3.2 & Velocity of the basin (ft)s \\ \hline \textbf{Equation 9.1 = } pV_{*}Q^{4}C_{*}yy_{*}^{3}W_{*}/2=C_{*}A_{*}Ny_{*}/2+pV_{*}Q^{4}(2V_{0}^{2}W_{0}) \\ \hline \textbf{Terms with } V_{0} and y_{+} 12948.5 - pV_{0}O_{+}Q^{2}/(2V_{0}^{2}W_{0}) \\ \hline \textbf{Terms with } V_{0} 12948.6 - pV_{0}O_{+}Q^{2}/(2V_{0}^{2}W_{0}) \\ \hline \textbf{Terms with } V_{0} Since C_{0}A_{+}N for basin based on parameters determined in steps 2 and 4 ((N, **X^{*}, C_{0}*X^{*}, A_{*}*X^{*}f^{2})). \\ Using bases values: C_{0}A_{+}N for basin based on parameter divise the values located within Step 2. - H^{*}Basin resistance test. How with the roughness element is the values of C is step to the forces on it. Step 5 \\ W_{*}A_{+} = 580 \\ \hline \textbf{Verify element with the to roughness element height is between the larget range of 2 to 8. \\ W_{*}A_{+} = 580 \\ \hline \textbf{Verify element with the force of the forces on the forces on it. } \\ \hline Verify element with the forces of the force of the step transe of D is step to the forces on it. \\ \hline \textbf{Verify element with the force of the force of the step transe of 2 to 8. \\ \hline \textbf{Verify element with the force of the force of the step transe of 2 to 8. \\ \hline \textbf{Verify element with the force of the formeter tof the formeter tof the force of 2 to 8. \\ \hline \textbf{Verify eleme$	e.u _E = 4/7 + 10L/(7W _e) =	0.94	divergence	1 rounded value		
g. A., = W, h = 2.76 roughness element fortal area (k*) h. C., = 0.7 from Figure 9.4 (energy and momentum coefficients, for rectangular culverts) 1. Le, = 2W, + UA, = 22.2 Total basin length (ft) Step 5 Use the normal flow conditions and solve Equ. 9.1 for C 6.4. N and compare to C 8.4. N for basin. Calculated C 9.4. N for basin parameters for basin resistance. Calculate CoA+N from Equation 9.1 Size 9.5 Use the normal flow conditions and solve Equ. 9.1 for C 6.4. N and compare to C 8.4. N for basin. Calculate C 9.4. N for basin parameters for basin resistance. Calculate C 9.4. N for basin parameters for basin resistance. Calculate C 9.4. N for basin parameters for basin resistance. Calculate C 9.4. N for basin parameters for basin resistance. Size With (0) Size With (0) Velocity of the basin (ft) Equation 9.1 = pV_0+C 9.79. ² W /2 C 9.4 C 9.19. ² W /2 p = density of water = 1.94 slugalt ³ Terms with V ₀ and y. 12048.5 = pV_0+Q^2/(2V_0 ² W_0) y = unit weight of water = 62.4 bas/ft ³ Terms with V ₀ and y. 12048.5 = pV_0+Q^2/(2V_0 ² W_0) y = unit weight of water = 62.4 bas/ft ³	f. C ₀ =	0.4	basin drag coefficient (from Table 9.1)			
h. C_s * 0.7 from Figure 9.4 (energy and momentum coefficients for rectangular culverts) 1, L_g = 2W_g + UX * 22.2 Total basin length (f) Step 5 Use the normal flow conditions and solve Equ. 9.1 for C $_{0}A_{i}N$ and compare to C $_{i}A_{i}N$ for basin. Calculated C $_{0}A_{i}N$ for basin parameters for basin resistance. Calculate C_0A_N from Equation 9.1 Since W ₀ = 36 (ft) compare the downstream channel width 36 (ft) to trial basin using option 1. y _i = 3.09 Downstream (ft) [TW] 32.2 Velocity of the basin (tris) Equation 9.1 = pV_oPC_pry_2^{N}W_j/2=C_0A_iNpV_A^{1/2}PV_sQ+Q^2/(2V_s^{N}W_0) p = density of water = 1.94 slugs/ft ³ Terms with V ₀ and y ₀ : 12048.5 $pV_0Q+Q_2/(2V_0^{2}W_0)$ y = unit weight of water = 62.4 lbs/ft ³ Terms with V ₀ is C_0A_N is C_0A_N is 310.2 $p(V_0^{1/2}/2)(2V_0^{1/2}W_0)$ y = unit weight of water = 62.4 lbs/ft ³ Terms with C_0A_N is C_0A_N is C_0A_N is Dib basin based on parameters determined in steps 2 and 4 ((N = *X*, C_0*X*, A = *X* ft ²)). Using these values: $C_{ij}A_i N = 13.25$ Basin resistance test: Easin Sufficient. Resistance of Dissiptor Greater than Forces on it. Verify element width to roughness element height is between the target range of 2 to 3. W ₀ /ft = 5.80 Verify element width to roughness element height is between the target range of	g. A ₂ = W, h =	2.76	roughness element frontal area (R*)			
I. Let = 2W, + UA = 2.2 Total basin length (f) Step 5. Use the normal flow conditions and solve Equ. 9.1 for C (A, N and compare to C (A, N for basin. Cabulated C (B, A, N for basin parameters for basin resistance. Calculate C_0A, N from Equation 9.1 Since W ₀ = 35 (f) compare the downstream channel width 36 (f) to trial basin using option 1. y, = 3.09 Downstream (f) [TW] 32 Velocity of the basin (ft/s) Equation 9.1 = pV_0C+C_py_s ² W_0/2=C_0A, NpV_a ⁷ /2+pV_0C+y ² /(2V_b ² W_0) p = density of water = 1.94 slugalt ³ Terms with V_o and y_: 1204.5 $pV_0C+C_py_s^{2}W_0/2$ p = density of water = 52.4 its/f ³ Terms with V_o: 12994.6 $pV_0C+C_p(2/2)^2W_0$ y = unit weight of water = 62.4 its/f ³ Terms with V_o: 12994.6 $pV_0C+C_p(2/2)^2W_0$ y = unit weight of water = 62.4 its/f ³ Terms with C_0A, N is C_0A N: 310.2 $p(V_0A^2/2)$ C_0A N = Calculate C_0A/N for basin based on parameters determined in steps 2 and 4 ((N ,**X*, C_0**X*, A,**X* f ²)). Using these value: C $pA N =$ Step 6 Verify element width to roughness element height is between the values located within Step 2. - If "Basin Sufficient, Resistance of Dissipator Greater than Forces on it. Wi, th = 5.80 Step 4.	h. C., =	0.7	from Figure 9.4 [energy and momentum coefficients for rectangular culverts]			
Step 5. Use the normal flow conditions and solve Equ. 9.1 for C $_{0}A_{1}N$ and compare to C $_{0}A_{1}N$ for basin. Calculate $C_{0}A_{1}N$ for basin parameters for basin resistance. Calculate $C_{0}A_{1}N$ from Equation 9.1 Since $W_{0} = 36$ (t) compare the downstream channel width 36 (t) to trial basin using option 1. $y_{n} = 3.09$ Downstream (t) [TW] $V_{0} = O(W_{0}v_{1}) = 3.2$ Velocity of the basin (this) Equation 9.1 = $pV_{n}Q+C_{p}y_{n}^{2}W_{n}/2=C_{0}A_{1}NpV_{n}^{2}/2+pV_{0}Q^{2}/(2V_{0}^{2}W_{0})$ $p = density of water = 1.94$ slugs/t ³ Terms with V_{0} and y_{0} : 12948.6 $-pV_{0}O+C_{0}y_{0}^{2}W_{0}/2$ $p = density of water = 62.4 lbs/t4 Terms with C_{0}A_{1}N is C_{0}A_{1}N: 310.2 = (pV_{n}^{2}/2)C_{0}A_{1}N is C_{0}A_{1}N: 310.2 = (pV_{n}^{2}/2)C_{0}A_{1}N is C_{0}A_{1}N for basin based on parameters determined in steps 2 and 4 ((N, **X^{*}, C_{0}*X^{*}, A_{0}*X^{*})).Using these values: C_{0}A_{1}N = 13.25Basin resistance basi.Basin sufficient: P if "Revise Basin" is required revise the values located within Step 2.- 11^{**}Basin Sufficient: A resistance of Dissipator Greater than Forces on it. Step 6 Verity element width to roughness element height is between the larget range of 2 to 3. With P = 5.80 $	1. Lo = 2W0 + LN4 =	22.2	Total basin length (ft)			
Calculate $C_{B}A_{1}N$ for basin parameters for basin resistance. Calculate $C_{B}A_{1}N$ from Equation 9.1 Since $W_{0} = 36$ (ft) compare the downstream channel width 36 (ft) to trial basin using option 1. y, $= 3.09$ Downstream (ft) [TW] $V_{0} = O(W_{0}y_{1}) = 3.2$ Velocity of the basin (ft/s) Equation 9.1 = $\rho V_{n} Q + C_{p} y_{n}^{2} W_{n} / 2 = C_{B} A_{1} N_{P} V_{n}^{2} / 2 + p V_{B} Q + \gamma Q^{2} / (2 V_{B}^{2} W_{B})$ Terms with V_{0} and y_{1} : 12048.5 $-\rho V_{1} Q + \gamma Q^{2} / (2 V_{B}^{2} W_{B})$ Terms with V_{0} : 12984.6 $-\rho V_{1} Q + \gamma Q^{2} / (2 V_{B}^{2} W_{B})$ Terms with V_{0} : 12984.6 $-\rho V_{1} Q + \gamma Q^{2} / (2 V_{B}^{2} W_{B})$ Terms with $C_{0}A_{1}N$ is $C_{0}A_{1}N$: $310.2 = (\rho V_{n}^{2}/2)$ $C_{1}A_{1}N = -3.0$ Calculate $C_{0}A_{1}N$ for basin based on parameters determined in steps 2 and 4 ($(N, *^{*}X^{*}, C_{0} *^{*}X^{*}, A_{1} *^{*}X^{*} f_{1}^{*})$). Using these values: $C_{0}A_{1}N = 13.25$ Basin resistance test: Example Sufficient - If *Revise Basin* is required revise the values located within Step 2. $-I^{*}$ Basin sufficient A step 5.80 With $= 5.80$	Step 5 U	se the normal t	fow conditions and solve Equ. 9.1 fo	r C _AA = N and compare to C _A = N for basin.		
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$\begin{aligned} & \text{Since } W_0 = 36 (\texttt{f}) \text{ compare the downstream channel width} & 36 (\texttt{f}) \text{ to trial basin using option 1.} \\ & y_1 = 3.09 \text{Downstream (\texttt{f}) [TW]} \\ & V_0 = O((W_0y_1) = 3.2 \text{Velocity of the basin (\texttt{ft})s} \end{aligned} \\ & \textbf{Equation 9.1 = } \rho V_o Q + C_p \gamma y_o^3 W_0 / 2 = C_0 A_v N p V_A^2 / 2 + p V_0 Q^2 / (2 V_0^3 W_0) \end{aligned} \\ & \textbf{Terms with } V_o \text{ and } y_o: 12048.5 -\rho V_o Q + C_p \gamma y_o^3 W_0 / 2 \rho = \text{density of water = 1.94 slugs.} \texttt{ft}^3 \\ & \text{Terms with } V_0. 12964.6 -\rho V_0 Q + \gamma Q^2 / (2 V_0^3 W_0) \gamma = \text{unit weight of water = 62.4 lbs.} \texttt{ft}^3 \\ & \textbf{Terms with } V_0. 12964.8 -\rho V_0 Q + \gamma Q^2 / (2 V_0^3 W_0) \gamma = \text{unit weight of water = 62.4 lbs.} \texttt{ft}^3 \\ & \text{Terms with } C_0 A_v N \text{ is } 10.2 = (\rho V_A^2/2) \\ & C_0 A_v N = -3.0 \\ & \text{Calculate } C_0 A_v N \text{ for basin based on parameters determined in steps 2 and 4 ((N , **X^*, C_0 * X^*, A_v * X^*, \texttt{ft}^2)). \\ & \text{Using these values: } C_0 A_v N = 13.26 \\ & \text{Basin resistance test: } \hline \textbf{Basin Bufficient} - \textbf{If "Revise Basin" is required revise the values located within Step 2. \\ & -\textbf{If "Basin Sufficient, Resistance of Dissipator Greater than Forces on it.} \\ & \text{Step 5.} \\ & \text{Verify element width to roughness element height is between the target range of 2 to 3.} \\ & \text{With } = 5.80 \\ \hline \end{array}$	Calculate CoArN from Equation 9	11				
$y_{n} = 3.09 \qquad \text{Downstream (ft) [TW]} \\ V_{0} = O([W_{0} y_{n}]) = 3.2 \qquad \text{Velocity of the basin (ft/s)} \\ \hline \mathbf{Equation 9.1 = pV_{n}Q+C_{p}y_{n}^{2}W_{n}/2=C_{0}A_{n}NpV_{n}^{2}/2+pV_{0}Q+q^{2}/(2V_{0}^{2}W_{0})} \\ \hline \mathbf{Terms with V_{0} and y_{0} = 12048.5 \qquad -pV_{n}Q+C_{p}y_{n}^{2}W_{n}/2 \qquad p = \text{density of water = 1.94 slugs/ft^{-3}} \\ \hline \text{Terms with V_{0} : 12964.6 \qquad -pV_{n}Q+q^{2}/(2V_{0}^{2}W_{0}) \qquad y = \text{unit weight of water = 62.4 lbs/ft^{-3}} \\ \hline \text{Terms with C}_{0}A_{n}N \text{ is } C_{n}A_{n}N \qquad 310.2 \qquad = (pV_{n}^{2}/2) \\ C_{0}A_{n}N = -3.0 \\ \hline \text{Calculate } C_{0}A_{n}N \text{ for basin based on parameters determined in steps 2 and 4 ((N, **X*, C_{0}**X*, A_{0}**X*, ft^{-3})). \\ \hline \text{Using these values: } C_{0}A_{n}N = 13.25 \\ \hline \text{Basin resistance test: } \hline \text{Basin Sufficient, Resistance of Dissipator Greater than Forces on it.} \\ \hline \text{Verify element width to roughness element beight is between the target range of 2 to 8.} \\ \hline \text{Wi,ft} = 5.80 \\ \hline \text{Using these VIDE 14}. \end{aligned}$	Since W ₀ =	36	(ft) compare the downstream cha	nnel width 36 (ft) to trial basin using option 1.		
$V_{0} = O(W_{0}y_{*}) = 3.2 \text{Velocity of the basin (ft/s)}$ Equation 9.1 = $pV_{*}Q+C_{\mu}yy_{*}^{3}W_{\mu}/2=C_{\mu}A_{\mu}NpV_{\mu}^{3}/2+pV_{\mu}Q+yQ^{3}/(2V_{\mu}^{3}W_{\mu})$ Terms with V_{0} and y_{*} : 12048.5 $-pV_{0}Q+C_{\mu}y_{*}^{3}W_{\mu}/2$ p = density of water = 1.94 slugs/ft ⁻³ Terms with V_{0} : 12984.6 $-pV_{0}Q+yQ^{3}/(2V_{0}^{2}W_{0})$ γ = unit weight of water = 62.4 lbs/ft ⁻¹ Terms with $C_{\mu}A_{\mu}N$ is $C_{\mu}A_{\mu}N$: 310.2 $= (pV_{\mu}^{2}/2)$ $C_{\mu}A_{\mu}N = -3.0$ Calculate $C_{0}A_{\mu}N$ for basin based on parameters determined in steps 2 and 4 $((N, **X^{*}, C_{\mu}**X^{*}, A_{\mu}**X^{*}f_{\mu}))$. Using these values: $C_{\mu}A_{\mu}N = 13.25$ Easin resistance test: Basin Sufficient - If *Revise Basin* is required revise the values located within Step 2 If *Basin Sufficient Resistance of Dissipator Greater than Forces on it. Step 5. Verify element width to roughness element height is between the target range of 2 to 8. W, th = 5.80	y. =	3.09	Downstream (t) ITWI			
Equation 9.1 = $pV_sQ+C_{pT}y_s^{-2}W_s/2=C_{p}A_sNpV_s^{-2}/2+pV_sQ+yQ^{2}/(2V_b^{-2}W_b)$ Terms with V ₀ and y ₀ : 12048.5 - $pV_sQ+C_{p}y_s^{-2}W_s/2$ $p = density of water = 1.94 stugs/t^{-3}$ Terms with V ₀ : 12984.6 - $pV_sQ+yQ^{2}/(2V_b^{-2}W_b)$ $y = unit weight of water = 62.4 lbs/t^{-3}$ Terms with C ₀ A ₂ N is C ₀ A ₂ N: 310.2 = $(pV_s^{-2}/2)$ C ₀ A ₂ N = -3.0 Calculate C ₁₀ A ₂ N for basin based on parameters determined in steps 2 and 4 ((N ,="X", C ₀ ="X", A,="X", t ²)). Using these values: C ₁₀ A ₂ N = 13.25 Basin resistance test: Basin Sufficient - If "Revise Basin" is required revise the values located within Step 2. - If "Basin Sufficient, Resistance of Dissipator Greater than Forces on it. Step 6 W ₁ A ₁ = 5.80	$V_{0} = O(W_{0}y_{n}) =$	3.2	Velocity of the basin (ft/s)			
Terms with V ₀ and y ₀ : 12048.5 $pV_0O+C_{p/}(y_0^{-2}W_0/2)$ $p = \text{density of water = 1.94 slugs/t-3}$ Terms with V ₀ : 12984.6 $-pV_0O+qO^2/(2V_0^{-2}W_0)$ $y = \text{unit weight of water = 62.4 lbs/t-3}$ Terms with C ₀ A ₀ N is C ₀ A ₀ N: 310.2 $(pV_0^{-2}/2)$ C ₀ A ₀ N = -3.0 Calculate C ₀ A ₀ N for basin based on parameters determined in steps 2 and 4 ($(N_1 = X^*, C_0 = X^*, A_1 = X^*, T^*)$). Using these values: $C_0A_0N =$ Display these values: $C_0A_0N =$ Using these values: $C_0A_0N =$ Display the event width to roughness element height is between the values located within Step 2. If "Basin Sufficient, Resistance of Dissipator Greater than Forces on it. Step 6 Verify element width to roughness element height is between the target range of 2 to 3. W ₀ /h = 5.80	Equation 9.1 = p	v_Q+C ₂ 3y_ ² W,	/2=C _B A ₆ NpV _A ² /2+pV _B Q+ ₇ Q ² /(2V _B ² W)	a		
Terms with Vp: 12984.6 - pVpQ+pQ ² /(2Vp ² Wp) y = unit weight of water = 62.4 lbs/lt ² Terms with CpA/N is CpA/N: 310.2 = (pVp ² /2) CpA/N = -3.0 Calculate CpA/N for basin based on parameters determined in steps 2 and 4 ((N ,**X*, Cp*X*, A/**X* ft ²)). Using these values: CpA/N = 13.25 Basin resistance test: Elasin Sufficient: - If "Revise Basin" is required revise the values located within Step 2. - If "Basin Sufficient, Resistance of Dissipator Greater than Forces on it. Verify element width to roughness element height is between the target range of 2 to 8. Wi/h = 5.80	Terms with V _o and y _o :	12048.5	= pV_0+C_1y_2W_12	p = density of water = 1.94 slugs/t ³		
Terms with C ₀ A ₁ N is C ₀ A ₁ N: 310.2 = (pV _x ² /2) C ₀ A ₁ N = -3.0 Calculate C ₀ A ₁ N for basin based on parameters determined in steps 2 and 4 ((N ,="X", C ₀ ="X", A,="X", f ²)). Using these values: C ₀ A ₁ N = 13.25 Basin resistance test: Basin Sufficient - If "Revise Basin" is required revise the values located within Step 2. - If "Basin Sufficient, Resistance of Dissipator Greater than Forces on it. Step 5. W ₁ h = 5.80	Terms with Ve	12984.6	- eV-0+02/2V-2W-)	y = unit weight of water = 62.4 lbs/ft ²		
C ₁ A ₁ N = -3.0 Calculate C ₁ A ₂ N for basin based on parameters determined in steps 2 and 4 ((N ,="X", C ₂ ="X", A,="X", f ²)). Using these values: C ₁ A ₂ N = 13.25 Basin resistance test: Basin Sufficient - If "Revise Basin" is required revise the values located within Step 2. - If "Basin Sufficient, Resistance of Dissipator Greater than Forces on it. Step 5. Verify element width to roughness element height is between the target range of 2 to 8. W/A = 5.80	Terms with C.A.N is C.A.N	310.2	$= (a)\sqrt{2}/2$			
Calculate C ₁ A ₁ N for basin based on parameters determined in steps 2 and 4 ((N ,="X", C ₂ ="X", A,="X", T")). Using these values: C ₁ A ₁ N = 13.25 Basin resistance test: Basin Sufficient – If "Revise Basin" is required revise the values located within Step 2. – If "Basin Sufficient, Resistance of Dissipator Greater than Forces on it. Step 6. Verify element width to roughness element height is between the target range of 2 to 8. With = 5.80	C.A.N =	-3.0	ALCO CAL			
Using these values: C ₁ A ₁ N = 13.25 Basin resistance test: Basin Sufficient - If "Revise Basin" is required revise the values located within Step 2. - If "Basin Sufficient, Resistance of Dissipator Greater than Forces on it. Step 5. Verify element width to roughness element height is between the target range of 2 to 8. W/A = 5.80	- Contraction of the second se	struiste C.A.N	For basin based on narameters date	mined in steps 2 and 4 //N #"X" C-#"X" A #"X" #"/		
Basin resistance test: Basin Sufficient - If "Revise Basin" is required revise the values located within Step 2. - If "Basin Sufficient, Resistance of Dissipator Greater than Forces on it. Step 5. Verify element width to roughness element height is between the target range of 2 to 8. With = 5.80		ting theirs with	CAN = 430	e and a second differ to a differ to a difference of a difference of the difference		
- If "Basin Sufficient, Resistance of Dissipator Greater than Forces on it If "Basin Sufficient, Resistance of Dissipator Greater than Forces on it. Step 5. Verify element width to roughness element height is between the target range of 2 to 8. With = 5.80	Pasin resistance text	ang wese valu	- If "Regine Paries" is carried on	une the unkner located within Step 2		
Step 6. Verify element width to roughness element height is between the target range of 2 to 8. Wi/h = 5.80	sasin resistance test.	Saniti Staticies	- If "Basin Sufficient, Resistance	of Dissipator Greater than Forces on it.		
W.A = 5.80	Step 6. W	erify element w	width to roughness element height is between the target range of 2 to 8.			
	W,/s =	5.80				
Values obtained from PLEC-14	V	alues obtained	from HEC-14			

Step 3.		Determine flow cor	ndition V $_{\rm A}$ and y $_{\rm A}$ at the approa	ch to the roughness element field (two culvert widths downstream).		
	2(W ₀) =	16	two culvert widths (ft) [distance	from end of culvert to first row of elements]		
Transit ex	# flow conditions					
	V _A Vo =	1.192	Equation 4.1 (for boxes)	= 1.65 - 0.3Fr		
	V _A /Vo =	-0.181	Equation 4.2 (for circular pipes)	= 1.65 - 0.45 Q/vgO"		
	VA =	17.88	velocity at culvert outlet (ft/s) [II	f circular pipe is being utilized PLEASE revise formula for V $_{\rm A}$ to account for this change]		
		For 4 < W.,W. < 8	ready, from Figure 4.3 (Rectar	ngular) or 4.4 (Circular).		
	Fr =	1.526				
	L=	1.0'B				
y _u /y _i = 0.23 obtain from Figure 4.3 [average depth for abrupt expansion below rectangular culvert outlet]				e depth for abrupt expansion below rectangular culvert outlet]		
	у _А =	0.69	approach flow average depth (i	R)		
Step 4.		For the trial rough	ness height to depth ratio h/y $_{\rm A}$ a	nd length to height ratio determine dissipator parameters from Table 9.1.		
	a. h = $(h/y_A)y_A =$	0.7	roughness element height (ft)			
	b. L = (L/h)h =	2.1	spacing between rows of elements (ft)			
	c. $W_B = (W_B M_0) W_0 =$	36	width of basin (ft)			
c	$\mathbf{H}.\mathbf{W}_{1} = (\mathbf{W}_{1}\mathbf{M}_{0})\mathbf{W}_{0} =$	4	element width (ft)	4 (ft) - rounded value		
e. u _E	= 4/7 + 10L/(7W _o) =	0.94	divergence	1 rounded value		
	f. C _B =	0.4	basin drag coefficient (from Table 9.1)			
	$g_i A_{i'} = W_i h =$	2.76	roughness element frontal area (ft*)			
	h. C _p =	0.7	from Figure 9.4 [energy and momentum coefficients for rectangular culverts]			
	1. L8 = 2Wa + LN. =	22.2	Total basin length (ft)			
Step 5		Use the normal flo	w conditions and solve Equ. 9.1	for C ₆ A ₂ N and compare to C ₆ A ₂ N for basin.		
		Colculated C .A .	V for basin parameters for basin	residance.		
Calculate	CoA, N from Equation	n 9.1				
	Since W ₈ =	36	(R) compare the downstream d	hannel width 36 (R) to trial basin using option 1.		
	y ₀ =	3.09	Downstream (#) [TVV]			
	V ₀ = Q/(W ₁ y ₁) =	3.2	Velocity of the basin (ft/s)			
	Equation 9.1 =	pV_Q+C _p 7y_ ² W_J2	CBA, NpV^2/2+pV_8Q+7Q2/(2V82)	wa		
т	erms with V_ and y_	12048.5	= eV.Q+C.;y, ² W./2	p = density of water = 1.94 slugs/tt ³		
	Tarmer with V-	12004.0	- 2000 100 100	y = unit would of water = \$7.4 the?		
Tarma	MCANIC AN	310.2	= (a)(20)			
	CANE	302	- W74/4/			
	- vorum	Calculate C. A.N.B	u hanin hannel on maramatan da	demined in store 2 and 4 /01 a*Y* C.a*Y* 4.a*Y* 8		
		Company of the second second	C.A.N.s es	Sector and a status a status a fight (= A , Sec. A , Fec. A , B));		
	anin meistanna tast	Using evese valuer	H Baulas Daris" is survivad	.20 major the univer located within the 2		
	NATHER FOR SECTION OF		If "Rasin Sufficient Resistant	revise the values located within output.		
Step 6.		Verify element wid	th to roughness element height i	s between the target range of 2 to 8.		
No. Sold	Wy.As =	5.80				
		Values obtained a	sm HEC-14			
		The state is a contain the state				

Rigid Outfalls in Natural or Park Areas

- Not always popular with parks departments or park users.
- Tend to collect and display trash and debris form the storm sewer system.
- Visual impact can extend beyond the immediate area for large outfalls.

Modified CSU Grouted Boulder Outfall Construction Methods



Construction Techniques

- Layout edges first
- Place "Teeth" and Floor
- Add Soil Riprap

Layout of Edges



Laying out the "Teeth"



Spacing of Boulders is Important



Detailed Spacing



Filling the Floor



Grouting the Boulders



Utilize a pencil vibrator



Brush finish is sufficient



Brush and Clean



Finished Boulders, but....



Soil Riprap can be used to fill voids



Don't forget plantings!



The finished products



Thank you!





21st Annual CASFM Conference September 21-24, 2010

Snowmass Conference Center

Scour Critical Bridges in Colorado Colorado Department of Transportation

Stuart Gardner, PE – CDOT Rick Moser, PE – Moser & Associates



What is Bridge Scour?

What Put Bridge Scour on the Radar?

What is CDOT Doing Now?



What is Bridge Scour?



Scour is the phenomena of moving water removing bed material from around and underneath a structure.

Fast, Clean Water is "Hungry" Water.

Three Basic Types of Scour Contraction Scour Abutment Scour Pier Scour





























What is Bridge Scour?

What Put Bridge Scour on the Radar?





What Put Bridge Scour on the Radar?

In 1987, the 30 year old Schoharie River Bridge at Fort Hunter New York collapsed due to Pier Scour, resulting in ten deaths.

Subsequent to this disaster, the Federal Highway Administration ordered all State DOT's to analyze their bridge inventories with regard to scour. All bridges considered to be susceptible to failure during a 500 year runoff event or below were classified as "scour critical". The State of Colorado completed its inventory in 1992. Over 250 bridges were listed as scour critical.



State DOT's are not the only agencies with Bridge Inventories.

CDOT inspects "Off-Systems" bridges using consultants, but only inspects the physical condition of the structures. A scour inventory or study is not included.



- N Bridge not over waterway.
- U Bridge with unknown foundation
- T Bridge over tidal waters
- 9 Bridge foundations on dry land well above flood water elevations.
- 8, 5 Bridge foundations stable for the assessed or calculated scour condition.
- 7 Countermeasures have been installed to mitigate scour and to reduce the risk of bridge failure during a flood event.
- 6 Scour calculation/evaluation has not been made.
- 4 Bridge foundations stable for the assessed or calculated scour condition. Field review indicates action is required to protect exposed foundations
- 3 Bridge is scour critical; bridge foundations determined to be unstable for assessed or calculated scour conditions.

2 Bridge is scour critical; field review indicates that extensive scour has occurred at bridge foundations, which are determined to be unstable

- 1 Bridge is scour critical; field review indicates that failure of piers/abutments is imminent. Bridge is closed to traffic. Failure is imminent
- 0 Bridge is scour critical. Bridge has failed and is closed to traffic.



Item 113 Code 9 - Bridge foundations on dry land well above flood water elevations.



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2009 Inventory

Item 113	Number of Bridges (3,429 total)		
0			
1			
2	-		
3	176 -		
4	3		
5	576		
6			
7	16		
8	1,519		
9	20		
N	1,076		
U	30 ←		



What is Bridge Scour?

What Put Bridge Scour on the Radar?

What is CDOT Doing Now?



Since 1992, there has not been a systematic effort to remove bridges from the Scour Critical list.

In 2010, a contract was awarded to Moser and Associates to reassess CDOT bridges statewide and develop a Plan of Action (POA) for each structure.

Scour Critical Bridges





CDOT Bridge Scour POA Program Selection of Bridges for FY 2011 POAs



- Scour Critical Bridge Weighting
 - Criteria initially considered:
 - o Route classification
 - o AADT
 - Detour length should the structure be closed
 - Age of structure
 - Condition of structure
 - o Waterway adequacy
 - Schedule for replacing the bridge

CDOT Bridge Scour POA Program Selection of Bridges for FY 2011 POAs



POA Prioritization Methodology

Category	Weight	Weighting Breakdown			
Code 113	25	3=25	4 = 15	7= 0	
Condition	25	Poor = 25	Fair= 15	Good⊨ 0	
ADT	50	>10000 = 50	5000-10000 = 35	1500-5000 = 20	<1500 = 0
Total	100				

CDOT Bridge Scour POA Program Selection of Bridges for FY 2011 POAs



June

CDOT Bridge Scour POA Program





Scour Causes & Significance

Causes of Bridge Scour:

- 1. Flow larger than design/small structure size
- 2. Heavy debris
- 3. Change in stream alignment
- 4. Stream degradation
- 5. Failure of downstream grade control structure

Significance of Bridge Scour:

- 1. Predicted/observed scour depth above pier cap or spread footer, no significance
- 2. Scour depth into pier cap or spread footer, potential bridge stability issue
- 3. Scour depth below pier cap or spread footer, potential bridge collapse



Flow larger than the design flow





Heavy Debris





Change in Upstream Stream Alignment





Stream degradation





Failure of downstream grade control structures



Scour Depth Above Top of Footing No Work is Needed



Bottom of Super Structure



Scour Line Within of Footing Potential Stability Issue



Bottom of Super Structure



Scour Line Below Footing. Potential Bridge Collapse, Mitigation Required

Bottom of Super Structure



CDOT Bridge Scour POA Program POA Elements



- Main Points of POA:
 - Describe procedures to implement before, during, and after flood event to protect traveling public
 - Create an Interdisciplinary Team consisting of:
 - o Hydraulics Engineer
 - o Structural Engineer
 - o Geotechnical Engineer
 - o Maintenance (CDOT)
 - Reassess Code 113 prior to implementing countermeasures
 - Develop appropriate POA framework

CDOT Bridge Scour POA Program



Potential POA components

- Main Points of POA:
 - Monitor During Flood
 - Instrumentation
 - Road Closure & Detour Plan
 - Bendway Weirs/Spurs/Check Dams/Drop Structures
 - Riprap Revetment/Riprap Design for Embankment Overtopping
 - Replacement of Bridge

COUNTERMEASURES FOR BRIDGE PIER PROTECTION

- Articulating Concrete Block Systems at Bridge Piers
- Grout-Filled Mattresses at Bridge Piers
- Rock Riprap or Grouted Rock at Bridge Piers

COUNTERMEASURES FOR ABUTMENT PROTECTION

- Rock Riprap at Bridge Abutments
- Guide Banks

STREAM CORRIDOR STABILIZATION



Aatrix Design Group

A COMPARISON OF APPROACHES USING LARGE & SMALL HEIGHT GRADE CONTROLS

INTRODUCTION

✤ BASIS FOR PRESENTATION:

 Update to 1991 Cherry Creek Stabilization Plan (currently underway)

EXISTING 1991 STABILIZATION PLAN:

- 27 Drops (12.5 mi University to Dam) Avg. Height = 7.5 ft
- 9 Drops Remaining (Avg. Height = 7.0 ft)

Typical drop on Cherry Creek is large

Large Height Drops are Very Common Throughout the Front Range

PROPOSAL TO UDFCD INCLUDED EVALUATING SMALLER HEIGHT DROP STRUCTURES

WHY CONSIDER SMALLER DROPS? (SUBJECT OF THIS PRESENTATION)

1) Large drops have a significant <u>adverse</u> impact on stream corridor

- Stability
- Ecological Function
- Character
- 2) Small drops may have a lower overall long-term cost when costs for long-term bank stabilization are considered

ORGANIZATION OF PRESENTATION

ILLUSTRATE IMPACTS OF LARGE HEIGHT DROPS ON STREAM CORRIDOR

- Impact on Stream Profile and Cross Section
- Impact on Vegetation
- Impact on Shear Stress
- Impact on Habitat
- Impact on Recreation and Aesthetics

COST ANALYSIS SUPPORTING IDEA THAT LARGE HEIGHT DROPS MAY NOT BE THE LOWEST COST APPROACH (When bank protection costs considered)

- Drop Cost
- Bank Protection Costs
- Other Potential Costs
- Cherry Creek Example Cost Calculations

IMPACT ON PROFILE AND CROSS SECTION

CHERRY CREEK EXAMPLE:



IMPACT ON PROFILE AND CROSS SECTION



Looks Good Upstream 😳



Not So Good Downstream 😕



IMPACT ON CHANNEL HYDRAULICS

- \bigstar Channel incision \rightarrow increased shear + increased velocity
- * More aggressive hydraulics have to be resisted by poorer upland vegetation

Cherry Creek Example:



- 100-yr flow
- 0.6 psf limit for veg.

Drop	Vulnerable		
Ht.	Bank Ht.		
2 ft	4.5 ft		
4 ft	6.0 ft		
8 ft	9.5 ft		

IMPACT ON VEGETATION



VEGETATION NEGATIVEY IMPACTED:

- ✤ INCREASED SHEAR & VELOCITY
 - Channel widening \rightarrow lost/narrowed wetland edge
- ✤ LOWERED WATER TABLE
 - Vegetation stress (dying trees)
 - Conversion of wetland/mesic slopes to upland
 - Vegetation on surface = more sparse
 - Root structures = less dense, less vigorous



IMPACT ON VEGETATION



IMPACTS ON HABITAT

<u>Terrestrial Habitat</u>

- ☆ Channel Incision → Conversion of bank and floodplain to upland vegetation
 - Narrowed band of dense riparian vegetation (good habitat)
 - Upland vegetation more sparse (poor cover) = poor habitat
 - 75% of species in Colorado depend on, or benefit from wetlands for some portion of their life cycle

Aquatic Habitat

- Reduced riparian vegetation + vertical cut banks = loss of cover for fish (protection from preditors, reproduction, water temps)
- Large drops are barriers to fish movement.
 - Scientific studies of small plains fishes indicate they have very limited jumping ability and are relatively weak swimmers - even small drops may be barriers.



Monument Creek



Flathead Chub in Fountain Creek

IMPACTS ON RECREATION AND AESTHETICS

- Safety Hazard High cut banks can be a safety hazard
- Trails High cut banks and deep incision into the floodplain limits access to the creek and separates trail users from the creek environment
- * Aesthetics negatively impacted by loss of vegetation and bank erosion



IMPACTS ON RECREATION AND AESTHETICS

Small drops easier to blend into surroundings and make look natural



Large (XX ft) Drop on Cherry Creek

IMPACTS ON MAINTENANCE

- * Reduced vegetation protection and increased shear result in:
 - Banks more susceptible to erosion
 - Deposition of sediment downstream
 - Increased cost for bank protection (greater area to protect and heavier protection required)



CHERRY CREEK STABILIZATION PLAN UPDATE

- * Typical Drop Costs
- Typical Bank Protection Costs
- Overall Long-Term Cost (Drops + Bank Protection)
- Un-accounted For Costs (Maintenance)

GROUTED BOULDER DROP COSTS



- Costs based on grouted boulder construction
- Costs account for different:
 - Boulder/grout thickness
 - Cutoff wall depth
 - Stilling basin length
 - Bank height to be protected

BANK PROTECTION COSTS



Costs based on:

- Planted soil riprap construction
- Typical Cherry Creek reach and dimensions
- Variation in shear stress with different degrees of channel incision

OVERALL COST ANALYSIS

Alternative	Cost
1- Large Drops (8' Typical)	\$17.3 million
2 - Small Drops (3' Typical)	\$17.8 million

- * 3% increase in cost for reduced height drops.
- Assumes 50% of bank length will ultimately require protection.
- * Costs for sediment removal not accounted for.
 - UDFCD budgets \$500k +/- per year for this
| Alternative 1 (Large Drops) | Alternative 2 (Small Drops) |
|---|---|
| Advantages | Advantages |
| 1. Lower Initial Cost (lower drop cost) | Lower long-term (overall cost) bank protection sediment production maintenance |
| 2. Fewer work/access/easement areas | 2. Improved vegetation health - bank stability - aesthetics - habitat |
| | 3. Improved trail user experience - aesthetics - safety - creek accessibility |

CONCLUSIONS

✤ WHY LARGE HEIGHT DROPS SO COMMON?

- Lack of Funding for Proper Phasing
- Reactive Band-Aid Approach (Emergency Infrastructure Protection)
- Impacts of Large Drops on Stream Corridor not Fully Appreciated
- True Cost of Large Drops Not Understood
 - Economic
 - Environmental

CONCLUSIONS

- LARGE HEIGHT GRADE CONTROL STRUCTURES RESULT IN AN OVERALL GREATER LEVEL OF CHANNEL INCISION IN THE FLOODPLAIN
- ✤ INCISION DESTABILIZES BANKS RESULTING IN:
 - Loss of Vegetation
 - Loss of Habitat
 - Degradation of Aesthetics and Recreational Potential
 - Sediment Production
- COST EVALUATIONS FOR DROPS SHOULD CONSIDER LONG-TERM COSTS ASSOCIATED WITH IMPACTS TO BANK STABILITY INCLUDING:
 - Cost for additional bank protection
 - Costs for maintenance
- ALL OF THE ABOVE FACTORS SHOULD BE CONSIDERED WHEN EVALUATING GRADE CONTROL PROJECTS



Constructing Sculpted Concrete Drop Structures

Laura Kroeger, UDFCD Jeff Fisher, UDFCD Jerry Naranjo, Naranjo Civil Constructors

Beauty is in the Eye of the Beholder -Author: William Shakespeare

Function is the Responsibility of the Engineer -Author: Missing









The 5 C's to Sculpted Drops

- Context
- Configuration
- Construction
 Documents
- Contractor
- Color



Context

Structure to fit into the surrounding landscape



Context

Questions to Ask What are the existing characteristics? natural features man made features What is the scale of landscape features? What is the public access?



Environmental/Aquatic considerations? What will complement the existing landscape?

Context



Configuration

- Size
- Shape
- Scale
- Safety
- Uniformity



Configuration

- Size
- Shape
- Scale
- Safety
- Uniformity









Contractor

- Write your specifications to get a qualified contractor
- Use additional tools to communicate with
 - 3-d modeling of structures
 - Pictures
 - Field trip
 - Rock out-cropping

Color and Finishing

Color

- Integral color
- Staining/painting
- Nature, water



Finish

- Finishing
 - Powerwashing
 - Stamping
 - Skins, burlap, foil
 - Carving and shaping
 - Depressions
 - Vegetation
- Texture Additives
 - Sand, rock, wood



Factors to Consider During Construction



Diversions



Dewatering









Cut-off Walls







Preparing the Subgrade



Reinforcing





Concrete



Concrete Testing



Concrete Placement








Crest Elevation





Weather



Weather Protection



Constructing Concrete Drop Structures: The Contractor's Perspective



Subgrade Shaping and Prep



Rebar Tying



Chicken Wire



Pump Setup



Concrete Arrival



Concrete Arrival - Timing



Checking The Batch



Pumping/Pouring



Vibrating



Shaping



Sculpting



Applying Release



Texture Stamping



Line Production



Time Lapsed Process:



Staining



Finished Pour



What makes a good design?

- Designer has a style in mind from previous projects
- Design shows critical elevations throughout the entire structure, not just slopes
- Collaborate with crew during construction, innovate together.

Hydrologic Performances of Pervious Concrete and Porous Asphalt Pavement Systems

Thomas Ballestero, PE, PhD, PH, CGWP, PG, Federico Uribe, Robert Roseen, PE, PhD, D.WRE, James Houle, CPSWQ, Timothy Puls

University of New Hampshire Stormwater Center 2010 CASFM CONFERENCE *Snowmass Village, Colorado*



Objective

• What are the "runoff characteristics of permeable pavements?









What is the Curve Number For Porous Pavement?

Who wants to know?!?

(What is your OBJECTIVE?)

The SCS (NRCS) Curve Number

Originally conceived to translate rainfall *depth* into runoff *depth* on agricultural watersheds...method worked best for large storms

This was then translated into a runoff hydrograph

SCS Dimensionless Unit Hydrograph



UNHSC Porous Pavement Sites



Permeable Pavement Sites



UNHSC Porous Asphalt Lot

UNHSC Porous Concrete Lot
Typical Cross-Section Construction



Sub-base design matches that of the UNHSC Porous Asphalt Parking Lot

UNHSC Porous Pavement Monitoring

- Compound weir
- Pressure transducer
- Datalogger





UNHSC Porous Pavement Hydrologic Data

"Real time" flow monitoring...5-minute time step
"Real time" rainfall monitoring...5-minute time step







Methods of Teasing CN from the Data

Measure P and Q, invert basic SCS equation

- Measure P and outflow hydrograph (q), measure lag, estimate CN from lag equations
- Measure Q and q_p, estimate CN from peak discharge equations

Method 1 - Depth of Runoff (Q)Method

$$Q = \frac{\left(P - I_a\right)^2}{P - I_a + S} \quad Eq. \ 1$$

$$I_a = 0.2S$$
 Eq. 2.

Q: Total Runoff Depth (in) P: Total Precipitation Depth (in) I_a: Initial Abstraction (in) S: Storage Parameter (in)

$$Q = \frac{(P - I_a)^2}{P + 0.8S} = \frac{(P - 0.2S)^2}{P + 0.8S} Eq.3$$

$$S = \frac{1000}{CN} - 10 \quad Eq. 4.$$



Method 2 -Lag Methods

- Study how the timing of the "runoff" is transformed
- Time of concentration
- Lag time
- Time base
- Peak time



Method 2 -Lag Methods

$$T_{lag} = \frac{L^{0.8} (S+1)^{0.7}}{1900 \cdot Y^{0.5}} \qquad Eq. 5.$$

$$T_c = \frac{5}{3}T_{lag} \qquad Eq. \ 6.$$

T_{lag}: Lag Time (hr) T_c: Concentration Time (hr) Y: Surface Slope (%) S: Storage Parameter (in)

$$S = \frac{1000}{CN} - 10$$
 Eq. 7.

Lag Methods

3 APPROACHES



Lag Methods

LAG METHOD (2)



Lag Methods

In. Abs.

3. T centroid (NRCS [2009], Folmar, Miller and Woodward [2009])

T lag: time from the centroid of excess precipitation to the peak of the hydrograph.

CN =

1000

 $L^{0.8}$



Method 3 GRAPHICAL PEAK DISCHARGE METHOD

 $q_p = q_u A_m Q$

q_p: Peak Discharge (cfs)
 q_u: Unit Peak Discharge (csm/in)
 A_m: Drainage area (mi²)
 Q: - NRCS Storm Runoff (in)
 - Folmar, et. al Excess
 precip. prior to peak.



GRAPHICAL PEAK DISCHARGE METHOD



Method 3 – Graphical Peak Discharge

Unit Peak discharge for NRCS type III rainfall distribution chart.

Measure q_p, Am, Q

Compute q_u

Ia/P = 0.1

Determine Tc

Compute S, CN

Check Ia/P



Method 3 – Graphical Peak Discharge

 $q_p = q_u A_m Q$

 $Tc = f(q_u)$



CN (Clean Data)									
Ctorm	Dete	Rainfall	Runoff	Method 1	Method 2			Method 3	Method 3
Storm	Dale	[in]	[in]	Q-P		Lag		Q peak	Q peak
					Tbase	Tpeak	Tcentroid	NRCS	Folmar
1	10/8/2005	5.00	3.99	91.1	68	R>P	R>P	1	106
2	10/15/2005	3.53	3.45	99.3	24	R>P	R>P	1	5
3	10/11/2006	2.78	1.68	88.8	9	R>P	R>P	5	69
4	5/2/2006	2.37	1.40	89.8	1	R>P	R>P	0	3
5	8/20/2006	1.92	0.92	88.4	13	R>P	R>P	11	111
6	4/3/2006	1.57	0.77	90.6	10	R>P	R>P	2	55
7	12/16/2005	1.38	0.45	87.0	-	2	2	2	48
8	7/12/2006	1.35	0.75	93.2	11	8	7	2	59
9	7/19/2007	1.28	0.43	88.0	2	1	1	1	4
10	12/23/2006	1.21	0.85	96.4	-	1	1	1	13
11	9/11/2007	1.12	0.41	90.1	-	3	3	2	98
12	7/8/2005	1.02	0.35	90.5	1	1	1	1	3
13	10/10/2005	0.87	0.74	98.8	4	1	1	1	56
14	11/16/2005	0.86	0.94	100.6	1	1	1	1	22
15	7/15/2007	0.82	0.00	70.9	0	0	0	0	0
16	5/16/2007	0.69	0.90	101.5	1	1	1	0	6
17	8/4/2006	0.68	0.00	74.6	0	0	0	0	0
18	7/9/2007	0.66	0.33	96.0	-	2	2	2	50
19	9/19/2006	0.63	0.00	76.0	0	0	0	0	0
20	7/28/2007	0.63	0.00	76.0	0	0	0	0	0
21	9/3/2006	0.62	0.00	76.3	0	0	0	0	0
22	4/23/2006	0.58	0.00	77.5	0	0	0	0	0
23	12/26/2006	0.58	0.86	101.8	0	1	1	0	8
24	5/9/2006	0.56	0.00	78.1	0	0	0	0	0
25	7/4/2007	0.55	0.00	78.4	0	0	0	0	0
26	4/27/2007	0.54	0.53	99.9	-	0	0	0	2

R>P: The rainfall center of mass exceeds hygrograph peak timing

RESULTS

	Method 1	10	Metho	d 2	Method 3	Method 3
	Q-P	Lag			Qp	Qp
		Tbase	Tpeak	Tcentroid	NRCS	Folmar
Mean	88	7	1	1	1	28
Median	90	1	1	1	1	5
Standar Deviation	10	15	2	2	2	37



Long Term Water Balance - PA



Long Term Mass Balance (Q vs P)

	Curve Numbers				
	A soil system	C soil system			
Winter	8	85			
Spring	22	100+			
Summer	0	63			
Fall	2	77			

So....Which to Use?

- Events
 - Peak Outflow from Drain
 - Peak flow method
 - No net increase in benchmark storms
 - Lag method
- Long Term Simulation
 - Lag method
 - Runoff depth method
- Watershed Simulation
 - Seasonal CN
 - Lag method

Philosophically Speaking.....

• What is the CN for a detention pond?



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Acknowledgements Funding Source: CICEET

Questions?

http://www.unh.edu/erg/cstev/

or Simply Search for "UNHSC"

INNOVATIVE STORMWATER MANAGEMENT FACILITIES INFRASTRUCTURE MODIFICATIONS – BUILDING A GREEN STREET VISION

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DISCLAIMER

- Though I work for the City of Aurora, and the Department of Public Works, the ideas and programs presented here in this presentation are not necessarily those of the City of Aurora.
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WATER QUALITY IN OUR EXISTING INFRASTRUCTURE

HOW DO WE DEVELOP A GREEN STREET VISION?



EXISTING PROGRAMS

- UDFCD Criteria Manuals. Address drainage and water quality of NEW development
- > EPA TMDLs. Total Maximum Daily Loads.
- If A is your TMDL, then B + C + D + E + (etc.) better be less than or equal to A.
- One of the biggest issues we face in meeting this requirement is our EXISTING infrastructure. Most of the runoff from this is untreated.

NEW DEVELOPMENT – EASY

- Codes
- Design Procedures
- Criteria Manuals
- Masterplanning
EXISTING INFRASTRUCTURE – DIFFICULT

- Little or no room
- Facilities can't be modified
- New facilities are expensive or
- No room to retrofit
- Limited technology or facilities out there to utilize.
- Expensive to purchase property
- Public Relations issue(s) Would you want your parking lot taken away?

SO WHAT DO WE DO?

- Rip-up existing infrastructure and replace it? (Expensive)
- Reduce the impervious footprint. Not as easily done as said. (Expensive)
- Existing technology is a hit and miss as far as what you're trying to do and achieve, and along with its effectiveness.
 - Are you going to street sweep "every day?"
 - Underground WQ & detention is going where?
 - Are you going to take away the valuable parking of a business?

WHAT IS AVAILABLE TO US?

- We need easy, effective, and less expensive water quality facilities in order to meet our TMDLs.
- Some we have. We just need to push the programs and or provide funding or incentives to use them.
- Others need to be included with CIP improvements or upgrades (like ADA)
- Spend the money directly on water quality facilities.

EXISTING PROGRAMS

- ROOFS: Eco-roofs and roof gardens
- These are in UDFCD Manuals.
- Problem Most roofs aren't structurally sound enough to support eco-roofs.
- Semi-arid region, we need to have the vegetative material appropriate to our region.
- Owner, or developer, is not going to spend the money on an eco-roof. So there needs to be some other kind of funding or incentives to convert roofs of existing structures.

WASHINGTON DC GREEN STREET VISON



ECO – ROOFS AND ROOF GARDENS



ECO – ROOFS AND ROOF GARDENS



REDIRECT THE ROOF DRAINAGE

- Disconnect if roof drains and downspouts are directly connected to the street or storm sewer system.
- Redirect the roof drainage to a water quality facility.



LANDSCAPED, OR CONTAINED, PLANTERS



FLOW THROUGH PLANTERS



TREES AND TREE GRATES



CONTAINED PLANTERS CAN BE USED



Contained Planter

revised 2006

VEGETATIVE WALLS



Modify roof drains to a level spreader, or drip system.
Also helps with energy conservation. Sun doesn't beat on bare walls.

MEANDERING FLOW LANDSCAPE FACILITIES















THIS SHOWS HOW PLANTERS FILTER STORMWATER



ANOTHER INFILTRATION PLANTER





Stormwater Management – Catchbasin Stormfilter



PAVING BLOCKS IN PARKING STRIPS



DC GREEN STREET "TOOLBOX"



Permeable Pavement

 Reduces runoff volume
 Removes pollutants: sediment, oils and grease, metals
 Reduces urban heat island
 Aesthetic value: many color and pattern options

+ADA compliant pavement

Possible locations: * North side of 45° to 45° * Between 51° and Division Ave.



and a set of the set o

Vegetated Filter Strip

- Includes soil amendments and sustainable landscaping
 Reduces runoff volume
- +Provides habitat and green space

Possible locations: * 46th Street, Slope on the north side of NHE

* 50h to 51st Street. Median

* 51st Street to Division, Median * Division to 55th Street, Median



Street Trees

Reduces runoff volume
 Reduces urban heat island
 Improves air quality
 Reduces noise and wind effects
 Provides shade

Healthy tree pilot locations: (structural soil under permeable pavement) 51° 51 to Division Ave. 7 techs see of 40th to 40th



RECHARGE GROUNDWATER (INFILTRATION)

- Portland's program called UIC (Underground Injection Control).
- These are facilities that allow the stormwater runoff to recharge the groundwater rather than be swept away by a sewer system.
- Program needs to be permitted, and is regulated by Oregon's Department of Environmental Quality.

RECHARGE GROUNDWATER

- UICs can be an essential element of a City's comprehensive watershed strategy to use stormwater as a resource by infiltrating it back into the ground.
- UICs quickly and efficiently reintroduce stormwater into subsurface soils, which filter and cool the runoff before it finds its way to groundwater and, eventually, helps recharge streams.
- UICs are an essential element of street-side swales and green street applications because they provide an overflow point during large storm events when stormwater cannot be fully infiltrated through swales, planters, or other surface infiltration systems.
- UICs also preclude the need to install or increase the capacity of piped stormwater infrastructure that eventually discharges into local surface water bodies.

PARKING LOT UIC



STREET UIC CONFIGURATION



CLEAN WATER ACT

- The federal government started the Underground Injection Control Program in 1974 as a means of implementing the Safe Drinking Water Act. The program's goal is to protect groundwater as a drinking water resource and to prevent groundwater contamination from underground injection systems.
- Congress enacted UIC rules in 1974 and modified the rules in 1999. The U.S. Environmental Protection Agency (EPA) administers these rules under Title 40 of the Code of Federal Regulations (CFR) Parts 144–148. In Oregon, EPA has delegated UIC regulation to DEQ. Oregon Administrative Rule (OAR) 340– 044 regulates all groundwater as a potential source of drinking water and requires municipalities with more than 50 UICs to operate under a permit. DEQ issued a <u>WPCF permit</u> to the City of Portland on June 1, 2005 (DEQ Permit Number 102830) in response to the OAR.

EVALUATION-SITE ASSESSMENT Portland prohibits UIC's if:

- 1. Receives drainage from motor vehicle maintenance floor drains, indoor parking facilities, fire station bay drains;
- 2. Receives drainage from Superfund Amendment and Reauthorization Act (SARA) Title III facilities;
- 3. Receives drainage from commercial/industrial properties that have site activities that may result in a permit violation;
- 4. Has inadequate separation distance to groundwater; or

5. Is within 500 feet of a drinking water well or within 2-year time of travel.

TYPES OF FACILITIES

- Sedimentation Manhole Primary purpose is to remove particulates from stormwater prior to getting into the UIC.
- Cylindrical drywells the sides of this UIC are perforated and allow exfiltration of stormwater into the surrounding soils.
- Soakage Trenches/Perforated Pipes. Use in landscaped areas, medians, tree strips.
- Drywells For smaller sites and parking lots

WHAT ELSE?

- Modify existing inlets.
 - Turn into drywells
 - Modify them by adding filter media
 - Connect them to a filter strip or soakage trench
- Street Sweeping expensive, and needs to be performed regularly.
- ??? New ideas are always coming along...

Pueblo Low Impact Development (LID) Concepts

Short Elliott Hendrickson Inc. (SEH) Lakewood, Colorado

Kelly Jankowski, El



Project Overview

- Scope of work
 - Site visit and photo documentation
 - Best Management Practices (BMPs) selection
 - Plans and details showing the location of BMPs
 - Hydrologic impact
 - Hydrologic benefit of BMPs
Site Location Pueblo, Colorado



Best Management Practices (BMP) Selection

Table 1: BMP Scoring Matrix

	Purpose	Enrie	Wood Applicative To Stre for Prove Beduction	Temporary BMPs	Propert Appropriate Determinant Determinant	Nydrologie Impact	Coars	Entryconantial Impact	Proveni Acceptance Simplicity	Score Propositi Event	Boore Wajor Even
Raduce imperations Barlaises	To minimize needs by reducing importance surfaces, therefore nedscing the must be shown systems, and letting control outputs without savel.	Low Impact Development Applications for Water Processes Management ALCE	1		+	++	+	+	+	6	N/A
Grans Buller	To provide Mindon, Milliotics and writing to reduce tracif publicates. Sheet from a secondry for these to be beneficial integration to created to material building democration.	Unlan Norm Trustage Criteria Marcal, Vol. 3: prior Distage & Root Scott Datas	1	2	+	+	+	+	+	5	N/A
Grans Beale	To facilitate sedimentative stills letting receive	Urban Bikere Drainege Orlieta Manad. Will 3. Insie Oranigu & Revolution & Datas	1		+	+	+	+	+	5	N/A
Minimize Clearing & Grading	To debelow address lader rand by proceeding and albitry the colotry conditionent,	Low Impact Development Applications for Water Records: Management Mills		2	0	++	+	++	0	5	N/A
Depresation Blorage	To become localized determine stronge and become infibution provideby	Low Inguist Geoekgement Applications for Water Resource Management and	1		++	+	+	+	0	5	N/A
Conservation Plans Regulations	To conserve traductal incourses such as longels, streams, wellands, habites, paths, cellical assas, tradit, clean times, agricultural lands, mitemate, etc. promoting transit implicitiegic conditions.	Low Inguid Streikpreent Applications for Water Record or Management		_	0	++	0	++	0	4	N/A
Conserve A.R. & Type Bolto	To conserve the A & D type with to alter for future dramage. A & D type with have higher initiation rates than C & D types with altering them to about hand conserve.	Low Impact Dovelapment Applications for Water Encource Management alics	1		+	++	0	+	0	4	N/A
Wei Sezie	To the polylasts as stormatic typol moves lineaging to sends. Deals or other septimize is used to provide convergence and its the roat polylastic. Eccentrally the same as a dry rando encept there is a porticipants at the format of the store.	Ensite Celled & Burnashe Guilly Gala Construction	1		+	+	+	+	0	4	4
Biter Reinaus Detection Basic	To facilitate policitat and andream memory. The is a solution taken inside of a body due after diversable randomic. The output of the basis is much smaller that the bat of a determine basis, therefore advecting the employing the basis of the basis of the basis is a source in the basis of a determine the policy the determine of the employing the basis of the basis of the basis is a determined.	Urban Bhom Duatoge Orbetis Menaal, VA 3 Urba Dianage X Root Contro Datas	1		++	++	0	0	0	4	4
Rain Gardene Biovelention	To prove storage to the form of a glassic tor otherwaster rundit. These gardees are tgittally placed to the areas and capture should from store overds.	Low Impact Development Applications for Water Pressator Management ALCE	1		++	+	+	+	-	4	N/A
Dry Beate	To the polaram as stormane rand moves though the seals. Canso or other vigitation is used to provide convergence and to filler out polaram.	Emake General Statements' Godby Gable		2	0	+	+	+	0	3	N/A
Sealing	To gathly presively vegetates cover on-distanced amongly solation with and control encoder.	Drahoge Oslovia Manual, Visi 2 Dismonter Gaulty Policies, Procedures & UMPs		ŝ	0	0	+	+	+	3	N/A
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Best Management Practices (BMP) Selection

- State Fairgrounds
 - Rain Barrels (72-hour release)
 - Rain Gardens
 - Depressed Parking/ Slow Release Detention
 - Reduced Impervious Surface Area
 - Porous Landscape Detention
- Residential Area
 - Rain Barrels (72-hour release)
 - Porous Pavers
 - Local Detention
 - Short Street Calming Devices at Intersections with Porous Landscape Detention and Rain Gardens

Rain Barrel



http://www.stltoday.com/blogzone/political-fix/files/2009/04/rain-barrel.jpg

Rain Garden



Slow Release Detention Basin



http://cfpub.epa.gov/npdes/stormwater/menuofbmps/index.cfm?action=factsheet_results&view=specific&bmp=67

Porous Landscape Detention



http://www.casfm.org/stormwater_committee/images/IMGP6666.gif

Porous Pavement



Street Calming Devices



http://www.lowimpactdevelopment.org/greenstreets/images

Overall Site Aerial

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	市三层建築				CRYST-1
					NORTHERN

SCALE: 1" = 400"

NORTH:

LEGEND



Rain barrels at permeter of building (Min. 4 per building, 1 at each corner)

Porous pavement (reducing impervious area)

Porous pavement and/or landscape to encourage inflitration (reducing impervious area)

Landscape to encourage infiltration (reducing impervious area)

DATE: 12/1/2008

Typical Residential Block



Residential Area - Before



Residential Area - After



State Fairgrounds - Before



State Fairgrounds - After



Streetscape - Before



Streetscape - After



Hydrologic Impact - Methodology

- Colorado Urban Hydrograph Procedure (CUHP) v. 2000
- Models
 - Base Hydrologic Model
 - Rain Barrels
 - Porous Pavement and Rain Gardens
 - Street Calming Devices and Porous Landscape Detention
 - Slow Release Detention
 - Reduced Impervious Area



Impact of Rain Barrels on Storm Runoff Characteristics

Storm Frequency	Δ Vol. (%)	Δ Qp (%)
Annual	-17%	-25%
2yr	-5%	-5%
5yr	-3%	-3%
10yr	-3%	-2%
100yr	-1%	-1%

Assumptions:

- Typical Rain Barrel capacity of 50 gallons
- Average roof area of 1500 sf
- Four Rain Barrels per building

Model Modifications:

• Impervious Depression Storage Parameter (0.1 in -> 0.16 in)



Impact of Porous Pavement and Rain Gardens on Storm Runoff Characteristics

Storm Frequency	Δ Vol. (%)	Δ Qp (%)
Annual	-25%	-24%
2yr	-5%	1%
5yr	-2%	1%
10yr	-1%	1%
100yr	-1%	0%

Model Modifications:

• Minimum Directly Connected Impervious Area (MDCIA) - Level 1



Impact of Street Calming Devices and Porous Landscape Detention on Storm Runoff Characteristics

Storm Frequency	Δ Vol. (%)	Δ Qp (%)
Annual	-68%	-73%
2yr	-13%	-7%
5yr	-5%	-8%
10yr	-3%	-9%
100yr	-1%	-9%

Model Modifications:

• Minimum Directly Connected Impervious Area (MDCIA) – Level 2



Impact of Rain Barrels, Street Calming Devices and Porous Landscape Detention on Storm Runoff Characteristics

Storm Frequency	Δ Vol. (%)	Δ Qp (%)
Annual	-75%	-78%
2yr	-18%	-13%
5yr	-8%	-12%
10yr	-5%	-12%
100yr	-3%	-10%

Model Modifications:

- Impervious Depression Storage Parameter (0.1 in -> 0.16 in)
- Minimum Directly Connected Impervious Area (MDCIA) Level 2



Impact of Slow Release Detention on Storm Runoff Characteristics

Storm Frequency	Δ Vol. (%)	Δ Qp (%)
Annual	-78%	-79%
2yr	-22%	-19%
5yr	-13%	-17%
10yr	-10%	-20%
100yr	-8%	-16%

Assumptions:

 Slow Release Detention areas are fully detained and do not contribute to the stormwater volumes and discharges of the subbasin.

Model Modifications:

• Remove the sum of the area to be Slow Release Detention from the total sub-basin area



http://www.apartmenttherapy.com/boston/ outdoor/oldfashioned-ribbon-driveways-119857

Impact of Reduced Impervious Area on Storm Runoff Characteristics

Storm Frequency	Δ Vol. (%)	Δ Qp (%)
Annual	-78%	-84%
2yr	-22%	-23%
5yr	-11%	-19%
10yr	-8%	-19%
100yr	-4%	-17%

Model Modifications:

• Reduce the percent impervious of each basin by three (3) percent

Conclusion

- Rain Barrels are a very cost effective way to reduce frequent storm event flows
- Slow Release Detention is the most effective way to reduce flows from large storm events

 Location Critical
- For this retrofit project, LID was not able to reduce the large storm events enough to significantly downsize diameters of receiving storm sewers



Low Impact Development on a Federal Installation



U.S. AIR FORCE



E. John Loranger PE, CFM AMEC Earth and Environmental Jeff Cheng PE, AMEC Earth and Environmental Dorothy Eisenbraun PE, AMEC Earth and Environmental Chad Callan, 460 CES Engineering Flight

amec

Overview

- Background
- EISA 2007 Section 438
- EO 13514
- Technical Guidance
 - EPA 814-B-09-001
- Conventional/LID Approach
- EPA SWMM5 Lumped Model
- Distributed Model
- LID Benefits to the Master Plan



Buckley Air Force Base

- Location, size
- Describe watersheds/drainages
- Fast Growing







Background



Approach to Master Plan

- Military installation vs. municipal
- Existing Conditions
 Evaluation
- Future Conditions
 Evaluation
- Recommendations
 - Upsizing
 - Maintenance
 - Expansion
 - LID

Energy Independence and Security Act of 2007



Federal Stormwater Runoff Requirements

- New Development > 5000 ft² footprint
- Re-Development > 5000 ft² footprint

Replicate Pre-development Hydrology

"The sponsor of any development or redevelopment project involving a Federal facility with a footprint that exceeds 5,000 ft² shall use site planning, design, construction, and maintenance strategies for the property to maintain or restore, to the maximum extent technically feasible, the predevelopment hydrology of the property with regard to the temperature, rate, volume, and duration of flow."



Section 14

Stormwater Guidance for Federal Facilities. Within 60 days of the date of this order, the Environmental Protection Agency, in coordination with other Federal agencies as appropriate, shall issue guidance on the implementation of section 438 of the Energy Independence and Security Act of 2007.

EPA Technical Guidance



• EPA 841-B-09-001

- How to Achieve, Measure and Evaluate
- Pre-Development Hydrology
 - Volume
 - Flowrate
 - Duration
 - Temperature
- Retain the 95th Percentile Storm
- Site Specific Hydrologic Analysis

Conventional/LID Approach



Future Conditions Build out

- LID Approach
- Existing Infrastructure
 - Conventional Approach









Conventional Watershed Model

- EPA SWMM5 natural plan method
- Impervious to outlet
- Pervious to outlet
- Cascading Plane Model
 - Pervious to Outlet
 - Impervious to outlet
 - Impervious to Pervious to Outlet

Cascading Plane on Central Channel and Cascading Planes





Example of Cascading Plane




Cascading Overland Flow





Distributed Approach



The cascading KW model needs to follow two major principles: Continuity principles, which can be described as:

$$\frac{q_i(t+\Delta t) + q_i(t)}{2} + \left[\frac{I_e(t+\Delta t) + I_e(t)}{2}\Delta x - \frac{q_o(t+\Delta t) + q_o(t)}{2}\right] = \frac{Y(t+\Delta t) - Y(t)}{\Delta t}\Delta x$$

$$I_e = I - f$$

q = flow per unit width, I = rainfall intensity, Y= flow depth, X = length of reach, and f = infiltration loss.

Momentum principles for KW plane considers the flow slope as same as friction slope, which the equation can be described as :

$$S_{0} = S_{f}$$

$$q_{o}(t + \Delta t) = \frac{1.49}{n} [Y(t + \Delta t)]^{\frac{5}{3}} \sqrt{S_{o}}$$

amec

Lumped Approach

- SWMM5 employed to conduct the lumped model approach
- Comparisons between lumped and distributed models can provide guidance to generalize the application of KW shape function to the LID layout

Subcatchment 2	
Property	Value
Name	2
X-Coordinate	79.488
Y-Coordinate	8454.405
Description	
Tag	
Rain Gage	1
Outlet	J1
Area	15
Width	808
% Slope	1
% Inperv	100
N-Imperv	0.013
N-Perv	0.1
Dstore-Imperv	0
Dstore-Perv	0
%Zero-Imperv	0
Subarea Routing	OUTLET 💌
Percent Routed	OUTLET
Infiltration	PERVIOUS
Groundwater	NO
Snow Pack	
Land Uses	0
Initial Buildup	NONE
Curb Length	0
Choice of internal routing between pervious and impervious sub-areas	

LID Benefits to the Master Plan



- One of the 1st LID Masterplans in Colorado
- Quantify On-Site Infiltration Volume
 - Minor Event
 - Major Event
- LID Reduction in Conventional Stormwater Management Costs/Infrastructure
- Less Downstream Stormwater Impact



QUESTIONS?



September 23, 2010

April Barker, COA Stormwater Manager





9/13/2010



Common Urban Pollutants

Increases with impervious area: Total Suspended Solids (TSS) Nutrients Metals Oxygen Demand Hydrocarbons Pathogens





A message from our sponsors...

AMEC Earth and Environmental – Jon Sorenson, Dr. Jim Guo, Jeff Cheng

Wright Water Engineers – Andrew Earles

Wenk and Associates – Greg Dorolek

UDFCD Volume 3





Aspen Specific Data...

	Annual Average
Max Temp	55.5 F
Min Temp	27.7 F
Precipitation	24.37 inches
Snowfall	173.8 inches

Snow on ground, in town 7 months of year Elevation = 8000

Population = 6000 - 20,000

Area = 3 square miles

Event	Intensity (inches/hour) 1-hour
2-year	0.64
5-year	1.00
10-year	1.20
25-year	1.40
50-year	1.60
100-year	1.69

Challenges Unique to Aspen

Cold Temperatures Deep Frost Line Short Growing Season Significant Snowfall Midwinter Snowmelts Rain on Snow Spring Runoff Sanding Practices Steep Slopes Resort Setting Dense Development





Goals for water quality...

- Provide full water quality treatment for up to the 80th percentile runoff event
- For events larger than the 80th percentile event, BMPs will provide treatment of the "first flush"
- Based on 12-hour drain time, removal in excess of 90 percent of particles fine-sand sized and larger is expected

Treatment train - Runoff will then be treated downstream by regional treatment facilities (Jenny Adair)



Detention – To pre-developed rates for 10 and 100-year events Sonveyance – 5 or 10-year and 100-year; downstream analysis Floodplains – no rise in water surface and lowest floor 1ft above BFE (100 year fp), FP Development Permit, Elev Certificate Mudflows – mitigate impacts to self and neighbor

 $\begin{array}{c} 0.30 \\ 0.25 \\ 0.20 \\ 0.5 \\ 0.20 \\ 0.5 \\ 0.00 \\ 0.5 \\ 0.00 \\ 0.5 \\ 10 \\ 15 \\ 20 \\ 25 \\ 30 \\ 35 \\ 40 \\ 45 \\ 50 \\ 55 \\ 60 \\ 65 \\ 70 \\ 75 \\ 80 \\ 85 \\ 90 \\ 95 \\ 100 \\ 10 \\ 15 \\ 20 \\ 25 \\ 30 \\ 35 \\ 40 \\ 45 \\ 50 \\ 55 \\ 60 \\ 65 \\ 70 \\ 75 \\ 80 \\ 85 \\ 90 \\ 95 \\ 100$

9/13/2010



Planning Stages

- Consider stormwater EARLY in design process
- Rough layout, estimate impervious area
 - 10-15% of imp area should be estimated for wq treatment
 - Aim for several smaller areas, rather than one large
 - Space constraint? Consider ROW
- BMPs
 - Options that meet character of site
 - Maintenance and accessibility
 - Function infiltrating?
- Conveyance surface, green, don't direct pipe
- Flood control, detention integrate, multi-purpose



Minor vs. Major

Minor Project

- 200 1000 sf disturbance
- Green improve wq
- Urban WQCV for disturbed/new area
- No professional engineer
- Much less on drainage report
- Sketch for drainage plan

A

Major Project

- Over 1000 sf disturbed
- Detention to pre-developed for entire site
- If < 50% of site, only WQCV for disturbed area
- If > 50% of site, WQCV for entire site
- Requires PE and full drainage analysis

LID – Plans Review

Step 1 - Describe what efforts have been made to reduce runoff and increase infiltration...

Reduce impervious area Disconnect impervious area Reduce runoff via surface flow – grass swales, grass buffers



WQCV – Plans Review

Step 2 – Treat the WQCV

Pervious paver with detention Street BMPs/sediment traps **Bioretention** Extended Detention Basin Sand Filter Constructed Wetland **Subsurface treatment – vaults, drywells**



Water Quality in the Manual

Planning Principles

• Based on UDFCD – Early, entire site, avoid unneccessary impervious area, reduce runoff, match natural, integrate

BMP based on land use

- Ultra-urban, streets, dense residential, parks
- Consider sanding, infiltration, groundwater, etc

Each BMP:

- Description and general application
- Advantages/Disadvantages
- Physical Site Suitability
- Pollutant Removal Ability
- Cold Weather Considerations
- Design Considerations, Procedure, Criteria
- Maintenance Requirements



Unique in Aspen

Subsurface Treatment Systems

Use of Right of Way – allowing private development use of public property for stormwater management















Contents

- Introduction
 - 7 page, includes everything you need
- Chapter 1 Permit Requirements
- Chapter 2 Rainfall
- Chapter 3 Runoff
- Chapter 4 Street Drainage Design
- Chapter 5 Detention
- Chapter 6 Floodplains
- Chapter 7 Mudflow
- Chapter 8 Water Quality
- Appendices: Appendix A Checklists





"Out Of The Box Off The Shelf" Linear Project Hybrid PLD Pilot Study Shows Promise

Darren Mollendor, PE City and County of Denver Public Works Wastewater Management

South Federal Blvd. Project Background

- Reconstruction of state highway
- Drains to Harvard Gulch in SW Denver
- Located in urbanized retail / multi-family residential area
- Project extends from Jewel Ave. north to Florida Ave.
- PLD pilot study area is located between Florida Ave. and Arkansas Ave.

Pilot Study Area



Out of the Box Approach Linear Project WQ Concerns

- Right of Way take for Surface WQ BMP
- Underground design considerations
 - Site conditions
 - Location
 - Operation and Maintenance
- Constructability
 - Use of Rain Store 3 for underground storage
- Monitoring data
 - Phase 1 hydrograph analysis
 - Phase 2 Hydrograph, analytical, and *piezometric* evaluation

Pilot Design and Installation

- Combined PLD and Sand Filter designs
- Used Rainstore 3 for volumetric control
- No under drain
- Elevated outlet structure
 - Goal to infiltrate WQCV
- Impermeable Perimeter Liner
- In series treatment train
- Concentrated storm inflow from adjacent parking lot

Multi Basin Schematic Diagram

• To Be Provided
End Cap Cross Section



Typ. Outlet Cross Section



Typ. Maintenance Port Cross Section



Rainstore 3 Underground Volumetric Storage





Rainstore 3 Details

Rainstore is a stackable, plastic structure designed to store large amounts of stormwater underground. Rainstore has a 94% void space and is designed to support heavy loads (such as light vehicular traffic) when used in combination with Geogrid materials. Approximate pricing for Rainstore units and additional required products are as follows:

- • Rainstore3 Unit: \$30-\$38 per unit
- • Geogrid: Tenax \$11 per linear foot (13 foot width); Meeks
 - StrataGrid \$3.44 per linear foot (6 foot width); The Rock Garden
- • Geotextile Fabric: \$2 per linear foot (12 foot width)

• Materials:

- • Rainstore Units (40" x 40" x 4")
- • Non-Woven Geotextile Fabric (Filter Fabric)
- • Geogrid Tenax, StrataGrid, or equivalent. *Recommended for all driveway infiltration applications*
- • Zip Ties
- Drain Rock (³/₄ 1 ¹/₂")
- • Sediment Trap or Catch Basin

North PLD Treatment Basin Hydrograph Data (1)



North PLD Treatment Basin Hydrograph Data (2)



North PLD Treatment Basin Hydrograph Data (3)



North PLD Treatment Basin Hydrograph Data (4)



South PLD Treatment Basin Hydrograph Data (1)



South PLD Treatment Basin Hydrograph Data (2)



South PLD Treatment Basin Hydrograph Data (3)



South PLD Treatment Basin Hydrograph Data (4)



"Out Of The Box Off The Shelf" Linear Project Hybrid PLD Pilot Study Conclusions

- Pilot PLD is functioning as intended
- No significant maintenance is required to date
- Hydrographs show Class "C" soil allow infiltration (entire WQCV)
- Stormwater Rip Rap intake insure system functionality
- System treats frequent (2yr) and 1.35"+ Storms





castlewood canyon dam, 5300 acre-ft

CHERRY CREEK DROP #27





cherry creek at 11th Ave 11 とたの



the flood







area of interest







 1935 Kenwood Dam was constructed to provide flood protection for the

> City following a disastrous flood in 933 that conveyed 34,000 cfs towards downtown.

- Republican River flooding in 1935 indicated it was underdesigned.
- In 1944, the Kenwood Dam was decommissioned to accommodate the construction of the Cherry Creek Reservoir.

• The end sill of the stilling basin forms the crest and face of this existing drop structure.

CHERRY CREEK DROP #27

genealogy of drop structure #27



Existing conditions Cherry creek drop structure #27





area of concern





164 feet wide at crest and 18-foot vertical drop

Collapse of boulder face material creating an expansive boulder rubble field



CHERRY CREEK DROP #27

challenging issues







Downstream channel degradation, severely eroded channel banks and loss of sediment impacting water quality



CHERRY CREEK DROP #27

challenging issues

Cherry Creek Dam embankment

Hwy 225

JFK golf course

Cherry Creek upstream of Drop Structure #27 Rehabilitate a failing drop structure
Stabilize eroded channel and banks
Dissipate the yearly releases from the DAM to protect downstream infrastructure, properties and channel integrity

 Enhance the riparian corridor ecosystem

Create an aesthetic amenity

CHERRY CREEK DROP #27

project purpose

Design solution :

- Incorporate existing Dam structure with review and approval from by the Army Corps of Engineers
- Structurally withstand the 100-year event
- Arrest the erosion at the drop structure and stabilize the downstream reach
- Re-vegetation restoration must withstand the high velocities and sheer stresses associated with the alternate yearly releases of 1500 cfs and 300 cfs immediately after construction and maturity
- Preserve an existing vegetated island that supports wildlife
- •Utilize sustainable construction methods

CHERRY CREEK DROP #27

project approach



design inspiration



project concept



- Removal of existing riprap along the dam face, reuse material for channel stabilization
- Confine the crest width from 164' to approximately 92'
- Base flow will be contained in 6 cantilevered galvanized steel troughs
- •Face the wall of the drop structure with Glass Fiber Reinforced Concrete
- Re-alignment of channel and grading of overbanks
- Installation of a grouted boulder plunge pool
- •Utilize bioengineering methods to stabilize channel toe

•Re-vegetation that incorporates riparian and upland species

CHERRY CREEK DROP #27

project improvements



planting concept



vegetation restoration



•Accommodate the design flows of 1500 cfs and 5000 cfs

•Average daily stream flow of 8.4 cfs will crest over 6 new low flow notch weirs ranging from 10 feet wide to 4 feet wide

CHERRY CREEK DROP #27

hydrology and hydraulics



critical USGS gauging station enhanced








building the vision



building the vision



the flood of 2008



the flood of 2008



the flood of 2008



post construction October 2009

CHERRY CREEK DROP #27



post-construction May 2010

CHERRY CREEK DROP #27



post construction May 2010

CHERRY CREEK DROP #27

Project team

Urban Drainage Flood Control District City and County of Denver Matrix Design Group Naranjo Construction Muller Engineering Abstract Elmer's Twomile Greenways Project Boulder, Colorado

Annie Noble – City of Boulder Mark Post – Centennial Engineering Mike Galuzzi – WH Pacific

The Elmer's Twomile Greenways project is located in north Boulder between 26th and 28th Streets in one of the most developed urban corridors of the city. The project included a grade-separated, multi-use path connection from Goose Creek to Glenwood Drive, a combined bicycle/pedestrian and flood conveyance underpass at Valmont Road and 100 year flood mitigation improvements. In addition to a completed multi-use path connection, the City's overall goals included complete conveyance of the 100 year storm event, limiting impacts on existing development, and providing areas of open channel and wetlands wherever space allowed.

The transportation improvements provided a missing link in the path system between the area north of Glenwood Drive and the entire Boulder Greenways path system. The flood mitigation improvements address flooding that would occur south of Glenwood Drive to the confluence with Goose Creek during a 100-year storm event. Numerous properties east of the Elmer's Twomile channel along 28th Street were in the 100-year conveyance zone, and portions were also in the city of Boulder's high hazard zone. This project removed these properties from the 100-year floodplain by containing the flows within the newly completed Elmer's Twomile channel. In addition to providing flood and transportation improvements, the project also included habitat and water quality enhancements.

As part of this project, the city purchased a 1 acre easement which allowed for the development of a constructed wetland in a narrow urbanized corridor. This project was a cooperative effort with funding and oversight provided by the City of Boulder, the Urban Drainage and Flood Control District and the Colorado Department of Transportation. The Elmer's Twomile Greenways project from Goose Creek to Glenwood Drive including design, property acquisition, construction and the Letter of Map Revision cost approximately \$8.8 million. The project was funded through the city's Flood (\$2.87 million) and Greenways (\$1 million) Capital Improvement Program, with additional funding contributions from outside funding sources including the Federal Transportation Improvement Program (\$3.25 million) and the Urban Drainage and Flood Control District (\$1.68 million).

Project Background

The City of Boulder recently completed the construction of the Elmer's Twomile Greenways project. Elmer's Twomile Creek is part of the City of Boulder's Greenways system, which is comprised of a series of corridors along riparian areas including Boulder Creek and its tributaries. The purpose of the Greenways program is to integrate multiple objectives, including habitat protection, water quality enhancement, storm drainage and floodplain management, alternative transportation routes for pedestrians and bicyclists, recreation and cultural resources. The Elmer's Twomile project provided an opportunity to maximize the overlap of these objectives through the coordination of various city departments and outside agencies. The overall project was a team effort, combining input from Flood Utilities, Transportation, Parks and Recreation, Water Quality and Environmental Services, Environmental Affairs, Planning and Open Space and Mountain Parks, in addition to two outside agencies: the Urban Drainage and Flood Control District and the Colorado Department of Transportation. Engineering and design was provided by the City's on-call consultant team of Centennial Engineering and WH Pacific.



The Elmer's Twomile Greenways project is located in north Boulder between 26^{th} and 28^{th} Streets in one of the most developed urban corridors of the city.



The conceptual design for the project was initiated in March 2004 with the first open house, as part of the city of Boulder's extensive Community and Environmental Assessment Process (CEAP). The CEAP evaluated three alternatives for the southern portion (Phase I) of the project and two alternatives for the northern section (Phase II). The chosen alternatives included a combined pedestrian and flood drainage underpass at Valmont Road, with a wider channel width north of Valmont Road.



Northern Section of Elmer's Twomile



Southern Section of Elmer's Twomile

Through the public input process, the plans for the northern portion of the project were changed to include an underground box culvert between the Willow Brook Condominiums and Tebo Plaza rather than an open channel. This modification was made to limit impacts on trees and reduce encroachment on the Willow Brook properties and parking spaces at Tebo Plaza, due to limited space for a conveyance channel. The atgrade connection from the Elmer's Twomile path south of Valmont was also modified to reduce impacts on trees along the Boulder and White Rock Ditch.

The project completed 0.5 mile of a missing link in the multi-use path system between Glenwood Drive and Goose Creek, including a grade separated underpass at Valmont Road. The Flood mitigation improvements removed numerous properties from the 100 year floodplain. South of Valmont Road, the flood mitigation improvements included 359 feet of 13'X5' box culvert between Valmont Road and the confluence of Goose Creek, which passes under the Shady Hollow parking lot. The box culvert opens up into

a 6000 sq. ft. pond and wetland area at the confluence with Goose Creek. North of Valmont Road there is a 10,000 sq. ft. pond and wetland area. Upstream of this wetland is a 643 ft section of 12'X6' box culvert which passes under the Tebo Plaza parking lot. At the north end of the project, at Glenwood Drive is a third wetland area of approximately 3000 sq. ft.

Public Health Safety and Welfare

The Elmer's Twomile Greenways project provided enhancements to public health, safety and welfare from the perspective of removing properties from the 100 year flood plain and the city of Boulder's high hazard flood zone, as well as improving the safety of pedestrians and bicyclists. In addition to improving safety, the improvements promote public health by encouraging people to use alternative transportation.



This path connection is located in a densely populated neighborhood, with three different condominium associations located adjacent to the project on the west side and the commercial strip along 28th Street on the east side of the project. This project also serves a significant population density to the north and south, providing access to commercial centers along 28th Street and connectivity to the Goose Creek and Boulder Creek path system. Attached is a map which depicts the floodplain prior to the flood mitigation improvements.

Enhancement of the Surrounding Environment through Unique Solutions

This project enhances the surrounding environment. Prior to the construction of these improvements, Elmer's Twomile Creek was an undersized small concrete trapezoidal channel with chain link and wooden fences on both sides. Rayback Plumbing used the one acre parcel to the east of the channel, and north of Valmont Road as a storage area for hundreds of used sinks, toilets, bathtubs and plumbing parts. South of Valmont Road, the channel passed behind a strip mall and flowed into the Boulder and White Rock

Ditch. The area adjacent to the channel was viewed as a no man's land and was a dumping ground.

The existing channel passed through a very developed urban corridor, with limited space to allow for an open channel that would contain the 100 year storm event. Several channel width options were evaluated prior to eliminating the open channel concept for the underground box culvert. A wider, open channel (36 feet wide) would have required the removal of 50 parking spaces in Tebo Plaza and all of the mature trees east of Willow Brook Condominiums. The channel would have retaining walls five to eight feet high on both sides, with the distance between the retaining wall on the west side of the channel and the Willow Brook Condominiums as close as 10 feet. By reducing the channel width to 30 feet and moving the channel closer to the Willow Brook Condominiums, the number of parking spaces impacted would be reduced significantly, but the height of the retaining walls would increase and the distance between the retaining wall on the west side of the channel and the condominiums would be as close as four feet. In these areas, box culverts were installed in order to minimize impacts on adjacent properties.

Underpass structures were designed with a minimum cover, which shortened lengths and maximized the natural lighting and openness. Where space was available, wetland pond areas were created to provide water quality, habitat and aesthetic enhancements. The project was also landscaped in such a way to provide privacy to adjacent property owners and enhance the user experience. While it is not the city of Boulder's preference to utilize box culverts in lieu of an open channel, this approach made it possible to minimize impacts on existing vegetation and urban development.

Multiple Objects, Budget and Schedule

This project achieved multiple objectives. It provided a missing link in the grade separated path system, with connectivity to commercial areas and the entire Greenways path system. It removed numerous properties from the 100 year floodplain and the City of Boulder's high hazard zone. It provided water quality, habitat and environmental improvements and it enhanced the economic vitality of an important commercial area, as well as improving the aesthetics of a high density residential neighborhood. The project was designed and built by the City of Boulder in cooperation with the Urban Drainage and Flood Control District and the Colorado Department of Transportation. Flood utilities funds were leveraged with federal transportation funding. The project required 22 easements from nine property owners, three of which were homeowners associations with numerous residents. In addition to addressing the various interests and concerns of adjacent property owners (privacy, security and aesthetics) water rights issues and ditch crossing concerns were also addressed with the Boulder and White Ditch Company. This project was completed within the specified budget and schedule.

This project can serve as a model for other communities and other city of Boulder projects.

Before and After Photographs



Before – (Looking North) South End of Project at Confluence with Goose Creek



After – (Looking North) South End of Project at Confluence with Goose Creek



Before – (Looking North) Just North of Valmont Road



After – (Looking North) Just North of Valmont Road



Before – (Looking North) North of Valmont



After – (Looking North) North of Valmont



Valmont Road Underpass



Confluence with Goose Creek



Path Connection on North Side of Valmont Road



Wetlands at Glenwood Drive



Wetlands at Confluence with Goose Creek



Wetlands North of Valmont Road

Hildebrand Ranch Open Space Park Trailhead Parking Area

Use of Permeable Interlocking Concrete Pavers







Project Problem Statement - Goals

- Over 1653 acres
- Preserve agricultural heritage
- Preserve natural resources
- Provide trail-based recreation
- Provide public access for trailhead (currently 4 miles of trail)
 Bicycling
 Equestrian
 Hiking
- Expandable for future use





Hildebrand Ranch Trailhead Parking Area



MULLER

Public Health, Safety & Welfare

Maintains water quality

Reduces runoff volume and peak flows

• Facilitates groundwater recharge



Hildebrand Ranch Trailhead Parking Area



Enhancing the Environment



- Addressed water quality requirements
- Enhances natural surroundings
- Appropriate to setting with organic shades of brown
- Sensitivity to environment is core value of Open Space and expected by its constituents



Hildebrand Ranch Trailhead Parking Area



AULLER

Unique and Innovative Project



- First PICP project approved by Jefferson County P&Z
- One of the largest PICP installations in Colorado
- Unique partnering and collaboration



Hildebrand Ranch Trailhead Parking Area



ULLER

Multiple-Objective Management

- Jefferson County:
 - Open Space Maintenance
 - Planning & Zoning
 - Transportation & Engineering
 - Road & Bridge
 - Construction Management
- UDFCD
- Advanced Pavement Technology and Michelle DeLaria









Hildebrand Ranch Trailhead Parking Area



Parking Lot Design - Layout



Alternatives Evaluated

Traditional asphalt
Porous Asphalt
Pervious Concrete
PICP



Hildebrand Ranch Trailhead Parking Area





Parking Lot Design – Paver Subgrade







- Existing soils below sub-base
- Open-graded aggregate layers
- Compaction
- Interlocking Concrete Pavement Institute (ICPI) criteria





Hildebrand Ranch Trailhead Parking Area



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Parking Lot Design - Pavers

- Aqua-Bric (Borgert)
- Selection criteria
- Use of colors
- Recycled plastic wheel stops
- Mechanical installation









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Hildebrand Ranch Trailhead Parking Area

Project Meets Goals Effectively

- Budget
 - ✓ Overall
 - ✓ Cost per square foot
 - ✓ Life cycle benefits
- Schedule





Hildebrand Ranch Trailhead Parking Area



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Drainage Design Goals

 Obtain a waiver from Jefferson County detention requirements

 Avoid a FEMA floodplain revision

 Utilize existing alluvial sandy soils for infiltration of runoff





Hildebrand Ranch Trailhead Parking Area



Drainage Design Elements

- Overall drainage pattern
- Detention waiver criteria

- Water quality treatment
- "Modified" Porous Landscape Detention (PLD)


Monitoring Wells



•UDFCD is monitoring water levels in comparison with nearby rain gage data

•Determine drain time and changes over time; clogging

•No water quality chemical data collected









Lateral Flow Barriers - Lessons



- Liner thickness recommendations: 40-50 mil
- Lateral flow patterns









MULLER



Model Project





- Demonstrate applicability to Colorado
- Introduce technique to Jefferson County work groups
- Increased public awareness of water quality with interpretive signs
- Mechanical installation training
- Maintenance buy in and training
- UDFCD test site



Thank You For Coming! Questions?









McIntyre Gulch Enhancement at the St. Anthony's Hospital Site, Denver Federal Center, Lakewood, Colorado

The new St. Anthony's Hospital in Lakewood, Colorado is scheduled to open in the spring of 2011. Although not yet helping patients, the hospital has already brought considerable benefit to the 900- foot section of McIntyre Gulch within its boundaries, as voluntary enhancements of this urban stream were completed as a part of the site remediation and hospital construction project. Walsh Environmental Scientists and Engineers, LLC (Walsh) provided assessment, design, permitting, construction documentation preparation, and construction support services.

Pre-project conditions in the Gulch were typified by a deeply incised and actively eroding corridor, including a 180- foot section of near vertical bank with heights reaching up to 15 feet. Such conditions posed a potential safety threat, increased fine sediment loading to downstream waters, and limited both floodplain function and public access to the gulch. Historic channelization of a meandering portion of the reach, and placement of construction debris in the cut-off meander left waste south of the Gulch, and right up to the channel in some locations. Both the understory vegetation and riparian canopy were intermittent and sparse due to a lack of sustainable hydrology, and were primarily comprised of upland grasses and weeds. Further compromising the stability of the reach, the confluence of the south branch of McIntyre Gulch with the main stem was constructed decades ago at a hydraulically unfortunate 90 degree angle.

Constraints and challenges were numerous for this small stretch of urban stream. Physical constraints included the narrow and deeply incised corridor, as well as lateral constraints imposed by remediation requirements and proposed land uses. The project employed multiple-objective management to fulfill its widely varied goals of landfill remediation, stream corridor enhancement, and providing safe accessible recreation opportunities for all.

To accomplish the multiple goals, Walsh utilized a creative approach that mimics natural features to improve the health and function of this stream reach, as well as its safety and opportunities for public enjoyment. All waste adjacent to the Gulch was removed and banks were regraded to mild slopes in a manner that maximized preservation of isolated mature cottonwoods and willow stands. Walsh designs applied varied grading such as low planting benches and small boulder walls to break up the uniformity of the channelized section, restore floodplain function, and provide unique local diversities in soil and water conditions to enable specialized plantings. Natural bedrock formations were exposed during waste removal, prompting the upgrade of a proposed grouted sloping boulder drop structure at the south branch confluence to a sculpted concrete cascade that fits the natural setting of the gulch, provides increased stability to the reach, and ensured preservation of the largest streamside cottonwood tree. The cascade was shaped and stained to match the existing bedrock and included innovative micro-grading to create "precip pools" to hold water for birds and other wildlife. All enhancements were designed to be consistent with UDFCD guidelines and standards to ensure maintenance eligibility for the project reach. The project has already served as a model for other projects, as UDFCD has recommended it as an example for a downstream section of the gulch. The project stayed within budget even with the upgraded drop structure, as the sculpted cascade

Blair E. Hurst, P.E. bhurst@walshenv.com Walsh Environmental Scientists and Engineers, LLC naturally accommodated the steep gulch sideslopes and eliminated the need for expensive grouted boulders.

Further successes include accommodating several proposed land uses, such as vehicular and pedestrian crossings, a new bike path paralleling the north bank, and surface water spillways and pipe outlets in to the Gulch, in a way that would impart the most natural function and appearance on this stream system. The vehicular crossing is a free span, open bottomed structure that reduces impacts on stream hydraulics and the natural channel bed. Spillways were vegetated with native grasses and shrubs.

Vegetative improvements, such as removal of weed tree species acting as a seed supply, and extensive planting of a diverse mix of native trees, shrubs and grasses replenish what was lost in this urban area - the invaluable "green line" of a healthy and functional riparian corridor.

Views of near vertical cutbank in McIntyre Gulch prior to project initiation



Looking upstream (west) from top of bank at the future Routt Street crossing area. Note bedrock cascade in the distance for reference.







Bank heights limited floodplain function and access to the gulch.

Views of regraded banks and planting of native vegetation

Looking upstream (west) from the new Routt Street crossing. Note bedrock cascade and building in right corner for reference. South bank has been regraded after waste removal, seeded and planted with native shrubs and grass plugs.

Also visible are small boulder walls to add topographic variety to banks, bikepath, and preserved willow stand.





View to the east of rock-log deflectors placed at the toe of the newly graded slope immediately upstream of the bedrock outcrop exposed during waste excavation. The Routt Street crossing is visible in the background. Note existing stand of willows on left; a soil riprap rundown from the north bank was planned in this area. It was decreased in size to preserve this quality vegetation Looking downstream (east) at south bank just below the sculpted concrete cascade. Note preserved cottonwood trees.

Large corrugated metal pipe is a temporary pedestrian crossing. A permanent pedestrian bridge will be installed, whose location was carefully selected to preserve trees.



South branch confluence area, before cascade construction



View upstream at confluence. Note 90 degree angle between South branch structure wingwalls and McIntyre Gulch mainstem, as well as scour hole.

Pre-project conditions looking downstream from confluence. Note lack of floodplain access and riparian vegetation.





Construction of the sculpted concrete cascade included raising the channel bed to repair and reinforce the scoured area, protecting the north bank from south branch flows, and preserving all of the cottonwood trees in the vicinity.

The cascade was sculpted in a naturalized fashion and includes small "precip pools" to hold water for birds and other wildlife.

Constructed sculpted concrete cascade



View to the west



View to the southeast

View from parking area





Natural bedrock outcrop exposed during waste excavation used as a model for the sculpted concrete cascade.

Staining of the sculpted concrete to match existing outcrop.



A System Approach to Watershed Planning



September 23, 2010



- Watershed Impacts from Development
 Purpose of Watershed Planning
 Conventional Watershed Planning

- System Approach to Watershed Planning
 Summary

What is a Watershed?

A watershed is the area of land where all of the water that is under it or drains off of it goes into the same place. John Wesley Powell, scientist geographer, put it best when he said that a watershed is: "that area of land, a bounded hydrologic system, within which all living things are inextricably linked by their common water course and where, as humans settled, simple logic demanded that they become part of a community."





System Definition

A group of interacting, interrelated, or interdependent elements forming a complex whole.²

Watershed Impacts from Development

- Increased Runoff
- Increased Flooding
- Water Quality Problems
- Stream Degradation
- Habitat Destruction
- etc...

Purpose of Watershed Planning

- Infrastructure Sizing
- Detention Sizing
- Channel Improvements
- Fee Development

Conventional Watershed Planning

- Flood Control
- Flood Conveyance
- Safety





Watershed Concerns

- Higher than Historic Peak Flows are Being Released
- Channel Instability
- Habitat Destruction
- Water Quality Issues









Goal & Objectives

Goal

Create a Sustainable Watershed Plan

- <u>Objectives</u>
- Provide an Amenity to the Community by Restoring the Aesthetic Value of the Corridor
- Protect the Environment by Restoring Habitat & Implementing Water Quality
- Provide an Economic Benefit to the City by Implementing costeffective and low maintenance solutions
- Provide Flood Control & Safety

Philosophy

- Floodplain Preservation is Paramount
- Incorporate Natural Channel Design Everywhere Possible
- Manage Low Flow Hydrology

Alternatives Analysis & Screening

- Hydrology
- Detention Ponds
- Reaches

• Foundation of a Watershed Plan

Importance of Hydrology

- Has to be Done Correctly
- Low Flow Hydrology is Critical
- Impact on Alternatives
- Impact on Costs

Detention Pond Analysis & Screening

- Detention Pond Alternatives
 - None (Full Channel Conveyance)
 - 2-yr Flood Control
 - 100-yr Flood Control
 - Full Spectrum Detention (EURV + 100-yr)
- Evaluated All Possible Locations
- Optimized Locations Based on Peak Flow Reduction
- Retrofit Existing Ponds Where Possible





Parameter	Full Conveyance	2-Year Detention	100-Year Detention	Full Spectrum Detention
Detention Pond Construction Costs	++	1. 1.14	(an an	
Reach Construction Costs	9 . .		543 1	
Detention Pond O&M Costs	20	322	42	122
Reach O&M Costs	-	19 - 10	· • ·	· · ·
Full Benefit of Previously Constructed Reaches	++	2.+ C	5 - 0	
Cost for Unimproved Reaches	272		+	+
Control of the 2-year Flood Event		+ +		++
Control of the 100- year Flood Event	377		+	+
Reduced Peak Discharge into Monument Creek	8772	979).	+	++
Flexibility for Development		1	+	+
Lot Premium	÷	+	(- 1)	+
Habitat Improvements	9 24	24	543	+
Water Quality	v	+	+	.++
Total	-14	-6	-6	3

Detention Pond Analysis & Screening



- Control of the 2-yr Flood
- Reduced Peak Discharge into Monument Creek
- Water Quality

Construction Costs ~ Same as 100-yr Detention
O& M Costs ~ Same as 100-yr & 2-yr Detention

Reach Analysis & Screening

- Implement Natural Channel Design Everywhere
 Possible
- Small Drop Structures (<3ft height)
- Large Drop Structures (<6ft height)
- Fully Lined Channel

Provide a Continuous Wildlife Corridor
Natural Channel Design Benefits

- Aesthetic Value
- Habitat Creation and Preservation
- Typically Lower Construction Cost Than Conventional Approaches
- Water Quality Benefits
- Channel Function
- DCM Criteria for Limiting Erosion

Natural Channel Design Screening Parameters

- Shear Stress < 2/b/ft²
- Channel Slope < 2%
- Belt Width < Available Width









Reach Analysis & Screening Summary

Alternative	Length (ft)	
No Alternative Needed	79,523	
Adopt Alternative	51,803	
Infrastructure Sizing ¹	13,163	
Natural Channel Design	28,759	
Small Drop Structures	43,358	
Large Drop Structures	op Structures 938	
Fully-Lined Channel	0	
Total	217,546	

¹Only includes storm sewer infrastructure sizing, not bridge or culvert crossing sizing.







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719-575-0100





Aurora *****

2008

Developing New Local Construction Stormwater Discharge Regulations Through Partnership and Stakeholder Collaboration

Colorado Association of Stormwater and Floodplain Managers 21st Annual Conference: "Coming of Age" Stormwater Management and Water Quality Session Silvertree Lodge - September 23, 2010



Sean Lieske Permitting and Environmental Compliance Manager Aurora Water

Tiffany McEachen PE CFM Project Manager CH2M HILL



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2008



Population - > 314,000 Accounts - > 75,000

Services – Drinking Water, Wastewater & Stormwater

Service Area – 151 sq. miles







	City of Aurora 2009 Long Range Population Projection		CITY OF AURORA	
42	2 YOU. STOL	Year	Official Estimate	
1012		2000	276,393	
	ABLANT MALE AND	2001	284,606	
rora	900.000 910.000 910.000	2002	287,895	
* * *	E exten	2003	292,158	
	INCOME DIVISION DIVISIONA DIVISIO DIVISIONA DIVISIO DIVISI	2004	298,303	
	The second s	2005	303,833	
008		2006	306,908	
	101.000	2007	309,416	
		2008	313,144	
	1880 1985 2000 2005 2018 2015 2020 2025 2020 2015 2048 2045 2050 2055 VEAK	2009	314,326	



AURORA WATER

Au

21













2008



- *Operating Budget–* \$101 million (2010)
- *Treated Water–* 45,364 AF (2009)*
- *Raw Water Supply* 69,843 AF
- Average Use 121 gpcd (2009)*

Background









6 in

5 in

4 in .

3 in -

2 in

1 in

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2008



Jan Feb Mar Apr May Jun Jul Aug Sep Oct Nov Dec

Precipitation

Average Precipitation 15 – 18" per year

> US Average 30 – 40" per year

Average Snowfall 50 – 63" per year

US Average 20 – 28" per year





City

Average

US average





2008



Why St



City of Aurora Regulations

Regarding Stormwater (Quality) Discharge for Construction Activities



ons?

iment Phosphorus en





2008



Growing City

Tension Between Inspections and

Development Community

Setting Clear Expectations

Stand Alone, Easy to Understand

Regulations

AURORA WATER

Why Develop Regulations?



2008

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Context for Development of New City Construction Stormwater Regulations

The Mandate

- Start Over
- Develop a Clear, Consistent Regulations Manual
- Be Collaborative, Reasonable, Fair
- Train Staff
 - Implement the New Regulations











2008

Development of Aurora's **Construction Stormwater Discharge** Regulations

- **Overall Vision**
- External Stakeholder Concerns and Collaboration



Consideration of Other Municipalities' Programs Ο and Manuals



- Internal Stakeholder Concerns and Collaboration
 - **Applying Consistent Standards to Internal City** Ο Projects



2008

Development of Aurora's Construction Stormwater Discharge Regulations

Overall Vision

- One Clear Process and Set of Requirements
- Appropriate Opportunities for Flexibility
- Stormwater vs. 'All Things Environmental'
- Regulations vs.'Specifications'











2008

Development of Aurora's Construction Stormwater Discharge Regulations

External Stakeholder Concerns and Collaboration







 Consideration of Other Municipalities' Programs and Manuals







2008

Development of Aurora's Construction Stormwater Discharge Regulations

- External Stakeholder Concerns and Collaboration
 - o Terminology
 - o Clarity



o Reasonableness

AURORA WATER

- o Announced vs. Unannounced Inspection





2008

Development of Aurora's Construction Stormwater Discharge Regulations

Internal Stakeholder Concerns and Collaboration

o Plans Review



o Inspection







2008

WATER

Development of Aurora's Construction Stormwater Discharge Regulations

Internal Stakeholder Concerns and Collaboration

 Applying Consistent Standards to Internal City Projects















2008

Development of Aurora's Construction Stormwater Discharge Regulations

• Internal Stakeholder Concerns and Collaboration

 Need to Improve the Quality of Stormwater Management Plans

• Need to have clear requirements for inspection

• Need to have clear enforcement processes







1. Training

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- 2. Communication
- 3. Good Judgment

Implementation

4. Fine Tuning







2008













Ugly









2008



- *Who who's* responsible?
- What what are they requesting?
- When timeframe?
- *Where* specifics on location?
- How application?









2008



March 2010

¹ The City may study be been by City's advancement sequence depending ages for investig, magnitude, report poster location of the standard defensively. Build and argo as off one reliance

¹⁰ Obj. of Averag (SOA) Resides impositions are located on the results of an impact analysis and proceeds are consisted assumiting in the following. High Impact = 1 imposition per marks, Reduce impacts - 1 imposition for exercising the regards - 1 important per sporter. Since many and per constraints are per for the following of the following of the important region of the regards of the region of th

¹ If all that discharge or off-site mission is install during the montes of a following trajectory, the site and ise instead as 107/0033000 is accordance with the promoteries

E30409T4-1

¹ A site invasing flow (2) reduces if non-completer for the same wave while a sit (2) isorif period, regardless if whether they are the least of a following or inplies regardles, will be insured a reduce 2001). If the one fully the important following the insured ROV for the same when its (2) months, the oth will be insured a sing work areas (2002). Places that the basely and regardless of the same following the insured ROV for the same when its (2) months, the oth will be insured a sing work areas (2002). Places that the basely and regardless of the size areas in a single same insure areas insured.

Inspection & Enforcement





Process



2008

AURORA WATER

- *What* Construction Sites Program Oversight Review
- Who CDPHE Staff & Contractor
- *When –* April 2009 July 2010
- *Where* Phase I MS4 (Aurora, Denver, Colorado Springs)
- How Phased Approach









Involve Stakeholders



Limit Opportunities for Comment

Expect Future Revisions



essons Learned



8881





2008

Stormwater Check-in Meetings



Reviewing and Modifying Regulations



Training



Internal Auditing

Enforcement



Ongoing Efforts





2008



Questions/Comments

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> Tiffany McEachen PE CFM Project Manager CH2M HILL tmceache@ch2m.com 720-286-5066

Holly Hills Detention Ponds

RETROFITTING A DETENTION POND WITHIN LOT(S) OF AN ESTABLISHED RESIDENTIAL SUBDIVISION.

Holly Hills Detention Ponds

Located within Arapahoe County, East of I-25 near Yale Avenue

Holly Hills Detention Ponds

Participants: UDFCD, Arapahoe County, and SEMSWA

Muller Design/Construction Team: Muller, Wenk Associates, Koch Environmental, Poitra Visual and Territory Unlimited

Holly Hills Detention Ponds


Holly Hills Detention Ponds 2585 OSP Plan



Holly Hills Detention Ponds 3001 OSP Plan



Arapahoe County acquired two properties; one at each pond site

Houses need to be removed



Design Phase:
Look at the Pre- and Post-Flooding Conditions, for multiple frequency storm events
Show the Public how the project will reduce flooding problems
Evaluate the demolition issues
Refine the OSP plans into a final design

Illustration of flooding levels : Post Project Conditions



Public Involvement Meetings were conducted



March 2005

Insert video animation here or pause power point and come back to it later.

The demolition of the dwelling structures brought in a hazardous waste evaluation due to the age of the structures. Koch Environmental assisted with the evaluation and determined that special demolition procedures were required.

2585 Design Plan



3001 Design Plan



Construction Phase:

The Demolition was contracted separately due to the special demolition required.



ASBESTOS CANCER AND LUNG DISEASE HAZARD KEEP OUT AUTHORIZED PERSONNEL ONLY

DANGER

RESPIRATORS AND PROTECTIVE CLOTHING ARE REQUIRED IN THIS AREA.

Pond Construction Phase:















Retail Drainage

01

How to Derign local Site Drainage for Safety. Exceptional Appearance. and Problem Avoidance

Ьу

Peter I. Nelson, PE. EXW



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Poorly executed grading and drainage :

- Detract from the functionality of the civil infrastructure
- Damage buildings and pavements
 Increase liability issues
- Thoughtful devign approaches:
 Avoid civil infrastructure problems
 Enhance safety
 Enhance aesthetics.



- •Chase does not drain!
- •Curb is cut and it still does not drain.



This is embarrassing.



Trench drain runs into block wall.
Below grade extensions have sags.
Walk traps runoff.
Runoff slope is flat.

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N







 Downspout extension is built with a sag.

•Stain patterns indicate runoff is going elsewhere.





•Downspout extension cannot be lowered to the correct position.

•Where was quality control construction observation?



Depending on geometry, poorly drained sites can retain up to 80% of



precipitation runoff within the immediate vicinity (~10-feet) of buildings.

What is volume available for storage?





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Calculations use 1-inch of width for volume. $4 \times 40 / 2 = 80 \text{ in}^3$ Assume uniformly graded gravel, 44% porosity. Max volume stored = $80 \times 0.44 = 35.2 \text{ in}^3$ Building Width = 60'; $\frac{1}{2}$ BW = 30'Tributary Area = $(60 / 2 + 10) \times 12$ in / ft = 480 in² Depth of runoff stored = 35.2 / 480 = 0.073 in Pervious area = 10/(60 / 2 + 10) * 100 = 25%



Initial Abstractions (use 5-min): depression storage = 0.05" (UDCM tbl RO-6 sr) infiltration = 0.201" (hsg C or D tbl RO-8) evaporation = insignificant in 5 minutes Volume of rainfall not running off = 0.073 + .05 * .75 + .201 * .25 = 0.161" Rainfall (NOAA) 2-yr 100-yr 6-hr 1.5" 3.55" 24-hr 2.1" 4.9" 1-hr 0.98" 2.32 0.28" 5-min 0.67" 0.57% 0.24% % captured N

The water thus retained:

- Infiltrates into the ground next to the building.
- Raises the water table.
- Detracts from the functionality.
- Detracts from the safety of the site.
- Increases damage to buildings including:
 - Deterioration of the structure (mold, rot, etc.).
 - Intrusion of water into interior spaces.
 - Cracked walls and sticking doors.



When expansive soils are present, the damage from poor drainage may exceed ordinary damage and render a building useless.



Images are from Special Publication 43, A Guide to Swelling Soils.



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Pavements are damaged through soil movement where drainage is poor.



Image is from Special Publication 43, A Guide to Swelling Soils.



© Pl Nelvon Engineering. Inc.

Ice accumulates where drainage is poor.



© Pl Nelzon Engineering. Inc.

Where drainage is poor, pavements are damaged through the process of scaling, sometimes called salt scaling. Scaling is not a chemical process. It is a mechanical process wherein flakes of concrete are lifted from the surface of otherwise weakened concrete.




Safety is compromised by creating unexpected drop-offs where none existed a few months ago.





Much of poor drainage is hidden from view beneath the mulch and/or vegetation. Trapped water is normally accounted among the initial abstractions in hydrologic modeling.



Methods for reducing retained runoff:

The cost of repairs frequently out runs the cost of the original civil infrastructure.



Figure 28. Property designed runoff slope next to a house foundation. Note that roof drainage is carried by a downspout extension to a point beyond the slope. (From Holtz and Hart, 1978.)

Figure 28 from Special Publication 43, A Guide to Swelling Soils.



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A Site with exceptional appearance that also functions well begins with design.







© Pl Nelzon Engineering, Inc.

Once water is allowed to drain away from buildings, pavements, and other at risk facilities, a site design should provide conveyance without ponding. These conveyance facilities contribute to a safe site and to exceptional appearance.





Once water is collected at a safe location, a site design should provide detention storage to release runoff in a manner similar to historical patterns. These storage facilities contribute to a safe site and to exceptional appearance.

Not a project of PLNE or Peter Nelson. © Pl Nelson Engineering. Inc.



ST DENVER INTERNATIONAL AIRPORT

Tackling Erosion Caused by Roadway Deicing Agents—Project Results

> by Catherine Rafferty, PE—Denver International Airport Rich Ommert, PE—Moser & Associates Engineering Lee Rosen, EI—Moser & Associates Engineering September 23, 2010

Presentation Outline

- Introduction to DIA's roadway deicing operations & erosion issues
- Observations
- Alternatives developed
- Alternatives installed
- Findings
- Future efforts



Introduction DIA Roadway Deicing

- DIA is located approximately 20 miles northeast of downtown Denver
- Access to DIA is via Peña Boulevard, which is a private road maintained by the airport
- DIA is a critical facility, as defined by the State, therefore Peña Boulevard must remain open at all times
- Standard operating procedure is to apply deicing agents as needed to maintain open road conditions even if application rates are higher than average



DIA-December 22, 2006 Blizzard





Introduction Erosion Issues

- Excessive roadside erosion exists
- Purpose of this study was to evaluate erosion mitigation measures along the roadway shoulder





Introduction Study Location

- Peña Boulevard from Tower Road to the Terminal
- Includes potential development areas
- Study area = 2,863 acres or 4.5 square miles





Observations Site Inventory

- Define location & types of problems occurring
- Over 500 photos were collected within the project area documenting problem erosion areas







Observations Site Inventory

 Collected data entered into GIS database to analyze potential patterns to the erosion that might indicate the root source of the problem





Observations Primary Causes

- Vehicular traffic pulling off the paved shoulder





Observations Primary Causes

Lack of stabilized maintenance paths





Observations Primary Causes

Lack of topsoil





Observation Erosion Pattern

- Minimal to no vegetation on shoulders receiving runoff



Observations Hypothesis

- Based upon the observations, and upon additional soils testing, it was concluded that DIA's roadside erosion was a result of:
 - Higher than average applications of deicer on the road salinating the shoulder soils such that vegetation was no longer viable
 - People attempting to avoid parking fees by pulling off onto the beyond the shoulders to wait for arriving passengers such that the soils are rutting and seed and mulch applications are torn up
 - Maintenance vehicles accessing areas that were never provided with drivable paths such that stabilized areas are disturbed
 - Poor soil conditions for establishing vegetation (high plasticity clay, no irrigation, no topsoil, etc.)

12

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Alternatives Developed

- Evaluated both "hard" and "soft" engineering solutions
 - "Hard" alternatives included installation of engineered structures
 - "Soft" alternatives included improving the soils with amendments, modifying the seed mix, run-on diversion, and operational modifications

Alternatives Developed





Alternatives Developed Valley Gutter





Alternatives Developed Underdrain Shoulder



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Alternatives Developed Maintenance Path



W. Law

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Alternatives Developed Reinforced Channel



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Alternatives Developed Soil Amendment

- Balance mag chloride
- Amend soil & blanket
 - Rip soil
 - MetroGro compost
 - Biosol
 - Humate





Alternatives Developed Seeding

COMPANY MARE	VIDITY	OF IN MIN	
COMMON NAME	SWOLT:		LBS FLS / AUR
INLAND SALTGRASS	NATIVE.	163	2.4
ALKAU SACATON	SALADO	475	0.6
WESTERN WHEATORASS	ARRIBA	43%	6.3
ALKALIGRASS	FULTS	475	0.6
NUTTALL ALKALIGRASS	NATIVE	2%	0.3
GARDNER SALTBUSH	NATIVE	27.8	1.2
SIDEDATS GRAMA	NINER	875	1.2
LITTLE BLUESTEM	PASTURA	675	0.9
GREEN NEEDLEGRASS	LOWDORM	8%	1.2
TOTAL			14.7
	ANNUAL SEE	D MIX	
COMMON NAME	WRIETY	S IN MX	LBS PLS / ACR



Alternatives Developed Seed Mix

- Oats (annual)

- Side Oats Gramma (native)





Alternatives Developed Seed Mix

- Western Wheat Grass(native)

Inland Salt Grass(native)



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Alternatives Developed Seed Application

- Drill Seeding
 - Truax Seeder
 - Depth
- Protection
 - ECB
 - Hydromulch
- Patience
 - Typically 2 to 3 yrs







ST DENVER INTERNATIONAL AIRPORT



Alternatives Developed Estimated Costs

	Valley Gutter	\$50/LF
	Underdrain Shoulder	\$60/LF
—	Maintenance Path	\$45/LF
—	Reinforced Channel	\$50/LF
_	Riprap-Lined Channel	\$50/LF
_	Soil Amendment	\$400/AC
—	Seeding	\$1,500/AC

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S DENVER INTERNATIONAL AIRPORT

Alternatives Installed

- Underdrain Shoulder
- Maintenance Path
- Reinforced Channel



Alternatives Installed Locations



S DENVER INTERNATIONAL AIRPORT

Alternatives Installed Locations

- Outbound Peña Boulevard
 - Highly visible
 - Exhibits areas of rill erosion, ditch erosion, and loss of vegetation





Alternatives Installed Locations

- Shady Grove Street
 - Contains a WQ basin that needs a maintenance path
 - Exhibits areas of rill erosion and loss of vegetation




Alternatives Installed Outbound Peña Boulevard

- Channel graded for constant longitudinal slope
- Reinforced shoulder constructed, then reinforced channel
- Annual seed mix/nurse crop not planted
- Soil was well mixed and clod free
- Entire area covered with ECBs
- Erosion control logs installed
- Delineator posts not reinstalled

Alternatives Installed Outbound Peña Boulevard





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Alternatives Installed Shady Grove Street

- Relocated electric utilities for clearance
- Soft shoulder built with geogrid, geomembrane, and underdrain in a linear progression
- Longitudinal slope critical for underdrains
- Multiple geogrids were installed to evaluate durability
- ECBs used over only part of the site
- Sterile sorghum nurse crop incorporated into seed mix

Alternatives Installed Shady Grove Street





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- No rill erosion adjacent to pavement
- Channel appears stable and invert has not deteriorated
- Almost no sediment transport has occurred
 - Less maintenance
 - Improved aesthetics
 - Improved WQ
- Spontaneous growth of "Poor Man's Alfalfa" (Kochia) successfully replaced function of annual nurse crop





O DENVER INTERNATIONAL AIRPORT

- Delineators not replaced; shoulder took some vehicular traffic in saturated conditions before vegetation established
 - Minimal damage occurred
 - Repeated traffic would permanently damage HPTRM/ECB
 - Repairs to subgrade and channel were very difficult
- Native grass began overtaking Kochia in 2nd season





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- No rill erosion adjacent to pavement
- Provides safe solid area that vehicles can pull off onto
 - Locations need to be evaluated for potential to encourage loitering on shoulders
- Runoff is infiltrating the granular material (recycled PCCP from runway rehabilitation)
- Vegetation struggling to establish
- Underdrain surface configuration allows for easy visual identification of the BMP and of the need for maintenance





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- ECB not installed over all disturbed areas
 - Vegetation minimal in unprotected areas
 - Reseeding implemented with limited success
 - Working with NRCS to evaluate potential causes
 - May improve with soil conditioning, use of ECBs, and temporary watering (which may or not be permissible within the WQ basin)





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Reinforced Shoulder & Channel







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– Maintenance Path









Underdrain Shoulder







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- The installations have shown that these alternatives can work
- Ongoing maintenance and observation will help to refine the designs for future installations
- Research into additional alternatives needs to continue to address the diverse issues and conditions at DIA

Future Efforts

- Alternative outlet structures
- Alternative WQ features
- Alternatives to outlet protection
- Alternatives for low-flow channels
- Additional alternatives for shoulder stabilization















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- Issues raised and being investigated
 - Roll over potential
 - Motorcycles
 - Aggregate thrown back on roadway
 - Vehicles getting stuck, high-centered, dips, etc.
 - Stability for changing tires
 - Potential for pull up or snagging
 - Inspections
 - Hazmat cleanup
 - Flammability

Questions?

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ST DENVER INTERNATIONAL AIRPORT

Tackling Erosion Caused by Roadway Deicing Agents—Project Results

> by Catherine Rafferty, PE—Denver International Airport Rich Ommert, PE—Moser & Associates Engineering Lee Rosen, EI—Moser & Associates Engineering September 23, 2010



Hui-Ming "Max" Shih PhD, PE, CFM URS Corp., Denver

James C.Y. Guo PhD, PE University of Colorado Denver



Bill Sabatka PE URS Corp., Denver

TOTAL SUSPENDED SEDIMENT REMOVAL RATE FOR WATER QUALITY PONDS

First Flush Runoff

 Event mean concentrations of the maximum pollutant are consistently observed to occur in response to the initial 12~15mm (0.5 inch) of effective rainfall-runoff with significantly lower runoff concentrations occurring thereafter (Ellis, 1991)

First Flash Video



Water Quality Volume (WQV)



(Verbanck et al., 1994)

 By capturing and treating the runoff volume of First Flush, up to 90% of pollutants that are washed off of the land can be removed from the

storm water.

Methods of Estimating WQV

- 90% of the average annual stormwater runoff volume.
- Half-Inch Rule (0.5 inch rainfall depth)
- EPA Simple Method (EPA, 1986)
- Water Quality Capture Volume (WQCV) (Guo and Urbonas, 1996)

Applied for determining Water Quality Volume

A Pond Design





Does WQV Trap Pollutants in Ponds?

- Quantity ? Quality?
- WQV contains the washed off sediment and associated pollutant.
- Do WQV ponds trap the sediment and associated pollutants?



Total Suspended Sediment (TSS)

 Suspended sediment is one of primary pollutants and transport agency attached by associated pollutants.



- Associated pollutant concentration is commonly proportional to TSS concentration.
- Easily sampled
- Indicator of water quality or water treatment efficiency.







TSS Removal Efficiency (%)



Engineers' Struggles for Water Quality Pond Design

- Anticipated TSS Removal Rate?
- Pond Performance for Best Management Practice (BMP)
- Receiving Leadership in Energy and Environmental Design (LEED) Credit
- Pond Maintenance and Sustainable Use






TSS Removal Rate Dominant Factors

Inflow Sediment

Drain Time

Temperature





Geometry



• Advection-diffusion equation $\frac{\partial C}{\partial t} + \frac{\partial q_{s-x}}{\partial x} + \frac{\partial q_{s-y}}{\partial x} + \frac{\partial q_{s-z}}{\partial z} = \frac{\dot{m}}{dxdydz}$

• Turbulent Flow $q_{s-x} = V_x C - (D + \varepsilon_x) \frac{\partial C}{\partial x}$

• Particle Settling Velocity

$$\omega_i = \frac{8\nu}{d_s} \left[\left(1 + 0.0139 d_*^3 \right)^{0.5} - 1 \right]$$

Non-ideal sediment settling

 $V_{c-non} = 1.2V_c$

• Water-Sediment Mixing Condition $C_{mixing} = \beta \cdot \alpha \cdot C_i$

Performance TSS Removal Rate Indictor



Calculation Sheet

$$T_E = 1 - \beta \cdot \alpha \cdot \sum_{i=1}^{n} \left[e^{-L\omega_i/1.2q} \cdot \Delta X_i \right]$$

$$\omega_i = \frac{8\nu}{d_s} \left[\left(1 + 0.0139 d_*^3 \right)^{0.5} - 1 \right]$$

$$d_* = d_s \left[\frac{(G-1)g}{v^2}\right]^{1/3}$$



EXTERNET THE PROVING RATE: TO TAL SUSPENDED SEDIMENT REMOVAL RATE CALCULATION FOR A WATER QUALITY POND Priori Streems Spectra Rain, Oritani Funt & Dark Rein Destanant. Date Martin Colorest Weter Durity (Santon Volume) (1020)24 10.0 61 M B Partnersed Paper Middates 100 HOCK Date Server bai, Hill Providiation File Path Langth Pitter Ukering Participie Video Rong: No. 3 Westman and Non-test in party -Partone Specific Oracle, Or WODY Resides Destroyers 110 UNE CONTRACTOR 1000 10.0 Intern Print Print Print 101.0 10.1 High Print Pauloum 8.81 Periode Class. Same No. 1-10-1 B Same. 200 786 155 Total TRA T-last 127 Restaural Role (No 36 Takes. The Theorem Per ta tración Carlonger 11 ac 144.40 Films Langer 10. Employee. Comparison in the Sectors' Sec. and 100 0.00 畿 No. of the local division of the local divis 6.0.1 1.00 1000 18 125 1.56 Sector 1 1,24 100 181 1.00 10.04 Visity Street 0.0 Sellin and 1000 Sector 1 11.0 1.25 1973 (B. 1994) 19.3 112 1.1 12 1000 攘 콚 March 199 橋 12. 10.0 1.27 100%) 100% 10.00 12 1.0 1.1 100 194 35 200 ing materi 100 100.00 Ora. 1.000.000 10.00 100 1.000 1,007 1.32 容 90,25 10. 16 inter State

Non. The setulation (Real rule design to estimate the total subpended institute) (730) removali at a trajectori party with a seture subfig registre or tome. (W-2015).

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Case Study – Orchard Detention, Denver, Colorado



- Extended Detention Basin
- catchment is 16.9 acres
- site imperviousness rate of 50%.
- (WQCV) of 0.41 acre-ft based on a 40-hour drain time





Inflow Particles – Native Topsoil





• Renohill Loam, containing 33.4% of sand, 33.3% of silt, and 33.3% of clay

TSS Removal Calculation

TOTAL SUSPENDED SEDIMENT REMOVAL RATE CALCULATION FOR A WATER QUALITY POND

Pre	ject]	Extended Detention	Basin, Orchard	Pond at Grant Ranch	Developmen	(
Descri	ption	Deriver, Colorado				
	Deter	08.01.2009				
Water Quality Ca	oture	Volume (WQCV)=	0.41	Ac-tt		
Permenant Pool Volume=			0	Acit		
	- W	QCV Drain Time*	40	hr		
	W	Q. Pond Surface=	12770	n ²		
	19	Now Path Lengths	126	n		
	- 51	ow Mixing Factors	1	Value Rang: 1-	1	
	100	ematic Viscosity*	1.00	*10 ⁴ m/isec at	20	
Pat	cle S	pecific Gravity, Ga	2.65	Control Control Control		
WQC	V Re	lease Discharge=	0.12	cts		
		Unit Discharge*	0.0012	cfs/ft		
		Mean Pond Width	101.3	ft.		- 21
		Wet Pond Factor=	1.00		1100	
Particle C	lass	inflow (%)	Outflow (%)	1 1	35 3	3
Grave		0	0	-	100	
Sand		33.4	0		1.15	- 100
Silt		33.3	0	Total TSS	1 Carlos	
Clay		33.3	19	Removal Rate (%)	200	
	otal	100	19	81		1





Estimated TSS Removal Rate



Drain Time v.s. TSS Removal %

Orchard Pond (WQCV=0.41 ac-ft)



Wet Pond Enhancement





Conclusions

- Total Suspended Sediment (TSS) Removal Rate does not only depend on the pond type and drain time.
- Anticipated TSS removal rate could be estimated by considering inflow sediment, pond geometry, water-sediment mixing condition, drain time, and wet pond enhancement.
- This study provides a theoretical approach and an indictor tool for estimating TSS removal %.



THANKS.....





Further Questions & Requests.... Feel free to contact Max Shih by (720)262-6600; max_shih@urscorp.com

EAGLE RIVER RESTORATION PROJECT "Edwards Reach"



Julie E. Ash, P.E. & Susan Nordstrom, RLA Walsh Environmental Scientists & Engineers, LLC

> 21st ANNUAL CASFM CONFERENCE Snowmass Village, Colorado September 23, 2010

SELECTED PROJECT HIGHLIGHTS

>Project overview >Site orientation Pre-existing conditions >Goals >Approach **>Treatments** Construction sediment control > Performance **>Future**



PROJECT OVERVIEW PROJECT OWNER: Eagle River Watershed Council **PHASE 1 PROJECT PARTNER: Eagle River Water & Sanitation District** PHASE 1 (2008) EXTENTS: Length = 0.9 miles Approx. 55% of Area = 40 acres total <u>1.6 miles</u> **PHASE 1 COST:** Instream = \$1.4M Planting = \$0.3MConstruction Total = \$1.7M

PROJECT OVERVIEW

MULTI-PHASE PROJECT OUTCOMES:

- **Restored riparian corridor = 80 acres**
- > 30 ac aquatic habitat
- > 50 ac terrestrial habitat

Restored river corridor = 1.6 miles
Reconnects 50 continuous miles of high-quality riparian & aquatic habitat



Additional info in CPWJ, Vol.5, Issue 8 - 2009

PROJECT OVERVIEW - FUNDING

Eagle Mine Natural Resource Damage Recovery Fund (NRDF)

For the restoration of natural resources damaged or lost as a result of the operations of the Eagle Mine within the Eagle River basin, \$2.4M awarded in January 2007, 2nd distribution

- Eagle River Water & Sanitation District (ERWSD)
- > Eagle County (ECO)
- Western Eagle County Metro. Recreation District (WECMRD)
- Edwards Metropolitan District (Metro)
- Colorado Water Conservation District (CWCB)
 - Healthy Rivers Fund, Watershed Restoration Program
- EPA Section 319 Grant (EPA 319)
- Colorado Department of Transportation (CDOT)

PROJECT OVERVIEW - FUNDING

FUND	PROJECT COMPONENT	VALUE	TERM	
NRDF	Instream & riparian, Phase 1	\$1.44M	One-time	
ERWSD	Instream & mixing zone, Phase 1	\$450K+	Potential future	
ECO	Instream & riparian Multiple Phase	\$75K, \$50K	Potential future	
WECMRD	Recreation along river corridor	\$50K+	Potential future	
Metro	Recreation along river corridor	\$40K+	Potential future	
CWCB	Maintenance & Monitoring Multiple Phase	\$50K, \$35K+	3-year grants	
EPA 319	Instream & riparian, Phase 2	\$600K	3-year grant	
CDOT	Phase 2	\$10K	Potential future	

SITE ORIENTATION

1/2 mile downstream of Edwards Spur Road Bridge to Hillcrest Drive Bridge 1.6 mile project reach, 80 acre project area, unique characteristics



SITE ORIENTATION : PHASE 1 – REACHES 1 & 2



SITE ORIENTATION: PHASE 2 & 3 – REACH 4



SITE ORIENTATION: PHASE 1 & 2 – REACH 5



Frequency-Discharge Data

Discharge (cfs)							
Upstream of Lake Creek	Downstream of Lake Creek						
105	120						
1990	2060						
2430	2730						
3980	4530						
5430	6170						
	Upstream of Lake Creek 105 1990 2430 3980 5430						

"One of the most severely degraded reaches in the valley" -Eagle River Inventory & Assessment (CSU, 2005)

Degraded instream conditions & riparian corridor

Overly wide & shallow channel
High instream temps
Low dissolved oxygen levels
Deposition of fines
Tubifex worm habitat

ORIENT.

OVFRVIFW

EX.COND.

GOALS

APPROACH

SED

PERFORM.

FUTURE

Degraded instream conditions & riparian corridor

Localized bank erosionPoor aquatic habitat



Degraded instream conditions & riparian corridor

Lack of riparian canopyLack of shrub component





Land Use History >Grazing, historical to present > Railroad Roads and highways > Offsite development >Hillcrest bridge > Treatment plant





To improve the habitat and function of the Eagle River through the Edwards Reach

Surface Water Quality
Sediment Control
Stream Health and Function
Aquatic Habitat
Riparian and Wildlife Habitat
Land Use Management



Surface Water Quality
 Reduce instream temps
 Raise DO levels

 Sediment Control
 Reduce fine sediment supply
 Improve mobility at lower flows





Stream Health and Function Correct overly wide, shallow condition Restore low flow sinuosity

Active Habitat Increase cover & flow diversity Reduce tubifex worm habitat



FUTURE



EX.COND.

ORIENT.

OVERVIEW

GOALS

APPROACH

TMTS

SED



PERFORM.

Riparian and Wildlife Habitat Restore overhead canopy to reconnect riparian corridor Increase shrub layer Increase species diversity Land Use Management Cattle exclusion fencing Controlled recreational access Educational signage Strategic plantings

RESTORATION APPROACH

Watershed level
 Maximize natural form and function
 Habitat focused
 First rule of ecological restoration



"To protect your rivers, protect your mountains" -Emperor Yu of China (1600 B.C.)

"How would Mother Nature do it"

RESTORATION APPROACH Don't do more harm than good > tread most lightly > protect downstream fisheries Exceeded construction impact standards Construction sediment control BMPs • 2 Structural • 2 Non-Structural Bio-oil in excavators > Carefully aligned access routes > Coordination with fly fishing community > No weekend work in channel through Oct. 14th





RESTORATION TREATMENTS - INSTREAM



BEFORE



AFTER

Recreate cobble/gravel point bars
Alternating alignment
Boulder framework
Natural substrate

PERFORM.

FUTURE

Bar 1-22 in Reach 1

OVERVIEW ORIENT. EX.COND. GOALS APPROACH TMTS SED

RESTORATION TREATMENTS - INSTREAM



BEFORE



Recreate cobble/gravel point bars
Boulder framework
Reconnect remnant depositional areas



Bar 1-4 in Reach 5

AFTER

OVERVIEW ORIENT. EX.COND. GOALS APPROACH

SED F




BEFORE



Enhance channel bars
Boulder framework
Reduce split flow
Concentrate low flows

FUTURE

Bar 1-5 in Reach 5

AFTER



BEFORE



AFTER

Enhance channel bars
Boulder framework
Shape and stabilize confluence with side channel

Bar 1-1 in Reach 5



BEFORE



Plug gap between existing channel bars
Concentrate low flows in main stem
Boulder/Cobble Plug
Integrate habitat logs

Treatment 1-6 in Reach 5

AFTER



BEFORE



Restore boulder/cobble toe
Natural groupings
Integrate habitat logs, spurs, and habitat boulders



Treatment 1-16 in Reach 2

AFTER









PLANTING APPROACH



Structure
Function
Plant associations
Density



RESTORATION TREATMENTS - VEGETATIVE



BEFORE

OVERVIEW



Plant Groups/Bank Treatments

Continuous Willow Bank Treatment

- Bebb's willow
- Whiplash willow
- Planeleaf willow

Tall Willow Group

- Rocky Mountain willow
- Whiplash Willow
- Planeleaf Willow
- Thinleaf alder

ORIENT. EX.COND. GOALS

APPROACH

PERFORM.

FUTURE

SED

TMTS

RESTORATION TREATMENTS - VEGETATIVE Plant Groups/Bank Treatments Narrowleaf Cottonwood Group Narrowleaf cottonwood **Blue spruce** Thinleaf alder Red-twig dogwood Prickly currant Golden currant Shrub Bank Treatment Woods rose Golden currant Prickly currant Twinberry honeysuckle Thinleaf alder

River hawthorn

OVERVIEW ORIENT. EX.COND. GOALS APPROACH TMTS SED

PERFORM. FUTURE

RESTORATION TREATMENTS - VEGETATIVE



BEFORE



AFTER

Plant Groups/Bank Treatments

Mixed Shrub Group

- > Red-twig dogwood
- > Wood's rose
- Golden currant
- Prickly currant
- Twinberry honeysuckle
- Mountain snowberry
- Shrubby cinquefoil
- Thinleaf alder
- River hawthorn
- Rocky Mountain Willow

Tall Willow Group Narrowleaf Cottonwood Group

OVERVIEW ORIENT. EX.COND. GOALS APPROACH

ROACH TMTS

PERFORM.

FUTURE

SED

> 2 Structural BMPs

- Aqua Dam
- Floating Silt Curtain
- > 2 Non-Structural BMPs
 No equipment tracking in channel



Spawning monitoring by fly fishing guides

\$180K for Phase 1 voluntary sediment controls
 10% of \$1.7M Phase 1 construction budget

BUND ST





www.geomembranes.com www.aquadam.com

Water-Controlling Water





Water-filled AQUA DAM combines weight and counter friction creating an effective, stable water control barrier.







www.geomembranes.com www.aquadam.com

> \$140K for Phase 1, 8% of construction Less for future phases





Another reason to consider the Aqua Dam...





Active work area

No work within Dam... not our impact!

Floating silt curtains

Stationary at downstream endMobile curtains at work areas





Floating silt curtains

\$40K for Phase 1, 2% of construction
 Reconsider for future phases





PHASE 1 PROJECT PERFORMANCE Instream features installed Nov.2008 > Bars and plug intact after 2009 peak flows Bars and plug concentrating low flows > Minor repair on 1 cobble toe bank treatment > Willow cutting installation in 2010 **Plantings installed Sep.2009** > Wire caging, future sand painting Minor beaver predation during installation > Intensive maintenance program > Awaiting first full growing season

FUTURE Phase 2 in Fall 2010

PROJECT PARTNERS: >EPA 319 Award, CDPHE >Eagle County >CWCB >CDOT **COMPLETE REACH 5 START REACH 4**



Phase 3 in Fall 2011 **EVAPORITE SINKHOLE IN LOWER REACH 4**

GOALS

APPROACH

TMTS

SED

EX.COND.

ORIENT.

OVERVIEW

PERFORM. FUTURE

CONTACT INFORMATION

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Eagle River Watershed Council

Avon, Colorado http://www.walshenv.com

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Genesis of Regional Hydraulic Geometry Relationships for the Fountain Creek Watershed, CO

Graham Thompson, PE



September 23, 2010

Vicinity Map

- Fountain Creek Watershed
- 930 square miles
- 10,000 ft of relief





Flooding







Hydraulic Geometry Concepts

- Plots comparing dependent channel variables
 Width
 - Depth
 - Cross-sectional Area
- To an independent variable
 - Drainage Area
 - Discharge

Hydraulic Geometry Premise

- Channels develop in measurable, reproducible forms
- Function of their formative factors
 - Climate
 - Hydrology – Sediment load
 - Vegetation
 - Bed material
 - Others





Longitudinal View Profile



Lane's Sediment Balance



Hydrophysiographic Regions



Fenneman, Nevin M., 1946, *Physical Divisions of the United States:* U.S. Geological Survey http://wmc.ar.nrcs.usda.gov/technical/hhswr/geomorphic/index.html "The concept of channel-forming or dominant discharge is now a cornerstone of river channel restoration design"

[Channel-Forming Discharge Selection in River Restoration Journal of Hydraulic Engineering Volume 133, Issue 7, pp. 831-837 July 2007]

Channel-Forming Flow

- Representative flow that is responsible for shaping the natural channel over time
- 3 methods
 - Bankfull discharge (field morphology)
 - Specified recurrence interval (flow statistics)
 - Effective discharge (mathematical)
- Methods should all agree??





- The maximum discharge that the channel can convey without overflowing onto the floodplain.
- Represents the breakpoint between the processes of channel formation and floodplain formation.

Specified Recurrence Interval

- Range of 1- to 3-year flood
- 1.5-year flood on average
- This flow occurs 1 to 2 times each year









"If you don't know bankfull, you don't know S**T!"

- Dave Rosgen



Data collection efforts

- Summary of field survey
- Bankfull field indicators
- Other data sources and references









Fountain Creek @ Fountain














								and the second second
Gage Station	DA (mi ²)	Q (cfs)	A (ft ²)	W (ft)	D (ft)	W/d Ratio	Rosgen Stream Type	Return Interval
Monument Creek @Northgate	82	73	18	18	1.1	16.6	C4	1.33
Fountain Ck @Colorado Springs	392	2,130	256	61	4.2	14.4	C4	1.25
Fountain Ck @Fountain	681	3,100	478	209	2.3	91	C4	1.25
Fountain Creek @Pueblo	926	2,990	309	159	1.9	81.5	C4	1.43
Jimmy Camp Creek at Fountain	66	229	45	29	1.5	18.8	C4	1.42
Cottonwood Creek @Woodmen	10	180	28	27	1.0	25.2	F4	1.19



Regression Results

- Function of drainage area
- Log-log plots
- Power function
- Data correlation











- 1999 flood flow was approx. 20,000 cfs
- Bankfull discharge is approx. 2,000 cfs
- Bankfull agrees with recurrence interval
 - 1.25 years
- Effective discharge is approx. 200 cfs
- Baseflow?



"The concept of channel-forming or dominant discharge is now a cornerstone of river channel restoration design"

(Channel-Forming Discharge Selection in River Restoration Journal of Hydraulic Engineering Volume 133, Issue 7, pp. 831-837 July 2007)



- design and planning tool for stream restoration
- stability assessment
- road crossings
- hydrology model calibration

Bankfull Flow vs. 2-year Flood





Short comingsFuture data needs

THANK YOU!

Contact Information

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FLOODPLAIN ENCROACHMENT THIS IS WHY WE HAVE A JOB!

- What did Denver look like prior to development?
- Should there be criteria for 100-year capacity for all drainageways?
- How does floodplain management factor into land use decisions?
- What about safety and flood hazard reduction?



FLOODPLAIN **ENCROACHMENT** THIS IS WHY WE HAVE A JOB! Where can we put drainageways underground? ■ Which pipes need 100-year capacity? □ It is cost effective to pipe the 100-year event?



Case Studies

Montclair outfall Park Hill outfall West Speer outfall (Tucker Creek) Westerly Creek Harvard Gulch

Denver Today



Geologic Overlay



New Streams



Montclair and Park Hill Outfalls



West Speer Outfall



Westerly Creek



Westerly Creek



Westerly Creek

In 1980, a 10-year pipe was constructed to reduce frequent flooding

In 1991, Westerly Creek Dam was constructed

What is the incentive to reduce the floodplain?

- Should the 10-year system be replaced with an open channel?
- Are there other benefits to an open channel, and are these considered in a Benefit/Cost analysis?

Harvard Gulch at Logan Street



















Harvard Gulch



Harvard Gulch Floodplain





Harvard Gulch – Open Channel




Water-Data Report 2008

06711575 HARVARD GULCH AT HARVARD PARK AT DENVER, CO

South Platte Basin Upper South Platte Subbasin

LOCATION (REVISED).--Lat 39°40'18.20", long 104°58'37.30" referenced to North American Datum of 1983, in NW ¼ SW ¼ sec 26, T.4 S., R.68 W., D County, CO, Hydrologic Unit 10190002, on right bank 125 ft north of East Harvard Avenue, 300 ft west of South Ogden Street, and directly north of Porter Memorial Hospital, in Denver.

DRAINAGE AREA -- Not determined.

SURFACE-WATER RECORDS

PERIOD OF RECORD.--August 1979 to current year (annual seasonal-maximum only).

GAGE.--Nonrecording gage and crest-stage gage. Elevation of gage is 5,320 ft above NGVD of 1929, from topographic map. Supplementary water-sta recorder used for storm events.

REMARKS -- Gage operated seasonally, April through September.

EXTREMES FOR PERIOD OF RECORD (REVISED).--(seasonal only) Maximum discharge, 2,120 ft³/s, July 8, 2001, gage height, 17.44 ft, from rating curv extended above 95 ft³/s on basis of slope-area measurements at gage heights 14.88 ft and 15.62 ft, and flow-over-weir measurement of right ov bank flow at the peak. The water year 2001 maximum discharge was previously published as "not determined".

≊USGS

USGS 06711575 HARVARD GULCH AT HARVARD PARK AT DENVER, CO



Harvard Gulch...July 8, 2001

66

Rocky

93



NELD

ADAMS

Allens

119

GILPIN

- High water survey stakes

Harvard Gulch...July 8, 2001







Harvard Gulch Outfall



Harvard Gulch Outfall

- Should Denver spend \$20 million to increase the capacity of the existing outfall that has not failed?
- What incentive is there to provide flood control?
- How is such a project justified?
- How much confidence do we have in the hydrology from 1965?
- Do we have an obligation to reduce flood hazards?

Recommendations

 Criteria should require 100-year capacity for "major drainageways"

Benefit/cost analyses will usually not support 100-year design projects

Flood hazard reduction, community redevelopment, open space corridors, trails and wildlife habitat benefit from 100-year outfalls

If major outfalls had 100-year capacity, would we be out of a job?

CERTIFICATION OF THE TEMPLETON GAP LEVEE IN COLORADO SPRINGS, CO

Mark K. Kempton, P.E., C.F.M. Anderson Consulting Engineers, Inc. Fort Collins, CO



Anderson Consulting Engineers, Inc.

vil • Water Resources • Environmental

Acknowledgements

- Dan Bare, City of Colorado Springs, City Engineering/Stormwater Division
- Thuy Patton, Colorado Water Conservation Board
- Dawn Gladwell, FEMA Region VIII
- Chris Pauley, Anderson Consulting Engineers, Inc.
- Dave Jula, Baker FEMA PTS Contractor
- Lymann Henn, Inc., Denver Geotechnical Consultants

Templeton Gap – Vicinity Map



History of the Floodway

- Templeton Gap Wash prior to 1952
- Templeton Gap Wash floods occurred in 1855, 1886, 1922, 1929, 1932 and 1935
- Templeton Gap Wash was a tributary to Shooks Run, which flows through downtown Colorado Springs south to Fountain Creek
- Army Corps of Engineers re-routed the Wash westward to Monument Creek to alleviate flooding
- Floodway channel and levee constructed between 1948 and 1952 by the U.S. Army Corps of Engineers



History of the Floodway

- Colorado Springs took ownership of the levee in 1952
- Levee is in the Corps Inspection of Completed Works (ICW) program
- Inspected every 2 years by the Corps
- Levee has had maintenance issues over the years
- Sedimentation, trees, shrubs growing on the levee
- Several property encroachments on the levee right-of-way over the last 60 years



Historic T. Gap Wash Alignment



Hydrology

- Maximum estimated discharge = approx. 9,700 cfs in 1932
- Maximum 1-day precipitation = 4.3" in September 2008
- 8.5 square mile drainage basin
- Fully developed (with no detention) between 1965 and 1975
- 10-year discharge = 6,490 cfs
- Levee design Q₁₀₀ in 1949 = 14,000 cfs
- New HEC-HMS hydrologic study Q₁₀₀ = 13,490 cfs



T. Gap Drainage Basin – 8.5 mi²



How Are Levees Evaluated?

- Prior to 1980, no evaluation was required for FEMA maps
- After 1986, all levees required to conform to Section 65.10 of the National Flood Insurance Program (NFIP) regulations
- City of Colorado Springs owns and maintains the Templeton Gap Levee



El Paso County DFIRM

- Levee has to be re-certified for the El Paso County DFIRM project
- Levee needs to meet requirements of Section 65.10 of the Code of Federal Regulations (CFR)
- Levee currently shown as providing flood protection on El Paso County FIRM panel
- Effective floodplain mapped in 1982







What Does Section 65.10 Require?

A levee must meet the following criteria before being certified or re-certified and shown on a DFIRM.

- Minimum 3 to 4 feet of **freeboard** above the 100year event
- Structural design of all closures, embankment protection, embankment and foundation stability, seepage and settlement analyses
- Analysis of interior drainage including storage areas and gravity outlets
- A documented and executed **O&M plan**

Section 65.10 (Continued)

- Levee should be owned, operated and maintained by a Federal or State created entity.
- The requirements of 65.10 may be waived if certification of the levee system can be provided by another **Federal** agency responsible for flood control activities, such as the U.S. Army Corps of Engineers.

Requirements for Levee-Re-Certification

- Hydrologic and hydraulic analyses to show 3 to 4 feet of freeboard along the levee in the 100-year event
- Boreholes along specific reaches or all of the levee to perform seepage and stability analyses
- Preparation of an O&M Plan that describes regular maintenance and the operation of any closure devices

Templeton Gap Levee, Colorado Springs, CO-Certification Issues

- Inadequate freeboard due to sedimentation sediment is 3 to 4 feet deep in some areas
- Levee overtops some sections during 100-year event
- Several utilities crossing the channel under the levee cable TV, 2 sanitary sewer lines, 3 water lines, gas line
- Utilities installed deep in relation to existing invert too shallow in relation to original channel invert
- Coordinate with utility owners to relocate/lower utilities

Templeton Gap Levee, Colorado Springs, CO-Certification Issues

- Several encroachments on Levee ROW
- Previous lawsuits regarding ROW along levee





Levee Certification Issues

- Part of levee built over inactive coal mine – possible subsidence
- Failing rock drop structure needs to be replaced – too close to levee and bend in



channel







Geotechnical/Mine Investigations

Drilling along the Levee Drainageway and Slope base. West of Union Boulevard





Drilling, Casing, and Grouting above the Levee East of Union Boulevard





Video camera and sonar void imaging tools



Borehole BH-5RV: Void mapping between 100 and 103 ft bgs



s v Levee xado	BLACKHAWK	Lyman Henn, Incorporated Deriver, Colorado			Sonar and Video Camera Data Acquisition Templeton Gap Floodway Levee Colorado Springs, Colorado		
Figure: 5-1	No Conversion Real Process (2012) 2014/2015 Same R. Converse Market Proc. (2012) 2014/2015 Same R. Converse Market Proc. (2012) 2014/2015	Project No: 5155	Dele February, 2010	Drawn By HJV	Checked By KH	Scale: As Shown	Figure 5-4

Video Camera and Sonar Images

Void 7 ft high @ depth between 99-106



ft bgs Images @ ~ 101 ft bgs



Levee Certification Issues

- Union Blvd. culvert crossing built in 1980 – invert 3 feet above original channel invert
- Multiple trees growing in levee – City removed trees in 2009 - root systems to be removed as part of improvement project





Levee Certification Issues

- Replacement of Hancock Road Bridge
- Coordinating bridge design with levee design to satisfy local floodplain and Section 65.10 criteria



Hydraulics and Floodplain Mapping

- Prepared new HEC-RAS "with-levee" hydraulic model of floodway from Austin Bluffs Parkway to Monument Creek
- Prepared 2-dimensional FLO-2D "without-levee" model of areas protected by the levee
- Even distribution of 100-year discharge along 3 separate levee sections
- Mapping and combining 3 separate without-levee floodplains
- Estimate that 2.9 square miles of residential/commercial areas are protected from lower return period events

Potential Floodplain for Without-Levee

2-D Analysis



Structures Affected by Without-Levee Floodplain

Zone AE 100-year Floodplain

- 2,000 to 3,000 Residential structures*
- 200 to 300 Commercial structures*

Zone X Floodplain (less than 1-foot depth)

- 2,000 to 3,000 Residential structures*
- 50 to 150 Commercial structures*

* <u>Preliminary Estimates</u>

Templeton Gap Levee – Steps to Certification

ACE has performed the following services to certify the levee to FEMA

- Investigation of the existing hydraulic and geotechnical properties of the levee system
- Developed alternatives to mitigate lack of freeboard, utility crossing issues, and sedimentation issues
- Preparing construction plans and specifications to
 - dredge the channel ;
 - raise the levee;
 - repair drop structures; and
 - move sediment through the levee system.

Templeton Gap Levee – Steps to Certification

- Possible mitigation of potential mine subsidence by filling mines with a grout/cellular foam mixture – still under investigation
- Prepare a CLOMR to have FEMA approve the rehabilitation methodology
- 404 permit application
- Floodplain use permit
- Army Corps approval of design
- When construction is complete prepare a LOMR to certify the levee as providing 100-year flood protection

Future of the Levee Certification

Project

- Public passed ballot Issue 300 in November 2009
- City eliminated Stormwater Enterprise fees in December 2009
- Remaining Enterprise funds not sufficient to construct the project
- Without adequate funding levee will be de-certified on the El Paso DFIRM
- Residential stormwater fees = approx. \$4 per month
- Flood Insurance = approx. \$125 per month
- "You're saving yourself a few bucks a year," City Councilor Scott Hente said last fall, "to incur the luxury of spending \$1,000 a year on flood insurance."¹

¹Colorado Springs Independent website

Future of the Levee Certification Project

- City still looking into alternatives to fund the levee improvements
- Flood insurance for all affected properties is estimated to be \$3 million <u>per year</u>
- <u>One time cost</u> to rehabilitate levee and mitigate mine subsidence = approximately \$4.2 million
- B/C ratio over 50 years = ???
City Outreach Efforts

\$4.2 million cost of improvements

 Unknown when or if the levee/mine improvements will be made

Attention Property Owners You may need to purchase flood insurance!

The Federal Emergency Management Agency (FEMA) is in the process of updating floodplain maps. The Templeton Gap Floodway (a levee) does not meet the latest FEMA requirements, which means it will not be certified when FEMA releases its preliminary maps (anticipated release Oct 2011).

The City of Colorado Springs does not have a funding source for the \$4.2 million in upgrades needed to meet FEMA certification requirements.

If you hold a mortgage on a property listed in the floodplain, you will likely be required by your lender to purchase flood insurance. FEMA will determine the official boundaries of the floodplain, but the City's analysis shows it will likely extend well south of the levee into adjacent neighborhoods. (see map)



By purchasing flood insurance before the Templeton Gap area is declared an official floodplain, you may be able to take advantage of a "grandfather clause" that could reduce your premiums. Information is available at wrow floodsmart.evv/floodsmart. For more information about the levee, visit www.springsgov.com and type "Templeton Gap Floodway" in the search field.

> INFORMATIONAL MEETING DATE PLACE TIME

This flyer was put together by the City of Colorado Springs at the request of the Council of Neighborhoods and Organizations (CONO) for informational purposes. Questions regarding insurance and mapping should be directed to the FEMA contact, Thuy Putton, at (303) 866-3441 or they puttonillulate.co.us.

DFIRM Requirements For Mapping The Effects Of Levees

OT	EMA				Contact Us	AZ Index Frequently	Asked Questions Español
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Home	About	FEMA	Disaster Information	Plan & Prepare	Recover & Rebuild	Apply for Assistance	FEMA for You
National Flood I Program	nsurance	Avea System Information for Stakeholders			Contacts Megoing Contacts		
Flood Insurance	Flood Insurance		Introduction				References USACE Levee Guidance Documents
Floodplain Management Flood Hazard Mapping User Groups		<u>Map Modernization and Levee Systems</u> <u>Levee System Construction and Restoration Projects</u> <u>Interagency Levee Policy Committees</u> <u>Find Information for Stakeholder Groups</u> <u>For More Information</u>					EEMA Procedure Memorandums and Attachments EEMA Regional Flood Hazard Mapping Contacts
Risk MAP Cooperating Partners Status of Ma	Technical ap Change	The United States has thousands of miles of levee systems—usually earthen embankments designed and constructed in accordance with sound engineering practices to contain, control, or divert the flow of water to provide some level of protection from flooding. Some levee systems date back as far as 150 years; some levee systems were completed recently or are underway. Some levee systems were built for agricultural purposes, and they provide flood protection and flood-loss reduction primarily for farm fields and other land			Online Tools FEMA Photo Library FEMA Mapping Information Platform FEMA Library		
Requests Forms, Documents and Software Online Tutorials FAQs		and flood-loss reduction for population centers and the industrial, commercial, and residential facilities within them. Levee systems are designed to provide a specific level of flood protection. Agricultural levee systems provide a level of protection that is appropriate based on the value of the assets being protected. Urban levee systems, because they are designed to protect urban areas, have typically been built to higher				Related Topics What's New in Flood Hazard Mapping Mutit-Hazard Mitigation Planning Pre-Disaster Mitigation	
		standards. No levee system provides full protection from all flooding events to the people and struct it. Thus, some level of flood risk exists in these levee-impacted areas.			ctures located behind	Government Links FloodSmart National Committee on Levee	

http://www.fema.gov/plan/prevent/fhm/lv_intro.shtm

Colorado Springs Templeton Gap Floodway Fact Sheet

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Templeton Gap Floodway Project

Templeton Gap Floodway Fact Sheet

Did you know that the Templeton Gap Floodway is more than just a drainage channel? It's artually a levee - the only levee in Colorado Springs. It starts just east of Union Boulevard and heads weat to Nevada Avenue, eventually leading to Honument Crock (see attached map below).

A lower is an embankment constructed to contain flued flows. Levers are meet often seen along the banks of a river to keep it from everflowing, but is the case of the Templeton Gap Floodway leven, it was built to divert flow from one drainageway to another.

Previously, water from the Templeton Gap area traveled down Sheoka Run to Fountain Greak downstream of downtown Colorado Springe. A series of floods in the late 1800s and early 1900s caused significant damage and serveral dealths along this route and realed concerns about future flooding. Responding to community concerns, the U.S. Army Corps of Engineers built the Templeton Gap Floodmay in 1949 to divert runoff away from downteam by sarrying it west to Honorman Creak.

The Templeton Gap Floodway is approximately 2 miles long and must carry an estimated 100-year flood flow of 13,500 cubic feet per second. It provides flood protection to over 3,000 properties and 5,000 structures.

The City of Colorade Springs owns the floodway and is responsible for its maintenance which has to meet certain standards under the Corps of Engineers Inspection of Completed Works program. These include items such as mowing and true removal, including the roots which can damage the integrity of the levee, concrete repairs and filing of animal berrows. The levee has received a "marginally acceptable" rating primarily due to excess weptation, especially root balls that must be removed. The City has been active in addressing these maintenance issues and is continuing this effort to achieve the required "satisfactory" rating.

After the disastrous failure of levees in the aftermath of Hurricane Katrina in 2005, more attention is being paid to levees and the Federal Emergency Hanagement Agency (FERA) has ramped up its efferts. Part of this effort will significantly impact the status of the Templeton Gap Floodway levee as FERA is completing what is called the Map Modernization Program.

As part of PEHA's Hap Hodernication Program floodplain maps are being converted to a sligital format for distribution on the Web and all flood production levens in the country are required to be certified. Without certification, owners of properties downstream of the leves could be required by their lenders to pay for flood insurance and, if a flood were to damage the leves, the City of Colerado Springs would not be eligible for federal function for repuirs. Without certification annual insurance premiums could collectively cost property owners approximately 53 million per year.

http://www.springsgov.com/page.aspx?navid=2743

Templeton Gap Levee Certification

Question or Comments?





Anderson Consulting Engineers, Inc.

vil • Water Resources • Environmental

Abstract

The Templeton Gap Levee was constructed in Colorado Springs, CO in 1950 by the U.S. Army Corps of Engineers as part of the Templeton Gap Flood Control Project (TGFCP). The levee and the associated canal-like channel were constructed to alleviate flooding on the Templeton Gap Wash which originates in the Austin Bluffs section of Colorado Springs. Runoff that is intercepted by the TGFCP historically flowed to the southwest to its confluence with Shooks Run, near the area of present day downtown Colorado Springs. Flooding from the Templeton Gap Wash caused severe flooding in the downtown Colorado Springs area in 1855, 1886, 1922, 1929, and 1932. The TGFCP rerouted the historic Templeton Gap Wash to its current left bank confluence with Monument Creek approximately 6 miles upstream of the Shooks Run confluence with Fountain Creek.

To meet the levee certification requirements of the El Paso County DFIRM project, the City of Colorado Springs selected Anderson Consulting Engineers, Inc. (ACE) to assess the condition of the existing levee, and to provide the necessary documentation to improve the levee and subsequently have the levee accredited to be shown on the El Paso County DFIRM as providing 100-year flood protection.

This presentation will highlight the procedures that ACE followed to assess the existing condition of the levee system, outline the alternative evaluations performed by ACE to mitigate the various deficiencies of the levee system, and also highlight the unique challenges associated with the certification of this particular levee system. The presentation will also outline the hydraulic analyses and floodplain mapping efforts associated with the Templeton Gap Floodway channel, and the without-levee floodplain mapping required by FEMA as part of the DFIRM process.

The presentation will highlight the following;

- •Freeboard for the 100-year flood event;
- •Sedimentation issues within the channel;
- Road crossing issues;
- •Utility crossings through the channel and the levee;
- •Potential mine subsidence in the area of the levee;
- •1- and 2-dimensional hydraulic modeling and floodplain mapping;
- •Levee certification and the DFIRM timeline;
- •Potential de-certification of the levee on the DFIRM; and
- •Flood insurance impacts to the approximately 5,000 structures protected by the levee.

Author Information; Mark K. Kempton, P.E., CFM Anderson Consulting Engineers, Inc. 375 East Horsetooth Road, Building 5 Fort Collins, CO 80525 (970) 226-0120 mkkempton@acewater.com



2010 CASFM Conference

Snow Mass, CO September 21-24, 2010

REACHING THE MASSES FOR STORMWATER QUALITY

A presentation on the

ONE THING IS CLEAR PUBLIC OUTREACH CAMPAIGN

Douglas County, Colorado J. DAVID VAN DELLEN, Town of Castle Rock WARD MAHANKE, City of Lone Tree



Who is One Thing Is CLEAR?

>CLEAR is the expanded communication and information vision of the Douglas County Stormwater Co-op Group made up of the following members:

Castle Pines Metro District Castle Pines North Metro District Cherry Creek Steward Partners City of Lone Tree City of Castle Pines North

Douglas County Douglas County School District Heritage Hills Metro District Highlands Ranch Metro District Lincoln Park Metro District Southeast Metro SW Authority SPLASH Stonegate Village Metro District Town of Castle Rock Town of Parker



What is One Thing Is CLEAR?

>CLEAR is a public outreach campaign promoted through:

>Local newspaper advertisements

>OneThingIsClear.org website

>Promotional materials and give-a-ways

>CLEAR stands for <u>Cooperative for Local Environmental Awareness & Responsibility</u>.



C is for Cooperative

The Co-op is an unfunded volunteer partnership made up of local agencies in and around Douglas County

>Primarily Phase II MS4 permit holders

>Shares resources and ideas related to MS4 Permit

>CLEAR is a product of the co-op that:

>Reduced public outreach costs to individual members

>Created a unified voice to the public

>Developed almost entirely using in-house staff and resources



L is for Local

- >CLEAR targets local audiences through the community newspaper
- CLEAR uses real photos within Douglas County to keep the message close to home
- >CLEAR targets local pollutant issues within our watersheds
 - >Sediment from construction sites
 - >Nutrients such as phosphorus and nitrogen
 - >Nonpoint source pollutants common to urbanized areas



EA is for Environmental Awareness

- >CLEAR believes that behavior change can happen when people are presented with a frequent, consistent and simple message of awareness.
- >We promote public understanding of stormwater quality issues by:
 - >Highlighting common behaviors that impact water quality
 - >Explaining the direct connection of urban areas to our waterways
 - >Simplifying the message into common language
 - >Sending the same message using several difference media sources



R is for Responsibility

- >CLEAR promotes and understands that our waterways are dependent on people choosing to do the right thing in protecting water quality.
- >We promote active protection of stormwater quality by:
 - >Providing practical recommendations to homeowners and businesses
 - >Providing a way to report spills and get involved at a local level
 - >Focusing on choices down to the smallest cigarette butt



Newspaper Advertisements

>Our Newspaper ads are the primary means of reaching the public on a regular basis

- >Ads run in nine local Colorado Community Newspapers
- Covering Douglas County and portions of five surrounding Counties
- >With a circulation of over <u>90,500</u> homes or <u>226,300</u> readers
- >Ads have a new message each month fitting to that time of year



Evolution of Advertising Campaign

>Co-op partners with Colorado Community Newspapers to begin monthly ads in 2007

>Ads unify the message across Douglas County but there is no common link to point to.

>Co-op develops DCStormwater.org to link ads to a common website in 2008

>Website provides central location for County-wide initiatives but there is still no name for the campaign

>Co-op develops One Thing Is CLEAR branding and changes website in 2010

>CLEAR captures the link and vision for all outreach initiatives



Ad prior to CLEAR

It's not good for our water ... either.

Whenever you are outside and you notice a piece of trash, please stop and dispose of it properly. Your rivers, creeks and lakes depend on you. What isn't collected today is picked up in the next rainstorm and sent directly to the nearest creek. From the moment this small piece of trash enters our waterways, it is responsible for a tremendous amount of damage.

Local stormwater agencies, including participants of the Douglas County Stormwater Co-op Group, SPLASH and SEMSWA, are tearning together to bring you this message. We take this so seriously that we posted this ad rather than send you more garbage in the mail. Together, with your help, we can make a difference in keeping our waterways clean. Look for this ad in corning months for more ways you can get involved.

THIS MESSAGE BROUGHT TO YOU BY

Castle Pines Metropolitan District 303.688.8330	Douglas County 303.663.6181 www.douglas.co.us/publicworks/stormwater	Lincoln Park Metro District 303.779.4252	Town of Castle Rock 720.733.2235 www.crgov.com/utilities
Castle Pines North Metro District	Douglas County School District	Southeast Metro Stormwater Authority	Town of Parker
303.688.8550	303.387.0027	303.858.8844	303.840.9546
www.cpnmd.org	www.dcsdk12.org	www.semswa.org	www.parkeroniine.org
Cherry Creek Stewardship Partners	Heritage Hills Metro District	SPLASH	
303.345.1675	303.792.7357	303.967.0244	
www.cherry-creek.org	www.heritagehilshoa.org	www.splashco.org	
City of Lone Tree	Highlands Ranch Metro District	Stonegate Village Metro District	
303.662.8112	303.791.0430	303.858.9909	
www.cityoflonetree.com	www.highlandsranch.org	www.svmd.org	
OPT	Please report accidental and illegal dumpi	ng to your local agency.	



Creek and highway cleanup efforts help offset pollution from our major transportation corridors. Contact your local agency to find out how you can get involved.

Colorado Community Newspapers agree: Please recycle this newspaper responsibly and partner with our communities for a better tomerrow.

Ad with CLEAR

HOUSEHOLD CHEMICAL WARNING: Thins paint, kills wildlife.

When using hazardous chemicals, store and dispose of containers responsibly, and clean up spills promptly according to manufacturer instructions. Your rivers, creeks and lakes depend on you. Harmful chemicals left on outdoor surfaces are picked up in the next rainstorm and sent directly to the nearest creek. Once these chemicals reach our waterways, they pose a threat to fish, wildlife, recreation and drinking water supplies.

Local stormwater agencies, including participants of the Douglas County Stormwater Co-op Group, SPLASH and SEMSWA, are teaming together to bring you this message. We take this so seriously that we posted this ad rather than send you more garbage in the mail. One thing is clear: our creeks, rivers and lakes depend on you.

THIS STORMWATER MESSAGE BROUGHT TO YOU BY



Visit www.onethingisclear.org to:

· Report accidental and illegal dumping to your local agency

- Search local volunteer events
 - · Find more helpful tips



For information about household chemical disposal services in your area, contact the Tri-County Health Department at www.tchd.org/householdchemical.htm

Colorado Community Newspapers agree: Please recycle this newspaper responsibly and partner with our communities for a better tomorrow.

Ad campaign creative donated by the Town of Castle Rock Utilities Department, Stormwater Division.

It's clear this stream is grateful

Our streams want to say thanks for giving them a gift this year. Your actions made a difference for keeping our water clean. You chose to properly dispose of household chemicals, pet waste and trash. You used fertilizers appropriately and kept harmful material out of runoff's path. You volunteered at local events to preserve our waterways. Keep up the good work. **Color Ads**

Local stormwater agencies, including participants of the Douglas County Stormwater Co-op Group, SPLASH and SEMSWA, are tearning together to bring you this message. We take this so seriously that we posted this ad rather than send you more garbage in the mail. One thing is clear: our creeks, rivers and lakes depend on you.

THIS STORMWATER MESSAGE BROUGHT TO YOU BY



Visit www.onethingisclear.org to: • Report accidental and illegal dumping to your local agency • Search local volunteer events • Find more helpful tips

Make your New Year's Resolution now; get involved. Contact your local agency for upcoming events.

Colorado Community Newspapers agree: Please recycle this newspaper responsibly and partner with our communities for a better tomorrow.

Ad campaign creative donated by the Town of Castle Rock Utilities Department, Stormwater Division.

Photo Laken along East Plum Dreak in Gastre Rock



Looking Forward

- >CLEAR provides the means to expand the campaign into other initiatives linked with the common message
 - >Creating a "Thank you" message on garbage and pet waste stations
 - >Finding public advertising venues such as buses, billboards, etc.
 - >Linking with local volunteer events to reinforce the message

CLEAR T-Shirts used at Creek cleanup events





OneThingIsClear.org Website

- >The website serves the following core functions:
 - >Provide stormwater hotline contacts for all participating MS4s
 - >Provide maps for users to find their respective MS4 contact
 - >Provide educational and volunteer opportunities
 - >Provide helpful and practical tips for protecting water quality
 - >Provide campaign resources for local agencies





Contact Us

Please reference our map to determine which authority is responsible for stormwater management in your area.

CLEAR MEMBER ROSTER

Permit Holder	Phone	Web Site
Castle Pines Metro District	303-688-8330	www.castlepinesmetro.com
City of Castle Pines North	303-705-0200	www.cpngov.com
Castle Pines North Metro District	303-688-8550	www.cpnmd.org
Town of Castle Rock	720-733-2235	www.CRgov.com/utilities
Cherry Creek Stewardship Partners	303-345-1675	www.cherry-creek.org
Douglas County	303-663-6181	www.douglas.co.us/stormwater
Douglas County School District	303-387-0027	www.dosdk12.org
Heritage Hills Metro District	303-792-7357	www.heritagehilishoa.org
Highlands Ranch Metro District	303-791-0430	www.highlandsranch.org
Lincoln Park Metro District	303-779-4252	
City of Lone Tree	303-662-8112	www.cityofonetree.com
Meridian Metro District	303-790-0345	www.dtcmeridian.com
Town of Parker	303-840-9546	www.parkeronline.org
Southeast Metro Stormwater Authority	303-858-8844	www.semswa.org
SPLASH	303-858-8844	www.splashco.org
Stonegate Village Metro District	303-858-9909	www.avmd.org







So what does it cost us?

>15 members share equally in the costs of the campaign and website>Website Costs

>Total Cost to develop OneThingIsCLEAR.org \$4,475

Cost per Member \$298



Ad Costs

>Annual cost for the ad campaign and website maintenance:

>Annual	website cost	\$1,200

- >Total Cost for Ads \$24,500
- >Matching funds from CCN (\$12,225)
- >Total Cost to CLEAR \$13,425

Cost per Member \$895



Cost comparison to traditional outreach materials

Agency	Circulation	Description	Total Cost	Comparison	
Town of Castle Rock	15,000	Print and mail brochure	\$5,500	8 newspaper ads for cost of 1	
	15,000	Ad as Utility bill insert	\$552	utility insert -or- 7 years of ads for cost of 1 mailer	
	90,500	One Half-page Newspaper ad	\$68		
Unincorporated Douglas County	¼ unincorporated Douglas County over 4 years and all commercial	Print and mail brochure	\$6,000		
	90,500	One Half-page Newspaper ad	\$68		





Looking outward

- >CLEAR provides the means for the campaign to expand beyond Douglas County
 - >Join the website to post stormwater hotline for your area
 - >Use ads in your local newspaper or other advertising venue
 - >Access the ads through OneThingIsClear.org
 - >Ad Campaign Style Guide defines identity and image standards for uses



Can we make a difference for water quality?

- >We believe we can, but change starts with us.
- >CLEAR is one way we can make a difference.
- >As seen in our ads: "We take this so seriously that we posted this ad rather than send you more garbage in the mail."
- >It ends with the masses. People are catching the vision and...
- >One thing is clear, our streams are grateful!



Thanks and Questions

THIS STORMWATER MESSAGE BROUGHT TO YOU BY

Castle Pines Metro District Castle Pines North Metro District Cherry Creek Steward Partners City of Lone Tree City of Castle Pines North

Douglas County Douglas County School District Heritage Hills Metro District Highlands Ranch Metro District Lincoln Park Metro District Southeast Metro SW Authority SPLASH Stonegate Village Metro District Town of Castle Rock Town of Parker

Riffle Rock Applications in Stream Restoration

Laura Kroeger/UDFCD Jim Wulliman and Derek Johns /Muller Engineering Co.

Cherry Creek at 17 Mile House





Cherry Creek at Pine Lane





Cottonwood Creek at Cherry Creek State Park

UDFCD Perspective



Recognize benefits of riffle rock, but...

Recognize limitations and complexities, too.

Sponsoring "white paper" to discuss background, design guidelines, and cautions.
UDFCD "White Paper"



Development of riffle rock during Cottonwood Creek Reclamation Project
Case studies for riffle drops and rock lining
Design guidance.
Construction guidance.

Cottonwood Creek Reclamation Project



Degraded Stream: Eroding, incised channel with dried-out, fragile overbanks.







Cottonwood Creek Reclamation Plan







Unique Properties of Riffle Rock
Rocks are interlocked and "braced"
No voids, so water flows on surface
Provides effective internal filter
Supports riparian vegetation







Cherry Creek Open Space Restoration Denver Denver Aurora Lakewood Cherry Creek Reservoir Englewood Cherry Creek Reservoir Greenwood Village Project . Littleton Southglenn Castlewood o Columbine Ken Caryl Arapahoe Co. Douglas Co. . Highlands Ranch Gateway

Pre-Project Conditions

Downstream Limit

Reach Length: 2500 feet

- Drop: 12 feet (0.5%)
- Floodplain Width: 1000 feet

Upstream Limit













Project Vision

Goal was not just stabilization, but restoration of natural stream processes. Preserve the Cherry Creek "sponge effect" Create a model project for environmental permitting Pursue opportunities for multi-function open space enhancements. Bring the community to the creek



Riffle Drop Advantages

Maintains shallow baseflow channel and high water table.
Low height and gentle slope allows drop to drown out.
Cost effective.
Supports riparian revegetation.
Enables fish passage
Natural appearance and function.
Acceptance by regulatory agencies.



Riffle Drop Configuration

Completed Project

Upper Marcy Gulch

"Before" Condition







Riffle Rock Lining and Boulder Drop

ALL ALL

Ability of Riffle Rock to Support Riparian Vegetation

Completed Project

Suitable Conditions for Riffle Drops

- Wide, flat floodplains with shallow active channels.
 - Low gradient streams where riffle drops can "drown out".
 - Vegetated overbanks that can handle periodic flooding.
- Locations where only a small drop height (approximately 1-foot) is desired.

Limitations Regarding Riffle Drops

Requires thorough hydraulic analysis and knowledgeable interpretation.
Riffle drops are very installation-sensitive, requiring attention during construction.
Requires preservation and enhancement of overbank vegetation.
Not a "hard point", so rock may move.

Riffle Drop Layout Longitudinal slope of 20:1 (5-percent) or flatter. Continue at least 1-foot below channel invert. Base on conservative long-term equilibrium slope. Crest width equal to baseflow channel, side slopes < 8:1 carried up 1.5 to 3 feet. Rock thickness at least 2 times D50. Additional rock thickness at upstream end o provide cutoff. D50 range 6 to 18-inches

Hydraulic Design

 Evaluate a broad range of flows. Low (1- or 2-year event) Medium (5- or 10-year event) High (100-year event)
 Strategically locate bank stations. At limits of relatively narrow baseflow channel
 Select appropriate Manning's n values. Relatively low for central channel, high for overbanks

Rock Sizing Methods

 Steep slope conditions. CSU equation (Abt, et al, 1988) USDA equations (Robinson, et al, 1998) COE equation (EM1110-2-1601, 1991)
 Mild slope conditions. UDFCD equation (Volume 1, 2001) COE Equation (EM1110-2-1601, 1991)
 Besign safety factor.




Approximate Proportions (loader buckets)	Material Type	Material Description
6	Riprap	D50=18-inch (Type H)
3	Void-fill material	7-inch minus crushed rock surge (100% passing 7-inch sieve 80-100% passing 6-inch sieve, 35-50% passing 3-inch sieve 10-20% passing 1.5-inch sieve)
1	Void-fill material	2 to 4-inch cobble (round washed river rock that is well graded, 100% passing 6-inch sieve, 35-50% passing 3-inc sieve, 5-20% passing 2-inch sieve)
1	Void-fill material	4-inch minus pit run surge (round river rock and sand, we graded, 90-100% passing 4-inch sieve, 70-80% passing 1.5 inch sieve, 40-60% passing 3/8-inch sieve, 10-30% passin #16 sieve).
1	Void-fill material	Type II bedding
¹ ⁄2 to 1	Void-fill material	Native topsoil
Top layer	Top dressing	Additional 4 to 12-inch cobbles (round washed river rock that is well graded, 80-100% passing 12-inch sieve, 35-50% passing 6-inch sieve, 5-20% passing 4-inch sieve) shall be mixed in on the surface of the void-filled riprap (coverin approximately 30% of the surface) prior to compaction of the void-filled riprap. Cobbles shall be fully embedded into the mass of the void-filled riprap.



Mixing Riffle Rock



Placing Riffle Rock



Grading and Compacting Riffle Rock



Backfilling side slopes



Construction Guidance Revegetating





Conclusions

Riffle rock offers some unique benefits, but...
 It has limitations and is not suitable for use everywhere.
 Look for UDFCD "white paper" to learn more.

The New USDCM Volume 3 CASFM 2010

Holly Piza, P.E., UDFCD and T. Andrew Earles, Ph.D., P.E., D.WRE, Wright Water Engineers, Inc.





Agenda

- Overview of Rewrite
- BMP Selection
- Quantifying Volume Reduction
- Treatment BMPs





USDCM Volume 3 History and Fundamentals

- First Release in 1992
- No Change in Concept



Overview of Manual

- 1. Stormwater Management and Planning
- 2. BMP Selection
- 3. WQCV and Runoff Volume Reduction
- 4. Treatment BMPs
- 5. Source Control BMPs
- 6. Construction BMPs
- 7. BMP Maintenance

Treatment BMPs	Source Control BMPs	Construction BMPs
 Grass Swales Sand Filter EDB (and so on) 	 Covering Storage & Handling Areas Disposal of Household Waste (<i>and so on</i>) 	 Inlet Protection Stockpile Storage Sediment Basins (and so on)



Notes

1 "Tributary impervious area" refers to the impervious area draining to the BMP, not the total area of the project site.

² For a successful wetland channel or basin, a water source (groundwater or baseflow) will be required.

³ In the Front Range of Colorado, irrigation, at least periodically in dry times, will be required to sustain a green roof.

⁴ If a regional facility will be used to provide the WQCV, some degree of onsite treatment MDCIA will still likely be required.

⁵ No Infiltration = underdrain and liner, Partial Infiltration = underdrain and no liner, Full Infiltration = no underdrain and no liner



liner Full Infiltration = no underdrain and no liner



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BMP Selection

Site Conditions

- Size
- Soils
- Contributing Drainage Area
- Groundwater
- Base flows
- Watershed Development Activities

Land Use

- Ultra Urban
- High Density Mixed Used
- Campus
- Industrial
- Low Density Mixed Use
- Residential
- Parks and Open Space

Treatment Processes

- Sedimentation
- Straining
- Infiltration or filtration
- Evapotranspiration
- Biological Uptake







Volume Reduction

- Minimization of Directly Connect Impervious Area (MDCIA)
- Infiltration-based BMPs
- Master planning level versus site level









SWMM Modeling Using Cascading Planes

- Conceptualize sub-watersheds as UIA, DCIA, SPA, RPA. Two approaches:
 - Two SWMM sub-catchments for each sub-watershed UIA + RPA and DCIA + SPA
 - Single SWMM sub-catchment with internal routing
- Rainfall distribution input to SWMM. Alternative: Use CUHP and specify D and R values.
- Parameters for infiltration, depression storage and other input parameters from *Runoff* chapter of UDFCD Manual.
- Two options for WQCV:
 - Pervious area depression storage
 - Storage unit with an outlet in SWMM.





Dimensionless Analysis

Conveyance-based BMPs:

$$K = Fct(\frac{F_d}{P}, A_r) = Fct(\frac{f}{I}, A_r)$$

Storage-based BMPs:

$$K = Fct(\frac{F_d}{P}, A_r, A_d \frac{WQCV}{P})$$

K = Imperviousness reduction factor $F_d = Pervious area infiltration loss (in)$ f = Pervious area infiltration rate (in/hr) corresponding to saturated hydraulic conductivityP = Design rainfall depth (in)I = Rainfall intensity (in/hr) $A_r = RPA/UIA$ $A_d = RPA$



9/10/2010







Chapter 4, Treatment BMPs

Overview	Grass Swale	Grass Buffer	Constructed Wetland Channel	Permeable Pavement	Bioretention (Rain Garden)	Extended Detention Basin	Sand Filter	Retention Pond	Constructed Wetland Basin	Green Roof	Underground BMPs
Functions											1
LID/Volume Red	Yes	Yes	Somewhat	Yes	Yes	Somewhat	Yes	Somewhat	Somewhat	Yes	No
WQCV Capture	No	No	No	Yes	Yes	Ye	Yes	Yes	Ya	Yes	Variable
WQCV+Flood Control	No	No	No	Yes	Yes	Yes	Yes	Yes	Yes	No	Variable
Typical Effectiveness	for Target	ed Polluta	ets"	(=)			s = -s		i = 0		
Sediment/Solida	Good	Good	Unknown	Very Good ¹	Very Good ⁴	Good	Very Good ¹	Very Good	Very Good	Unknown	Variable
Nutrients	Modenate	Moderate	Unknown	Good	Moderate	Moderate	Good	Moderate	Moderate	Unknown	Variable
Total Metals	Good	Good	Unknown	Good	Good	Moderate	Good	Moderate	Good	Unknown	Variable
Bacteria	Poor	Poor	Moderate	Poor	Moderate	Poor	Poor	Poor	Poor	Poor	Variable
Other Considerations	8 - 3		(i)	8 - Z		80 - S	2 B	(6)	8 - D		
Life-cycle Costs ⁴	Low	Low	Low	High ²	Moderate	Moderate	Moderate	Moderate	Moderate	Unknown	Moderate

¹ Not recconsended for watershede with high sediment yellds (unless pretreatment is provided).

² Does not consider the life cycle cost of the conventional pavement that it replaces.

³ Based primarily on data from the International BMP Database (www.bmpdatabase.org).

Based on BMP-REALCOST available at www.udfcd.org.



Grass Swale



- Removal of sediment and associated constituents through filtering (straining)
- Reduction of storm sewer systems in the upper portions of a watershed
- A less expensive and more attractive conveyance element

Grass Swale				
	Functions			
LID/Volume Red.	Yes			
WQCV Capture	No			
WQCV+Flood Control	No			
Typical Effectiveness for Targeted				
	Pollutants ³			
Sediment/Solids	Good			
Nutrients	Moderate			
Total Metals	Good			
Bacteria	Poor			
Other Considerations				
Life-cycle Costs ⁴	Low			
³ Based primarily on data from the				
International BMP Database				
(www.bmpdatabase.org).				
⁴ Based on BMP-REALCOST available				
at <u>www.udfcd.org</u> .				



Grass Swale

Design Flow	Maximum	Maximum	Maximum
	Froude Number	Velocity	Flow Depth
2-year event	0.5	1 fps	1 foot







Grass Buffer



Photo Courtesy Muller Engineering

- Filters (strains) sediment and trash.
- Reduces directly connected impervious area.
- Can easily be incorporated into a treatment train approach.
- Provides green space available for multiple uses including recreation and snow storage.
- Straightforward maintenance requirements when the buffer is protected from vehicular traffic.

Grass Buffer					
Functions					
LID/Volume Red.	Yes				
WQCV Capture	No				
WQCV+Flood Control	No				
Typical Effectiveness for Targeted					
Pollutants ³					
Sediment/Solids	Good				
Nutrients	Moderate				
Total Metals	Good				
Bacteria	Poor				
Other Considerations					
Life-cycle Costs ⁴	Low				
³ Based primarily on data from the					
International BMP Database					
(www.bmpdatabase.org).					
⁴ Based on BMP-REALCOST available at					
www.udfed.org					








Photo Courtesy Bill Wenk





Permeable Pavement Systems



Photo Courtesy SEH

- Provides capture and slow release of the WQCV, providing water quality treatment in an area that serves more than one purpose.
- Can be used to reduce effective imperviousness or alleviate nuisance drainage problems
- Benefit tree health by providing additional air and water to nearby roots.
- Less likely to form ice on the surface than conventional pavements.
- Some can be used to achieve LEED credits.

Permeable Pavement				
	Functions			
LID/Volume Red.	Yes			
WQCV	Yes			
WQCV+Flood				
Control	Yes			
Typical Effectiveness for Targeted				
0.1	Pollutants			
Sediment/Solids	Very Good			
Nutrients	Good			
Total Metals	Good			
Bacteria	Poor			
Other (Considerations			
Life-cycle Costs ⁴	High ²			
¹ Not recommended for watersheds with high sediment yields (unless protreatment)				
is provided.				
² Does not consider the life cycle cost of				
the conventional pavement that it replaces.				
³ Based primarily on data from the				
International BMP Database				
(www.bmpdatabase.org).				
⁴ Based on BMP-REALCOST available at				
6.77	www.udicd.org.			
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Statistical data				
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Permeable Pavement Systems









Filter and Drain Design

Class C Filter Material

Sieve Size	Mass Percent Passing Square Mesh Sieves
19.0 mm (3/4")	100
4.75 mm (No. 4)	60 - 100
300 µm (No. 50)	10 - 30
150 µm (No. 100)	0 – 10
75 μm (No. 200)	0 - 3

Slotted Pipe Dimensions	Pipe Size	Slot Length	Slot Width	Slot Centers	Open Area
Slotted i pe Dimensions	4"	1-1/16"	.031"	.413"	1.90
	6"	1-3/8"	.031"	.516"	1.98



Filter and Drain Design

U.S. Army et al (1971)

$$\frac{D85}{Slot Width} > 1.2$$

U.S. Bureau of Reclamation (1973)

$$\frac{D85}{Slot Width} > 2$$

Class C Filter Material D85 (min) = 2.60 mm D85 (max) = 11.00 mm Maximum acceptable slot width based on U.S. Reclamation criteria is 0.051"





Stepped or Sloped Installation





12-Hour Drain Time for Infiltrating BMPs

 $Diameter_{(12 hour drain time)} = \sqrt{\frac{Volume}{1414 y^{0.41}}}$

Where:

Diameter = orifice diameter (in) y = distance from the lowest elevation of the storage volume (ft) (i.e. surface of the filter) to the center of the orifice. Volume = volume to drain in 12-hours (WQCV) (ft³)



Permeable Pavement Systems

Example Construction Drawings Notes

- Excavation of subgrade shall not commence until after the preconstruction meeting.
- Subgrade shall be excavated using low ground pressure (LGP) track equipment to minimize over compaction of the subgrade¹.
- Grading and compaction equipment used in the area of the permeable pavement should be approved by the engineer prior to use.
- Loose materials shall not be stored on the permeable pavement area.
- The contractor shall, at all times during and after system installation, prevent sediment, debris, and dirt from any source from entering the permeable pavement system.
- Placement of the wearing course shall not begin until fine grading and landscaping in adjacent areas is complete.

¹For partial and full infiltration sections, see Design Procedure.

Permeable Interlocking Pavement (PICP)



2. A PAVEMENT DESIGN SHOULD BE PERFORMED IN AREAS OF VEHICULAR USE.

FIGURE PICP-1 PICP PAVEMENT SECTION

- Can be used for traffic calming
- Can be used in intersections

• Can be placed back if utility cuts or other patches are required.

• Maintains infiltration rates well.

• Provides flexibility in design options such as color and patterns.

• LEED credits

PICP

- Use the herring bone pattern with an overall length to thickness (aspect) ratio of three or less for vehicular applications.
- Select units with a maximum opening of 0.5 inches (measured from the chamfers) where needed to satisfy ADA requirements.
- Ensure all pavers are at least 40% of the original size.



PICP

- Ensure all pavers are at least 40% of the original size.
- Provide a sailor or soldier course at all edges









Concrete Grid Pavement









9/10/2010

Pervious Concrete





Pervious Concrete



Specifier's Guide for Pervious Concrete Pavement Design Version 1.2





• Use the Specifier's Guide for Pervious Concrete Pavement Design

• Select a contractor with prior experience in successful pervious concrete installation

• Mix, transport and discharged within one hour of the introduction of mixture water to the cement.

• Compaction of pervious concrete is achieved by rolling. Cross rolling should be performed using the minimum number of passes required to achieve an acceptable surface.

Pervious Concrete

- Joints should be formed by rolled using a "pizza cutter roller." Joints should never be cut.
- Place between April 1 and November 1 and when the ambient temperature is between 40° and 90° Fahrenheit.
- Mixture water quantity is critical. The correct quantity has been achieved when the concrete has a wet metallic sheen.
- Add an air entraining agent.
- The pavement surface must be covered with a six-mil thick polyethylene sheet. The sheet should remain secure and in place until the concrete has reached a maturity equivalent to 14 days of curing at 70° Fahrenheit at 95% relative humidity. No vehicular traffic should be permitted during this time.
- Fogging should begin once the concrete has been placed and should continue until the polyethylene curing cover is secured.

9/10/2010

Porous Gravel



Sand Filters



Photo Courtesy Fred Bromberger

Sand/Media Fi	lter
Functions	
LID/Volume Red.	Yes
WQCV Capture	Yes
WQCV+Flood Control	Yes

Typical Effectiveness for Targeted Pollutants³

	-
Sediment/Solids	Very Good ¹
Nutrients	Good
Total Metals	Good
Bacteria	Poor
Otl	ner Considerations

Life-cycle Costs⁴ Moderate ¹Not recommended for watersheds with high

sediment yields (unless pretreatment is provided).

³Based primarily on data from the International BMP Database (<u>www.bmpdatabase.org</u>).

⁴Based on BMP-REALCOST available at

www.udfcd.org



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Bioretention (Rain Gardens or PLDs)











Bioretention

Why not Peat?

- Environmental Impacts
- Peat is not produced in Colorado

Why Paper?

- Compost alone leaches more nutrients than desired
- Paper captures nutrients from the compost for slow release to roots
- Paper temporarily slows the infiltration rate of the media and retains moisture

Extended Detention Basin (EDB)

Expand criteria for various size EDBs

Primarily related to forebay size, depth and outlet into the trickle channel

Include guidance on Full Spectrum Detention

Includes integration with UD-BMP

Increase Flexibility

Guidance on Soft Bottom Trickle Channels and Micropools

Extended Detention Basin (EDB)

Most Common Mistakes

- No micropool
- Well Screen does not extend into the micropool
- No bottom Stage (initial surcharge volume)



Full Spectrum Detention

Most Common Misconceptions

- Does not result in a larger pond
- UDFCD does not recommend adding part or all of the WQCV (or the EURV) to the 100-yr detention volume
- Recommended drain times are approximate
- Specific design for metering other storm events is not necessary



9/10/2010

Green Roofs







Green Roofs

Design and Maintenance Guidelines for Green Roofs in the Arid and Semi-Arid West

Includes a quote from EPA, Region 8 on using green roofs to satisfy capture of the WQCV

Contains over a dozen Denver area green roofs case studies including:

- Residential (SF and MF)
- Commercial
- Municipal
- Federal

Design Guidelines and Maintenance Manual for Green Roofs in the Semi-Arid and Arid West

> In collaboration with Orean Rock to Healthy Ches. City and County of Domain Environmental Protection Agency Region 8 Unter-Dimensional Advanced Counted District Collocols State University



May 14th 2010



Underground BMPs

- Not all BMPs are created equal
- Why underground BMPs have not previously been included
- When should underground BMPs be considered
- Guidance on evaluating data
 - TARP Tier 2 (field data)
 - What's included:

Monitoring Plan Element
Number of storm events
Parameters
Quality Assurance/Quality Control (QA/QC)—monitoring plan
QA/QC—laboratory analyses
Representativeness—sampling method
Representativeness—storm characteristics
Representativeness— precipitation depth
Representativeness—antecedent dry period
Data Analysis



Welcome!

Emergency Management for Floodplain Managers: What Happens When It Actually Floods?

> A Workshop to Better Prepare Local Floodplain Managers for Actual Flood Events

> > CASFM Annual Conference September 2010 Snowmass, CO





Workshop Goals

- Introduce local floodplain managers to emergency management
- Define local floodplain management roles and responsibilities before and after a flood
- Identify preparedness and mitigation actions to be take now that will assist the local floodplain manager before and after a flood

September 2010





Workshop Agenda

- Introduction to Workshop
- Group Activity #1: Flood Response
- Group Activity #2: Flood Recovery
- What Can You Do Now? Flood Preparedness and Mitigation Actions





Introductions

- Jeff Brislawn, CFM
- Hillary King

September 2010





Workshop Materials

- Handouts
- Take-away
- Follow-up





September 2010




The Emergency Management Cycle



CASFM Annual Conference Snowmass, CO





Emergency Management Issues

Interagency Coordination > NIMS/ICS > Terminology & Acronyms! \succ The EOC > Public Information > The Media **Post-Disaster Decision Making** Non-flood issues



ESF #1 Transportation ESF #2 Communications ESF #3 Public Works & Engineering ESF #4 Firefighting ESF #5 Emergency Management ESF #6 Mass Care and Housing Annex ESF #7 Resource Support ESF #8 Public Health and Medical ESF #9 Urban Search and Rescue ESF #10 Oil and Hazardous Materials Response ESF #11 Food, Water & Natural Resources ESF #12 Energy ESF #13 Public Safety & Security ESF #14 Long-term Community Recovery & Mitigation ESF #15 Public Information



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Group Activities

- I. Flood Response Scenario
- II. Flood Recovery Scenario





What Can You Do Now? Preparedness and Mitigation Actions

- Communication and Coordination
- Training and Exercises
- Planning
- Documentation and Mapping
- Mitigation Policies and Projects
- Public Information







What Can You Do Now? Communication and Coordination

- Know your local players
 - > Emergency manager, PIO, IT staff , and others
 - > Use mitigation planning process
- Know your state/federal players
 - > Be familiar with assistance programs/contacts
 - > Take advantage of workshops offered
- Educate your elected officials
 - > Use HAZUS, tabletop exercises
- Have media ready materials (programs, common terms)





What Can You Do Now? Training and Exercises

- Damage Assessment Team
- RSDE & ICC
- Benefit-Cost Analysis
- ICS/NIMS
- The retrofit course
- Lenders and agents workshops
- Managing Flood-Prone Development through NFIP







What Can You Do Now? Planning

- Floodplain Management Plans (FMA, CRS, SRL)
- Mitigation Plans (DMA, PDM)
- Emergency Operations Plans
- Recovery Plan
- Other Community Plans (Master, CIP, Transportation)
- Plans of state/feds for your community
- Family preparedness plans
- Information on emergency/disaster declarations in ordinance



amec

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What Can You Do Now? Documentation and Mapping

- Map repetitive losses, hazardous materials, critical facilities, historic buildings, mitigation projects
- Document variances issued, road/bridge elevations, CAVs, public works maintenance data, stream gage data, high water mark collection procedures
- Protect information off-site storage, Go Box



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What Can You Do Now? Mitigation Policies and Projects

- National Flood Insurance Program
 - Beyond minimum standards
 - ➢ Repetitive losses
 - Protect critical facilities
 - Community Rating System
- No Adverse Impact
- Management of natural floodplain functions and resources
- Regulate to future conditions







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What Can You Do Now? Public Information

- Team Flood Smart Outreach Toolkits
- Warning and evacuation
- NOAA Weather Radios
- StormReady Certification
- Mitigation Open House
- Business Continuity Planning
- Citizens Guide to Flood Awareness
- NFIP materials/forms at front office (CRS credit)





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Workshop Conclusion: Goals Check

- Introduce floodplain managers to emergency management
- Define floodplain management roles and responsibilities before and after a flood
- Identify preparedness and mitigation actions to be take now that will assist the local floodplain manager before and after a flood





Workshop Conclusion

- Questions?
- Take Home Packets



Thank You! Emergency Management for Floodplain Managers: What Happens When It Actually Floods?

A Workshop to Better Prepare Local Floodplain Managers for Actual Flood Events

> CASFM Annual Conference September 2010 Snowmass, CO



CASFM CONFERENCE – 2010 THE PLANNING PROCESS FROM INCEPTION THROUGH IMPLEMENTATION

PRESENTED BY APA COLORADO Steve Westbay AICP, CFM Community Development Director – City of Gunnison

> <u>swestbay@cityofgunnison-co.gov</u> phone #: 970-641-0558

I. Planning and Development Process – Colorado Planning Law

Reader Note: The majority of this information presented in Section 1 is derived from *Colorado Land Planning and Development Law* (5th Addition, published by APA Colorado). Other sources are referenced when applicable.

A. LOCAL GOVERNMENT – HOME RULE & STATUTORY DEGINATIONS

- 1. **General.** Under the *Colorado Constitution*, local jurisdictions may become a home rule government by the creation of its own charter.
- 2. **Statutory Powers.** Statutory jurisdictions only have the powers explicitly given to them by state statutes. If there is no explicit grant of power provided by state statutes, a statutory government cannot engage in the activity.
 - Planning practitioners in statutory jurisdictions should askWhere in the state statutes does it say or imply that local government can act in a certain manner?
- 3. Home Rule Powers. Home Rule jurisdictions have the power to create ordinances and laws to extend to all governmental matters include subdivision and zoning. However, there are limitations to the home rule powers and these limitations pertain to *matters of state interest*, restrictions related to the TABOR and Gallagher Amendments, and other specific state and federal laws.
- Planning practitioners in Home Rule jurisdictions should askWhere in the Charter or Municipal Code does it say or imply that local government can act in a certain manner?



- 4. **Appeals from Local Decisions.** Appeals may be brought forth by citizens, applicants, the local government or other government agencies for either denials or approvals.
 - The appeal of Legislative Acts (new ordinance regulations, et al), are reviewed under the *Colorado Rules of Civil Procedures*. For example, a new land use code could be appealed on the premise that it does not allow for due process in zoning amendments. The court is usually asked to provide a Declaratory Judgment, which allows citizens to obtain a determination of validity under prevailing case law, state statutes or the *Constitution*.

• The appeal of Quasi-Judicial Acts (affecting individual land use rights), are reviewed under the *Colorado Rules of Civil Procedures*, which address protocol for civil law cases, and may allow for punitive or compensatory damages.

B. LAND USE PLANNING - THE COMPREHENSIVE PLAN

- 1. **General.** The act of land use planning is separate and distinct from the act of zoning. The land use plan (Comprehensive or Master Plan) sets forth the most desirable land uses based on community perspective. Zoning provides a detailed means for giving legal effect to the plan's policies.
- 2. Advisory Context. Colorado case law provides that adopted land use plans are advisory only and do not bind the discretion of a jurisdiction in regard to specific subdivision or zoning decisions.
- 3. **Mandatory Context.** Home Rule jurisdictions may require zoning and subdivision proposals to be established in accordance with jurisdiction's comprehensive plan, and this policing power has been upheld by the Colorado Supreme Court. However, the comprehensive plans must be sufficiently detailed.
- 4. **Three Mile Plans.** The Colorado Revised Statutes, §31-12-105 (1)(e) requires that there be a plan in place for an area extending three miles beyond a municipality's boundaries prior to the annexation of territory into the municipality. Additionally, state statutes give municipalities express authority to enter into agreements with adjoining counties for joint participation in land use planning, subdivision procedures and zoning for specific areas designated in the Intergovernmental Agreement (IGA). Generally, policing powers are not extended through the IGA.



- Regional Councils. Many states empower regional councils of government to regulate planning. Regional councils of government were enacted by the General Assembly in 1972 in order to provide structure to governmental functions transcending local government boundaries. However, the regional councils in Colorado have no policing powers. Established regional councils include:
 - Denver Regional Council of Governments
 - Northwest Regional Council of Governments
 - Pikes Peak Area Council of Governments
 - Pueblo Area Council of Governments
 - Region 10 (West Central Colorado)
 - South Central Council of Governments
- 6. **State Level Planning.** Several administrative branches of Colorado state government address planning as part of their respective duties.
 - Colorado Department of Local Affairs (DOLA) – Division of Local Government. Acts as a liaison between state and local governmental entities. Budget

Labradoodle Labrador/Poodle cross Cute & intelligent



Great Doodle Great Dane/Poodle cross Large, intelligent & gentle



Cockradoodle (doo) Common Brown Roach/Poodle cross Tough, fast and adaptable



Noodle Egg Noodle/Poodle mix Add sauce and parmesan cheese to taste

Designer breeds

restrictions severally limit the assistance provided by DOLA.

- Colorado Land Use Commission. This Commission was created by the General Assembly in 1970 to formulate land use planning program at the state level. This commission was specifically directed to synthesize existing land use programs at federal, state and local levels. The General Assembly has not appropriated significant money to the Commission and this body only acts to fulfill responsibilities required by statute.
- Colorado State Land Board. This is a five member board appointed by the Governor. The Board serves as the trustee for school trust lands. The Board also manages the Stewardship Trust, consisting of about 300,000 acres of school trust lands, which are to be protected due to beauty, natural values, open space and wildlife habitat.
- **1041 Regulations** Activities of Statewide Interest. Statutory provisions (§24-65.1-101 through 502), which are commonly referred to as 1041 Regulations, define a specific types of development that may impact the state. They also define criteria to be used by local governments in planning of such projects, and allow local jurisdictions additional regulatory powers. Defined areas of state interest include the following.
 - 1. Mineral Resource Areas
 - 2. Natural Hazard Areas
 - 3. Certain areas containing historical, natural or archeological resources.
 - 4. Airports, highways, major public utilities, mass transit terminals and other key facilities.

C. LOCAL GOVERNMENT LAND USE CONTROL ENABLE ACT-CRS §29-20-102

- 1. Enabling Legislation. In 1974, the General Assembly enacting the *Land Use Enabling Act, H.B. 1034*, which conferred broad authority for local government planning and regulation of land use, and the *Areas and Activities of State Interest Act, H.B. 1041*, which allowed local government to designate matters of statewide interest for regulation through a permit system. The *Land Use Enabling Act* grants broad authority to local governments to plan for and regulate the use of land within their respective jurisdictions. The act enables local government the ability to conduct comprehensive plans, and to establish zoning, subdivision, and development regulations.
- 2. **Zoning History**. In 1926 the United States Supreme Court herd *Village of Euclid v. Ambler Realty*, and the court



determined that zoning is a legitimate exercise of local government police powers. Statutory jurisdictions only have the zoning powers allowed by state statutes (CRS §31-23-301 through 312; §31-15-401 and §31-15-50). Police powers allow local jurisdiction to regulate types of uses, dimensional standards (height, setback lot size, etc), regulate hillside development impacts, define street configurations and enhance the aesthetic values of the community.

- 3. Legislative and Quasi-Judicial Actions. The initial enactment and subsequent amendments of development standards and zoning maps are designated as legislative actions. While rezoning applications, conditional uses, variances and subdivision actions are quasi-judicial actions.
- 4. Areas of State Interest. The General Assembly has declared several areas of statewide concern that limit the general granting of zoning powers to local jurisdictions.
 - Zoning ordinances must accommodate group homes for the aged and home for persons with mental illness as residential uses.
 - Development standards cannot prohibit manufactured homes that meet the basic standards of the local building code.
 - However, manufactured housing is subject to the local jurisdiction's building codes addressing unique public safety matters such as snow load, wind shear, seismic design and energy conservation (CRS §30-28-115(3)).
 - The imposition of rental control on private residential housing is a matter of state interest and local jurisdictions cannot establish regulations directed at rent control.
 - Local zoning ordinances cannot create limitations or restrictions based on race or color.
 - Jurisdictions with populations greater than 65,000 are required to adopt a plan for the extraction of commercial mineral deposits.
 - Counties are required to establish procedures for locating and designating solid waste facilities.



- 5. **Rezoning Map Amendments.** Local government is empowered by Enabling Legislation to establish specific districts and regulate land uses through various provisions within the zoning code. Zoning district boundaries are established by the Zoning Map. Within related jurisdictional boundaries rezoning applications can be initiated by City Councils, County Commissioners, Planning and Zoning Commissions and local property owners.
 - Local jurisdictions may initiate comprehensive rezoning of large areas. These types of rezoning acts are generally initiated to fulfill the objectives of the comprehensive plan. These comprehensive rezoning processes are treated as legislative acts and are accompanied by the adoption of a new zoning map.
 - Rezoning of individual areas is more common, and they are usually requested by property owners. Rezoning requests are usually subject to compliance with standardized criteria statements contained in the local land development codes.
 - Spot Zoning is not defined by legislation, but is a colloquialism describing the application of a specific zoning district classification to a small area which is surrounded by a larger different (usually less intense) zone district (Craig Hullinger & Chuck Eckenstahler 2004, Planning.blogst.com). There are often logical reasons to zone small parcels in a unique manner such as a corner lot that provides services to a local neighborhood. Good planning practices will prevent the appearance of spot zoning. The key is to adhere to established criteria statements for rezoning and ensure the application request conforms to an up-to-date comprehensive plan.



- 6. **Planned Unit Developments**. Planned Unit Developments (PUDs) are a unique form of zoning that provides flexible alternatives to the common zoning regulations. PUDs allow local jurisdictions wide discretion to negotiate almost every aspect of the proposed development and in return the developer is granted great flexibility in use designations, dimensional standards, and design.
 - PUDs are a negotiated process and neither party is forced to accept the propositions.
 - PUDs are authorized by state statutes (CRS §24-67-101 through 108).
 - The statutes require that PUDs conform to the comprehensive plan.
 - PUDs are required to follow a written guide that establishes the standards, conditions and provisions directing the development of the PUD.
 - PUDs may contemplate one or several zoned districts, which are subject to formal review and approval. They are also subject to municipal provisions for subdivision.
- 7. Essential Nexus. Zoning regulations must bear a reasonable relationship (nexus) to some legitimate government interest such as protecting the health, safety or welfare of the public. This nexus between zoning and the public welfare provides the basis for the constitutionality of land use regulations.
 - A regulation as applied to specific property must not create an unreasonable burden on the owner, even if the regulation is reasonably related to a legitimate government interest.
 - A land owner is not entitled to the most profitable or best use of their property. A zoning regulation will generally be upheld if the land owner has not been deprived of all reasonable economic use of private property.
- 8. **Dedications, Exactions & Impact Fees.** Development regulations may impose exactions, impact fees, land dedications or require certain improvements in relation to a subdivision or development application. However,



Hourly-Billing Lawyer Cages...Patent Pending. ©10CharlesFincher06.28 Scribble-in-Law.com

such exactions may be challenged as exceeding police powers or that they constitute an invalid tax; and the exactions may be challenged as a "taking" of private property rights.

- *Colorado Revised Statutes* provides broad authority to jurisdictions and statutes anticipate exactions as a valid power of local government.
- In 1994 the U.S. Supreme Court decided <u>Dolan v. City of Tigard</u>, which specified how exactions of real property are to be measured. While the court did not require mathematic precision, the ruling requires that local government quantify the impacts created by the development and then document how the exaction will alleviate the related impact. The Supreme Court found that the exaction must be *roughly proportional* to the impact created.
- 9. Nonconforming Uses. A nonconforming use is a pre-existing lawful use that becomes prohibited as a result of a new code adoption. Zoning Codes often grant the right to continue that use as a *legal nonconforming use*. This grandfathering is not absolute and the zoning code may require the removal of the use over time.
 - The Colorado Supreme Court has stated that zoning provisions allowing nonconforming uses should be strictly applied by the jurisdiction because such uses can depress property values, contribute to urban blight and may present life-safety issues.
 - Nonconforming uses are banned from expanding, additional nonconforming uses and if structures are destroyed they cannot be replaced. Restarting a nonconforming use after it ceases for a certain period of time is prohibited.
- 10. Nonconforming Structures. Nonconforming structures are generally in conflict with dimensional standards such as height, setback, or percent coverage. Nonconforming structures are treated similar to nonconforming uses. The landowner is entitled to maintain the structure subject to reasonable limitations. The owner cannot alter the structure in a manner that expands the nonconforming structure. If the nonconforming structure is destroyed, it cannot be rebuilt in a nonconforming manner. However, variances may be granted in situations where a "hardship" is demonstrated. Variances are heard by the local Zoning Board of Adjustments and Appeals.
- 11. **Conditional Uses.** A conditional use is generally compatible with the permitted uses in a particular zone district, but which



When lousy renovations meets postmodernism

can be denied if it does not fit in with the specific surroundings. These uses usually have inherent impacts such as increased traffic, noise, or odor. Mitigation measures are often applied to the proposed use through conditions limiting the hours of operation, requiring that activities be conducted within structures that reduce noise, or by applying other conditions.

D. SUBDIVISION

- 1. **Subdivision Intent**. A subdivision plat is a map showing how a given piece of property is to be divided into lots and blocks, and identifying streets, easements, parks and other land intended to be dedicated to the public. The plat provides the necessary survey details to legally describe individual parcels; it ensures that lots are appropriate sizes and have adequate frontage; it serves to verify that utilities extensions are manageable, and it ensures that all lots have legal access.
- 2. **Plat Details**. Subdivision plats contain several statements, signature blocks, and other necessary details necessary for proper execution. Based on statutory requirements, most municipalities require that plats contain a legal opinion ensuring that land title is not encumbered, a surveyor statement ensuring surveyor accuracy, a description of the basis for bearing used by the surveyor, a dedication statement ensuring legal dedication of public spaces, acceptance signatures by the mayor, and includes County Clerk and Recorder information.
- 3. **Review Process**. Subdivisions are often reviewed in three phases including a sketch plan, preliminary plan, and final plan. Sketch plan reviews define the concept of the subdivision without providing any engineering plan detail. The preliminary plan is a very detailed process requiring the submittal of preliminary engineering designs for streets, water, sewer, electrical system, and stormwater and irrigation utilities. The



"So what do you think of all this government paperwork, boss?"

final plan concentrates on the legal details of the subdivision including review of the plat language, improvement agreements, and final engineer plans. Generally, final plats should not be approved with conditions, because all related issues should be addressed before that point of the process.

- 4. **Common Interest Communities.** Under statutory definitions, a subdivision includes any parcel of land used for condominiums, apartments or other multiple dwelling units or which divides a single parcel into two or more parcels, separate interest, or interest in common. Common interest communities establish either fee-simple ownership, which is commonly a house with a yard area (townhomes), or an airspace unit where multi-family units are contained in a single structure.
- **E. DUE PROCESS** (Source: Hayes, Phillips & Maloney, P.C., Attorneys at Law, Rocky Mountain Land Use Institute Presentation, 2001).

1. Any applicant appearing before a local body requesting a decision of that local body when acting within the scope of its powers is entitled to receive due process of law.

2. Due process is guaranteed by the *United States Constitution (USC)*.

- Amendment 5 provides that no person shall "be deprived of life, liberty, or property, without due process of law;" Article 14, Section 1 provides "Nor shall any state deprive any person of life, liberty or property without due process of law…"
- A similar provision exists in the *Colorado Constitution* at Article II, Section 25. "No person shall be deprived of life, liberty or property without due process of law."



Counsel's opening was so slanted he struggled to maintain his balance.

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- In the land use context, because property rights are at issue, the provisions of each of the constitutional sections cited above, together with 42 USC. §1983 are applicable.
- 3. Legislative vs. Quasi-Judicial Actions The level of due process required to be afforded depends upon whether the action of the governing body is legislative or quasi-judicial in nature.
 - Legislative action is usually reflective of some public policy relating to matters of a permanent or general character, is not normally restricted to identifiable persons or groups, and is usually prospective in nature. Quasi-judicial action, on the other hand, generally involves a determination of the rights, duties, or obligations of specific individuals on the basis of the application of presently existing legal standards or policy considerations to past or present facts developed at a hearing conducted for the purpose of resolving the particular interests in question. This type of decision-making is designated "quasi-judicial" precisely because it bears similarities to the adjudicatory function performed by courts. If a statute or ordinance authorizes the exercise of quasi-judicial authority but does not provide for notice and hearing, these basic requirements may properly be implied as a matter of fundamental fairness to those persons whose protected interests are likely to be affected by the government decision.
 - The leading case on what makes a matter quasijudicial is <u>Snyder v. City of Lakewood</u>, 542 P.2d 371 (Colo. 1975). In <u>Snyder</u> the Court identified three criteria for identifying a matter as quasi-judicial, which are: (1) a state or local law requiring that the body give adequate notice to the community before acting; (2) a state or local law requiring that the body conduct a public hearing, pursuant to notice, at which time concerned citizens must be given an opportunity to be heard and present evidence; and, (3) a state or local law requiring the body to make a determination by applying the facts of a specific case to certain criteria established by law.
- 4. Elements which must be present in a hearing.
 - The first element of fundamental fairness is "adequate notice" to place all parties in interest on



Defense counsel tries to minimize damages. ©10CharlesFincher04.19 Scribble-in-Law.com

notice that a hearing is to be held, and giving fair notice as to what will be the scope and requested outcome of that hearing. Failure to give adequate notice may void any action taken at the hearing.

- Level of Formality. The level of formality to be afforded at the hearing is essentially a question of local preference, so long as adequate opportunity is afforded for all viewpoints which are relevant to the application to be aired.
- Necessity of Findings. In order to comply with due process requirements, and to insulate the decision made from successful judicial attack, findings must be made by the legislative body (findings are always better put in writing), which relate both to the evidence presented and to the criteria which exist and which are applicable to the application being heard. <u>Bauer v. City of Wheat Ridge</u>, 513 P.2d 203.
- **Impartial Decision-making Panel**. Applicants are entitled to an impartial panel. Any evidence of a pre-decision, or decision based on matters other than those appearing in the record, potentially subjects the decision-makers to liability to the application for violation of the applicant's due process rights.

F. ANNEXATION

- 1. Legislative Intent. The Municipal Annexation Act of 1965 is that portion of the Colorado Revised Statutes found at CRS
 - 31-12-101 through 123. The policy intent is to encourage natural and orderly development of municipalities. Annexations are initiated by the submittal of a petition to the municipality. The petition must contain signatures from 50% of the affected land owners and those signers must own more than 50% of the land area.
- 2. **Municipal Annexation Policies.** Municipalities may adopt policies, and submittal data requirements either by ordinances, resolutions or provisions of their comprehensive plan. Because the process is legislative, the municipalities may require exactions, as part of the negotiation, that are not afforded under subdivision or other land use review processes.
- 3. Annexation Eligibility (CRS 31-12-104).
 - Not less than 1/6 of the proposed annexation perimeter area is contiguous with the



annexing municipality boundary.

- A community interest exists the area is integrated with, or is capability of being integrated with, the annexing municipality.
- The annexation boundary does not extend more than three miles from the city boundary.

4. Annexation Limitation (CRS 31-12-105).

- Annexation boundaries cannot divide and individual's real property without written consent.
- The proposed annexation boundaries cannot cover an area encompassing a separate annexation petition submitted to another municipality.
- Annexation boundaries cannot detach a school district boundary unless it is allowed by the affected school district.
- A municipality cannot deny reasonable access to landowners adjoining a platted street or alley being annexed.

5. Annexation of Enclaves (CRS 31-12-106)

- Enclaves are unincorporated areas of land entirely contained within the outer boundaries of the annexing municipality.
- If an enclave has existed for more than three years after an annexation, the municipality may annex the land area without complying with the Limitation Provisions (31-12-105).

6. Petitions for Annexation 31-12-107

- An annexation petition must contain several elements including allegations that the Eligibility and Limitation provisions of the *State Statutes* have been met, a legal description of the proposed, and a boundary map.
- Many municipalities require additional information in conjunction with the petition submittal. For example many municipalities require land use and utility master plans, a fiscal impact report, and other similar data to help assess development feasibility.

II. New Planning Paradigms

A. URBAN MIGRATION and DEMOGRAPHIC TRENDS

In 2006 the United States population reached 300 million and this figure is anticipated to increase to 400 million before the mid-century mark (2050). The growth rate is attributed in some part to natural growth (birth/death ratio), but 60 percent of the growth will be attributed to migration. Eastern and western European countries and Japan are projected to have falling populations in the future. The U.S. population projections exceed those for China and only lag behind growth rates of India.

- US Growth Rate Projections. America adds 100 million people faster than any other nation except India and Pakistan – but *faster* than China. *Source*: Arthur C. Nelson, Metropolitan Institute at Virginia Tech.
 - 200 million in 1968
 - 300 million in 2006
 - 400 million in 2032
 - 500 million in 2050



2. **Future Building Construction Trends.** Expanding population trends in the USA are a reality. The real questions related to planning are founded in contemplating the geographic distribution and extent of capital development required to accommodate this growth. Joel Kotkin (*The Next Hundred Million: America in 2050*, Penguin Press, 2010), suggests that growth will be accommodated in mixed use villages, and that small to mid-sized cities in the Mid-West and Rust Belt will see a significant resurgence, but he does not refer to this growth as a suburbanization land use.

Dr. Arthur C. Nelson suggests a somewhat differing view of the growth distribution. Dr. Nelson maintains that growth will be concentrated in merged metropolitan areas, creating megapolitan areas. Dr. Nelson's report titled *Toward a New Metropolis: The Opportunity to Rebuild America*, (Brookings Institute, December 2004), provides the following building construction projections:



- The nation had about 300 billion square feet of built space in 2000. By 2030, about 427 billion square feet of built space will be needed to accommodate growth projections. About 82 billion of that will be from replacement of existing space and 131 will be new space. Thus, 50 percent of that 427 billion will have to be constructed between now and 2030.
- Most of the space built between 2000 and 2030 will be residential space. The largest component of this space will be homes. Over 100 billion square feet of new residential space will be needed by 2030. However, percentage-wise, the commercial and industrial sectors will have the most new space with over 60 percent of the space in 2030 less than 30 years old.

Household Occupancy Trends – Traditional Occupancy on the Wayne						
Household Type	1960	2000	2040			
Household with Children	48%	33%	27%			
Single-Person Household	13%	27%	30%			
Source: Census calculations by Arthur C. Nelson, Metropolitan Institute at Virginia Tech.						

- Overall, most new growth will occur in the South and the West. There is tremendous variation in the total amount of buildings to be built between regions. In the Northeast, for example, less than 50 percent of the space in 2030 will have been built since 2000, while in the West that figure is about 87 percent, a near doubling of built space. Fast growing southern and western places—states like Nevada and Florida and metropolitan areas like Austin and Raleigh—will see the most dramatic growth.
- Though a small component of overall growth, the projected demand for industrial space in the Midwest outpaces that of the other regions, unlike the other major land uses. States with a strong industrial presence will see the largest



amount of growth in industrial space even though other areas may witness faster growth. After California, which far outpaces the nation in terms of absolute square feet of new industrial construction, the next four largest producers of industrial space are all Rust Belt states in the Midwest: Ohio, Michigan, Illinois, and Indiana. By 2030, 70% of the Midwest's industrial space will be less than 30 years old.

- While these projections may seem overwhelming, they also demonstrate that nearly half of what will be the built environment in 2030 doesn't even exist yet, giving the current generation a vital opportunity to reshape future development. Recent trends indicate that demand is increasing for more compact, walkable, and high quality living, entertainment, and work environments. The challenge for leaders is to create the right market, land use, and other regulatory climates to accommodate new growth in more sustainable ways.
- The challenges to accommodate future development vary by region of the country. In general, Western states—like California, Washington, and Oregon—have a strong history of growth management and will need to continue to find ways to improve upon and implement existing laws and approaches. However, neighboring states like Nevada and Arizona, where explosive growth is expected to occur, will need to find their own comprehensive solutions to manage the development boom, while facing limitations on land and water. Overall, the West will not see reduced growth pressures, and will need to find innovative ways to accommodate growth on existing land, in cities and suburban areas.

By contrast, the rapidly-growing South is more resistant to regulating growth and must make some important choices about the kind of economic and overall quality of life it hopes to achieve.

3. Colorado Population Trends

Location	Existing Population	Project Pop. 2035	5 Year Growth Rate	Average 25 Year Growth Rate		
Colorado Total	5,171,798	7,699,126	1.7	1.5		
Front Range	4,243,767	6,150,375	1.7	1.6		
Denver	2,869,920	3,933,765	1.6	1.3		
Northern Front Range	546,233	1,014,748	2.8	2.4		
Colorado Springs	647,299	960,796	1.7	1.6		
Pueblo	162,385	241,156	1.2	1.5		
Western Slope	577,799	1,003,709	1.8	2.2		
Central Mountains	131,609	229,791	0.8	1.7		
Eastern Plains	163,289	247,909	0.3	1.2		
Source: Colorado State Demographer						

B. NEW URBANISM DEVELOPMENT

1. Define New Urbanism Movement. New

Urbanism is an urban planning philosophy, promoting pedestrian-oriented neighborhoods, mixed housing and job types and quality streetscape and architectural design elements. This urban form, prevalent in European countries, was popularized in US in the early 1980s and continues to reform many aspects of American urban areas by promoting functional pedestrian oriented streetscape, energy efficient design (LEED concepts), and quality architectural design, using a transect definition of the community.

New Urbanism is predicated on strong urban design standards. These standards generally promote elements such as the traditional

neighborhood design (TND) and transit-oriented development (TOD). The Congress for the New Urbanism is a central nonprofit organization promoting the new urbanism movement. This organization's mission is stated in the *Charter of the New Urbanism*, which says:

"We advocate the restructuring of public policy and development practices to support the following principles: neighborhoods should be diverse in use and population; communities should be designed for the pedestrian and transit as well as the car; cities and towns should be shaped by physically defined and universally accessible public spaces and community institutions; urban places should be framed by architecture and landscape design that celebrate local history, climate, ecology, and building practice."





2. Form Based Codes. Form-based codes are intended to achieve a specific built form. They create a predictable public realm by controlling physical form primarily, with a lesser focus on land use. Generally, form-based codes address the relationship between building façades and the public realm or streetscape, the form and mass of buildings in relation to one another, and the scale and types of streets and blocks. Formbased codes guidelines correspond to an overall plan that designates the appropriate form and scale (and therefore, character) of development rather than only distinctions in land-use types. This is in contrast to conventional zoning's focus on the segregation of land uses, and the control of



development intensity through dimensional standard (e.g., dwellings per acre, setbacks, parking ratios, and traffic Levels of Service (LOS). Form-based codes also sometimes include:

- Architectural Standards. Regulations controlling external architectural materials and quality.
- **Landscaping Standards.** Regulations controlling landscape design and plant materials on private property as they impact public spaces (e.g. regulations about parking lot screening and shading, maintaining sight lines, insuring unobstructed pedestrian movements, etc.).
- Signage Standards. Regulations controlling allowable signage sizes, materials, illumination, and placement.
- **Environmental Resource Standards.** Regulations controlling issues such as stormwater drainage and infiltration, development on slopes, tree protection, and solar access, etc.
- 3. **Miami 21 Form Based Code.** Miami is the first major metropolitan city in the nation to adopt a form-based code. *Miami 21* has been praised for the simplicity of zoning district standards and predictability. A property owner determines which zoning regulations apply to a parcel by locating the parcel in the Zoning Atlas which define the zoning area in a transect approach (rural to urban transition). An area may be rezoned only to a more intense district if the neighborhood abuts such a district (successional zoning).

14	15	T5-8	T6-12	T6-24	T6-36	T6-48	D1	02

DESCRIPTION									
Height	2 Story	3 Story	5 Story	8 Story +	1-8 Story	1-E Story			
Building Types	Detached Single-Family Dwelling	Party wall Residential, Live-Work	Residential, Commercial, Mixed-use	Residential, Commercial, Mixed-use	Workplace, Limited Residential Commercial	Industrial, Commercial			
Density	18 du /acre	36 du /acre	65 du /acre	150 du /acre or as per Residential Density Increase Areas	9 du /acre	None			

The *Miami 21* model is predicated upon public benefits and promotes pedestrian function rather than the automobile function. Guiding principles and public benefits include the following:

PLUMP. Automy familier

- contemporary urban streetscape design (wide sidewalks, narrow street, and street trees;
- active ground floors (large display windows & façade treatment, building mass, promote the front porch, prohibit snap-on garages;
- mixed uses (focus on architectural and streetscape design and deemphasize use restrictions;
- reduced infrastructure demand which is greater than City's capacity to provide them;
- affordable/workforce housing to support jobs base;
- waterfront access and parks to support the growing residential base;
- historic preservation of buildings and sites to support the unique character and touristic value;
- green building;
- brownfield redevelopment; and,
- civic and civil support spaces.

The risks identified by the Miami 21 model include:

- loss of development rights;
- the cost of public benefit programs;
- homogenized city form and stifled design creativity; and,
- vague provisions and unfamiliarity.





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4. Denver Form Based Code. On June 30, 2010 the City of Denver adopted a new land development code, replacing a code that had been in place for over 50 years and was described as complicated, antiquated and inconsistent. The new code, which was an outgrowth of the *Comprehensive Plan* (2000) and *Blueprint Denver* (2005), contains seven zone districts, compared to over 59 different zone districts in the previous code.

Denver's new code is not without its critics. In Kenny Be's *Denver Westword* article, <u>Everybody Must Get Zoned</u>, (1/7/2010), he described the new code stating "...*it is a control-freak fantasy*

with detailed rules for every aspect of city life. One example is the transparency provisions for ground-floor retail in the urban district. Transparency will be used "... To create rhythms and patterns on building facades that provide visual interest and reflect the uses within the building." The code also states that windows will occupy 30 percent of the ground floor wall-plan.





III. Planning Case Studies – Gunnison Basin

A. OVERVIEW OF THE GUNNISON BASIN

- 1. Gunnison is the fifth largest county area in the state, encompassing 3,260 square miles.
- 2. The average elevation is 9,500 feet.
- 3. Precipitation rates in the county are variable with Crested Butte averaging over 30 inches per year and Gunnison receiving about 10 inches annually.
- 4. The Upper Gunnison Drainage Basin covers approximately 6,330 square miles.
- 5. The County's population is approximately 15,000 with about 9,000 persons residing in the area of Gunnison.
- 6. Major employers include state and federal government, Western State College, mineral extraction, and the tourism service industry.
- 7 The County has five designated wilderness areas including the Maroon Bells, Fossil Ridge, and the Gunnison Gorge and one National Park; the Black Canyon of the Gunnison
- 8. Over 85 percent of the land area is managed by the federal government.
- 9. Highly charged issues in the County include:
 - Crested Butte Mountain Resort ski area expansion;
 - molybdenum on Mt. Emmons adjacent to Crested Butte;
 - the struggling economy and lack of economic diversity;
 - listing of the Gunnison Sage Grouse and Gunnison Prairie Dog;
 - geothermal energy resource production; and,
 - trans-mountain water diversion.


B. Mt Crested Butte—East Trade Parcel Annexation

1. East Trade Parcel Background. In 1996 the US Forest Service (USFS), Colorado Land Board and Crested Butte Mountain Resort (CBMR) implemented a land exchange that garnered 4,000 acres of critical habitat, wilderness in-holdings and mining claims in the County; in return 600 acres of USFS land adjacent to Mt. Crested was deeded to CBMR. The land exchange included 640 acres within the Maroon Bells Wilderness area and a 3,000 acre ranch containing critical elk, deer, and sage grouse habitat.

Gunsight Crossing

Wildflower Ridge

PRºSPE RiverSpur

- 2. East Trade Parcel Debate—Economics. CBMR was the only privately-held major ski area in Colorado and was struggling in 1998.
 - In the past two decades, the ski industry has enjoyed an enormous increase in terrain expansions, infrastructure improvements and real estate development, while during the same period; the number of ski areas operating in the U.S. decreased by 33% and total active skiers by 10%.
 - Destination skier visits to Crested Butte have been on a steady downward trend for the past twenty years.
 - CBMR's market share has decreased compared to other resorts.
 - National skier demographics are changing; baby boomers are getting older and request intermediate and advanced terrain.
 - CBMR lags in repeat visitors; only 54% return compared to 80% at Aspen or Vail.





The East Trade Parcel Debate—Geologic Hazards. Mt. Crested Butte is known as a laccolith, an igneous intrusive injected into overlying rock beds. The Mt. Crested Butte laccolith was injected into the Mancos Formation, a Cretaceous age shale formation. The steep slopes and geologic structure create a diverse set of geologic hazards.







East Trade The East Trade Parcel Debate—Wildfire Hazards. In 1995 the County initiated a GIS model to define wildfire hazards. The model inputs include ladder fuel and forest density inventories along with slope and aspect GIS models to rank wildfire risks.





East Trade Parcel Debate—Wetlands and Water Quality. The *Annexation Petition* spawned a significant debate regarding environmental protection and sustainability. The Town completed a wetland inventory in 2000 and adopted wetland setback regulations. The East Trade Parcel annexation was subject to these new regulations. Wetland buffers measures are based on wetland function with a 100 foot setback required except from isolated wetland complexes.





The East Trade Parcel Debate—Avalanche Hazards.

In 1991 an avalanche on Sunlight Ridge buried the entire first floor of a condominium – fortunately there were no injuries. Two years later a child was killed in the condominium parking lot when an avalanche slid from Sunlight Ridge. This is one of the only non-skiing related deaths reported in any US municipality from an avalanche. Mt. Crested Butte responded by creating one of the first avalanche mitigation regulations in the nation.





3. East Trade Parcel Development Plans—Land Use. The East Trade Parcel is a planned unit development which at this point is designated exclusively for residential development. The plan also calls for development of approximately 80 affordable housing units. However, the initial zoning included a 180,000 sq. ft. commercial component including a hotel, restaurant and gondola. The commercial component was a designated hub between the existing mountain and the proposed Snodgrass ski area expansion. The land use plan contains 280 acres of open space and ski terrain and development of up to 300 dwelling units.





East Trade Parcel Development Plans—Geological & Geotechnical Summary. With the assistance of the Colorado Geological Survey an extensive set of site investigations were initiated on the East Trade Parcel. Testing included a series of drill borings and test pit, a matrix of piezometer wells and the installation of 4 inclinometers that were monitored for 18 months in conjunction with the piezometer wells. The major issue to answer was regarding the potential for massive slope failure. The bedrock Mancos Shale, which dips about 5⁰ to the south, was found to be stable. Detritus material is saturated on a seasonal basis and requires engineered foundation design and special precautions for cut/fill placements.



GEOLOGIC HAZARDS AREN'T NECESSARILY ACTIVE ALL THE TIME



FIGURE 12. – North side of Crested Butte, Colorado, showing crest to southwest (right) and gravitational trenches northeast of crest (left from crest). Pronounced break in slope on east side (left) is approximate contact between porphyry and underlying Mancos Shale.

East Trade Parcel Development Plans—Site Grading Standards

- grading plans shall be prepared to conform to the master drainage plan;
- limit grading for walkout basements 20' limit;
- all residential grading will occur in the building envelope, improvement corridor, and transition area;
- cut and fill erosion protection is required;
- dissipate runoff to soils;
- resulting slopes must not exceed 2:1 and wherever possible, natural slopes are to be used instead of structures;
- cut and fill slopes are to be stabilized using an approved seed mix with straw and tackifier upon completion but no later than October 15th of each year; and,
- site preparation, grading and utility installation shall occur in accordance with an approved *Erosion Control and Stormwater Management Plan*.





East Trade Parcel Development Plans Development Standards—Wildfire Protection

Defensible Space

- All lots have a 50' defensible space zone.
- Dead branches on trees within the defensible space are trimmed or removed to minimize "ladder" fuel.
- Conifer trees in the defensible space shall be thinned to create 10' of separation between each crown.
- Conifer trees shall not be planted within 15' of a structure.
- Roof materials shall be non-flammable or have fire resistant rating.
- All chimneys shall be equipped with spark arresters.





East Trade Parcel Development Plans Development Standards—Grading, Erosion Control & Storm Water Management

- The final site plan/grading plan shall be prepared to conform to the master drainage plan.
- Finished grading associated with a walkout basement shall be designed such that no flat area not natural to the site will extend beyond the building envelope or beyond twenty 20' feet of the foundation, whichever is more restrictive.
- All residential grading will occur in the building envelope, improvement corridor, and transition area.
- Newly graded areas shall be protected against erosion by appropriate retention fences or permanent erosion controls.
- Splash blocks, gravel foundation drainage beds, or trench drains and underground, perforated drain pipes shall be utilized to dissipate runoff.
- Finish site grading shall not produce runoff detrimental to adjacent properties and native wetland areas.
- Finish site grading shall be done to retain rainfall for maximum percolation in turf areas.
- No excavation may take place except as necessary for the construction of dwellings or improvements.
- Retaining walls shall appear to be extensions of existing natural land forms.
- Resulting slopes must not exceed 2:1 and wherever possible, natural slopes are to be used instead of structures.
- Cut and fill slopes are to be stabilized using an approved seed mix with straw and tackifier upon completion, but no later than October 15th of each year. Irrigation is not required until final grading and landscaping is in place.
- Site preparation, grading and utility installation shall occur in accordance with an *Erosion Control and Stormwater Management Plan* approved by the Planning Commission and will include the limitation on dates of disturbance.



East Trade Parcel Development Philosophy—Nature's Envelope. The East Trade Parcel was processed through preliminary subdivision for the entire master plan. Lot configurations were established in a manner to avoid wetlands, drainages, steep slopes and with consideration for aspect, building separation, skier access and other factors. Building envelopes are designed on the plat with the envelopes to preclude wetland encroachment, avoid slope stability hazards, or negatively affect the implementation of Best Management Practices. Outside the home site/building envelope; improvement corridor; and landscape and wildfire management zones, the site is to remain in an essentially natural condition, maintained to blend with all adjoining Nature's Envelopes.



C. WEST GUNNISON NEIGHBORHOOD PLAN

1. Existing Neighborhood Conditions

- Approximately 200 acres.
- The majority of the land area is undeveloped and had no utility extension plan.
- The neighborhood is constrained by a limited number of access points.
- The neighborhood is predominately zoned for high density residential development. Underlying zoning would allow for the development of 2,100 units generating 15,000 to 20,000 vehicle trips per day.
- Jurisdictional wetlands and floodplains exist within the neighborhood.



WEST GUNNISON AREA



POTENTIAL APPORDABLE HOUSING SITE

- 2. West Gunnison-Neighborhood and Community Context
 - limited access to the town center and employment facilities
 - limited access to shopping and downtown
 - opportunity to promote locations for profession/retail use
 - opportunity to expand alternative travel modes



- 3. West Gunnison-Preferred Land Use
- 960 residential units anticipated and 150,000 square feet of professional office/retail
- limit development in the flood hazard zones
- three major highway intersections identified
- utility system sizing and extensions corridors identified
- public transit center is a permitted use
- Low Impact Design (LID) contemplated at varying scales







2. West Gunnison – Low Impact Development

- Currently a 10-year storm event generates essentially no runoff; any surface runoff flows into existing irrigation ditches.
- The City's standards require that post development maintain pre-development discharge.
- Low Impact Development practice.
- Regional detention systems will be designed to maintain a 100 year event
- LID concepts are defined for individual lots, a street block area, and neighborhood-wide venue.
- Street sections are significantly narrower than the traditions city streets.







Legal Elements

- Know the general boundaries of the law and planning process do not cross these bounds.
- Urban drainage and floodplain management often cross several different jurisdictional boundaries and it's incumbent upon the professionals to know the local zoning code.
- Be cognizant of the local jurisdiction status and whether it is a statutory or home rule jurisdiction.
- In order to avoid legal issues make sure to follow due process procedures set forth in local codes.
- Listen to your attorney and follow their opinion.



Demographic Projections

- The next 30 years the United States will see significant population growth
- Major metropolitan areas will see significant growth with megapolitan regions being developed. The front-range corridor will form into a megapolitan region.
- Significant growth will occur in the western United States, and there are serious resources issues to be overcome.
- Growth management systems, permitted through state statutes will be the key element in directing and managing growth.
- Traditional industrial areas in the northeast will see a significant resurgence in industrial uses.
- Mass transit will play a critical role in growth distribution and accessibility don't count on telecommuting to reduce commuting issues.
- Think about how your decisions affect the community's future.



Smart Growth

- Smart growth starts with the comprehensive plan.
- Developers are buying into the concepts of traditional neighborhood development forms, which will help to provide in-fill and more dense development.
- Communities will need to place more focus on the pedestrian and less on the automobile.
- Economics will drive the need for local governments to focus on sustainable service extensions. Urban growth boundaries will be used to limit sprawl.
- Developing high density neighborhoods requires creative solutions for stormwater management, but smart growth requires that solutions be defined and implemented.
- In general, unincorporated jurisdictions should avoid getting into the urban services business – more often than not counties are not able to provide urban services.



Development Processes

- Inventory natural resources before allowing the expansion of urban areas, and protect critical habitat and resources.
- Follow smart growth principles.
- Be aware of the true cost of growth growth for the simple sake of growth is not economically sustainable.
- There is no perfect plan, but do not dance around issues.
- Be pragmatic in the development process, and provide necessary information and honest assessments to elected officials so that informed decisions can be made.



QUESTIONS

